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# DEVELOPMENT OF AN IMPROVED COMPUTER MODEL OF THE HUMAN BODY AND EXTREMITY DYNAMICS

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BUFFALO, NEW YORK 14221*

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## PREFACE

This report describes the modifications which were incorporated into the Phase III\* Calspan Three-Dimensional Crash Victim Simulation Program to satisfy current Air Force requirements.

Three principal modifications are:

1. Improved Joint Formulation
2. Improved Belt Formulation
3. Inclusion of Aerodynamic Forces.

The modifications have been made so that they may be used on the CDC6600 computer at the Mathematics and Analysis Branch of AMRL.

The research effort summarized in this report was performed for the Aerospace Medical Research Laboratory [FY8990] under Contract No. Calspan F33615-75-C-5002. Dr. John T. Fleck of the Computer Mathematics Department of Calspan served as principal investigator.

The authors wish to thank Ints Kaleps of the Aerospace Medical Research Laboratory for his suggestions and direction during the analytical development of the program.

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\*Phase III was sponsored by the National Highway Traffic Safety Administration, Department of Transportation. The ground work for the simulation was performed in Phases I and II, both jointly sponsored by NHTSA and the Motor Vehicle Manufacturers Association.



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## Section 1

### INTRODUCTION

The Calspan 3-D Crash Victim Simulation Model was originally developed to study human body dynamics associated with automobile accidents. The formulation, however, is quite general, giving it great versatility and making it applicable to many studies involving human body dynamics. Reference 1 contains a complete description of this model.

To fit the specific needs of the Mathematics and Analysis Branch (BBM) of the Aerospace Medical Research Laboratory (AMRL), three principal modifications have been made to the program. These are: an improved joint formulation, an improved belt restraint formulation and the inclusion of aerodynamic forces.

The modifications are described in the following sections.

## Section 2

### JOINT ALGORITHM

The joint routine, subroutine VISPR, which is in the Calspan 3-D Crash Victim Model, has been modified to provide the option of computing the flexure torque as a function of both the flexure angle (elevation) and azimuth angle.

### NOMENCLATURE

$D_m$	3 x 3 direction cosine matrix specifying the orientation of segment m's local reference with respect to the inertial reference.
$T_{m,n}$	3 x 3 direction cosine matrix specifying the relative orientation of joint n's local reference with respect to the local reference of segment m.
$T$	3 x 3 direction cosine matrix specifying the relative orientation of joint's local reference systems, $T=I$ , the identity matrix, is the equilibrium position.
$T_{ij}$	$ij^{th}$ element of matrix $T$ .
$r_{m,n}$	3 x 1 matrix (vector) specifying the location of joint n as measured in segment m's local reference.
$x, y, z$	used to designate axes of a right handed coordinate system
$x_m, y_m, z_m$	may be regarded as 3 x 1 matrix (vector) which is of unit magnitude and is orthogonal.

# NOMENCLATURE (CONTINUED)

$\theta$	flexure angle of joint.
$\psi$	torsion angle of joint.
$\phi$	azimuth angle used to describe flexure torque asymmetrically.
$\mu$	3 x 1 matrix (vector) of unit magnitude used to designate axis of flexure.

## Joint Routine

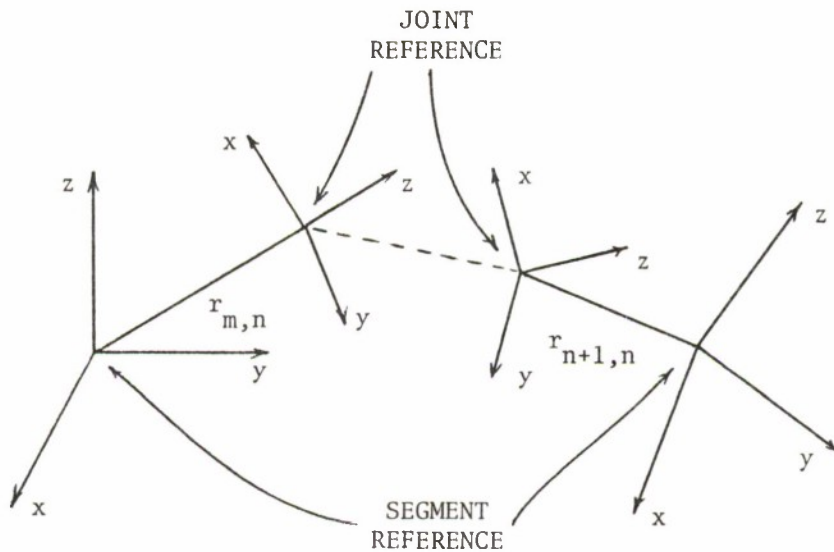


FIGURE 1 Joint Coordinate System

The position of joint n, which is fixed in segment m, is given by vector  $r_{m,n}$  (see Figure 1). The orientation of the joint with respect to segment m's reference system is given by the direction cosine matrix  $T_{m,n}$ . The matrix  $T_{m,n}$  is computed from the yaw (about Z), pitch (about Y), and roll (about X) angles, which are specified on input along with the vector  $r_{m,n}$ .



Joint  $n$  connects segments  $m$  and  $n+1$ . The vector  $r_{n+1,n}$  and the matrix  $T_{n+1,n}$  are determined from input as were  $r_{m,n}$  and  $T_{m,n}$ .

For the relative orientation of the joint we have

$$T_{m,n}^T D_m = T_{n+1,n} D_{n+1}$$

$$T = T_{n+1,n} D_{n+1} (T_{m,n} D_m)^1$$

where  $D_m, D_{n+1}$  are the direction cosine matrices specifying the orientation of the segments and  $T$  is the direction cosine matrix specifying the relative orientation of the joint, and where  $A^1$  is the transpose of  $A$ .

$T_{m,n}$  and  $T_{n+1,n}$  are defined so that the equilibrium position of the joint occurs when  $T=I$ , the identity matrix.

Consider the following figure

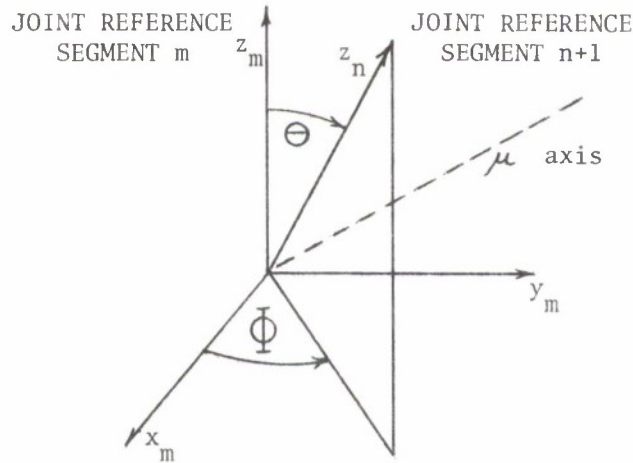


FIGURE 2 Joint Flexure

The angle,  $\theta$ , between the  $Z$  axes of the joint reference systems is defined as the flexure angle of the joint. The angle,  $\phi$ , between the projection of  $z_n$  in the  $X_m Y_m$  plane and the  $X_m$  axis is defined as the azimuth angle. A twist (torsion) angle,  $\psi$ , may be defined as either a rotation about  $Z_m$  or a rotation about  $Z_n$ .

If the joint is pinned (hinge joint), the pin axis is taken as the Y axis, hence  $Y_m$  is parallel to  $Y_n$  for this pinned joint. In this case,  $\bar{\Phi}$  may either be 0 or  $\pi$ .

### Flexure

The axis of flexure,  $\mu$ , may be computed as the vector cross product of  $Z_m$  and  $Z_n$ .

$$\text{That is } \mu = Z_m \otimes Z_n / |Z_m \otimes Z_n|.$$

Note that when  $\theta=0$  or  $\theta=\pi$ ,  $\mu$  is undefined. The case  $\theta=\pi$  will not be considered. We will assume that  $0 < \theta < \pi$ . That is, any flexure angle equal or greater than  $\pi$  will never occur.

The direction cosines of a vector in the direction of  $Z_n$  with respect to joint reference m are given by the third row of the matrix T (i.e. the third row of T is a unit vector in the  $Z_n$  direction.)

We have

$$\sin \theta \cos \bar{\Phi} = T_{31}$$

$$\sin \theta \sin \bar{\Phi} = T_{32}$$

$$\cos \theta = T_{33}$$

Hence

$$\theta = \cos^{-1} T_{33}$$

$$\bar{\Phi} = \tan^{-1} \left( \frac{T_{32}}{T_{31}} \right) \quad \text{if } \theta \neq 0$$

$$\mu = \begin{pmatrix} -T_{32} \\ T_{31} \\ 0 \end{pmatrix}$$

where  $T_{ij}$  is the  $i, j^{\text{th}}$  element of the matrix T.

Define the matrix  $T_{\mu}$  which represents a rotation of  $\theta$  about the axis  $\mu$ . We have, in matrix form,\*

$$T_{\mu} = \mu \mu^1 + (I - \mu \mu^1) \cos \theta - \sin \theta \mu \otimes$$

where  $\mu \otimes$  is the matrix

$$\mu \otimes = \begin{pmatrix} 0 & -\mu_z & \mu_y \\ \mu_z & 0 & -\mu_x \\ -\mu_y & \mu_x & 0 \end{pmatrix}$$

In our case,  $\mu_x = -T_{32}$ ,  $\mu_y = T_{31}$  and  $\mu_z = 0$ .

We compute the restoring torque for flexure,  $f(\theta, \Phi)$ , as a function of the flexure angle,  $\theta$ , and the azimuth,  $\Phi$ . The torque,  $+f(\theta, \Phi)\mu$ , will be applied to segment  $m$  and the torque,  $-f(\theta, \Phi)\mu$ , will be applied to segment  $n+1$ . We assume that when  $\theta = 0$ ,  $f(\theta, \Phi) = 0$ , hence the fact that  $\Phi$  and  $\mu$  are undefined in this case will be of no consequence.

### Representation of Flexure Torque

We use the following approximation for the torque function  $f(\theta, \Phi)$ .

The function,  $f(\theta, \Phi)$ , is represented as a continuous or tabular function of  $\theta$  for discrete values of  $\Phi$ .

That is,  $f(\theta, \Phi_n) = g_n(\theta)$   $n=1, N$

and where  $\Phi_1 = -\pi$ ,  $\Phi_2, \dots, \Phi_N, \Phi_{N+1}$ , ( $\Phi_{N+1} = \pi$ ), are equally spaced between  $-\pi$  and  $\pi$  and it is assumed that  $f(\theta, \pi) = f(\theta, -\pi)$  therefore  $\Phi_{N+1}$  is not required. (The range  $-\pi$  to  $\pi$  is used to be consistent with the four quadrant arctan routines, which are used to evaluate  $\Phi$ .)

---

\* Reference 1, Volume 1, page 23.

The value of N will be restricted only by the storage one is willing to allocate and the computing time involved.

The function  $g_n$  may be defined as the  $m^{th}$  degree polynomial in  $(\theta - \theta_o)$  or as a table. (They cannot be mixed, i.e. for a particular joint all  $g$  must be tabular or polynomial.)

In both cases, a deadband may be specified, i.e. a  $\theta_{n_o}$  is given and  $g_n(\theta) = 0$  if  $\theta < \theta_{n_o}$ .

For intermediate values of  $\Phi$  (i.e.,  $\Phi_n < \Phi < \Phi_{n+1}$ ), we evaluate  $f$  for  $g_n$  and for  $g_{n+1}$  and linearly interpolate on  $\Phi$ . The wrap around if  $\Phi > \Phi_N$  or  $\Phi < \Phi_1$  is treated consistently (i.e., interpolate between  $g_N$  and  $g_1$ .)

#### Twist (Torsion)

When there is no flexure, i.e.  $\theta = 0$ , the twist  $\gamma$  is easily defined as the rotation about the  $Z_m$  axis. In this case

$$T = T_Z(\gamma) = \begin{pmatrix} \cos \gamma & \sin \gamma & 0 \\ -\sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

When  $\theta$  is not equal to zero, we may think of first twisting about  $Z_m$  and then rotation about the axis  $\mu$

$$T = T_\mu(\theta) T_Z(\gamma)$$

or we may first rotate about  $\mu$  and then twist about the resultant  $Z$ , i.e.  $Z_n$ .

$$T = T_Z(\gamma) T_\mu(\theta)$$

These definitions are equivalent and thus give a unique definition of the angle  $\gamma$ . To show this, we expand  $T$  as

$$T = T_Z(\mu \mu^1 + (I - \mu \mu^1) \cos \theta - \sin \theta \mu \theta)$$

and as

$$T = (\mu_1 \mu_1^1 + (I - \mu_1 \mu_1^1) \cos \theta - \sin \theta \mu_1 \theta) T_Z$$

where  $\mu_1 = T_{Z_m} / \dot{\psi}$ , i.e. the axis of rotation is fixed in the  $X_m, Y_m$  plane. Substituting for the value of  $\mu_1$  in the above expression shows the equivalence.

Although the angle  $\psi$  is well defined, it does not seem possible to uniquely define an axis, which may be used for the restoring torque. This problem exists because we are talking about a mathematical definition of twist and not a physical description of a joint.

The program has been coded to use the  $Z_m$  axis. The magnitude of the torque is computed by the standard spring function characteristics available in the program. This is done using subroutine EFUNCT.

The torque,  $q$ , is computed from the five parameters  $S_1, S_2, S_3, S_4$  and  $S_5$  by the following algorithms.

$$\begin{aligned} \text{If } \psi &\leq S_5 \\ q &= S_1 \psi \end{aligned}$$

If  $\psi > S_5$  an additional torque  $q_s$  is computed as

$$q_s = S_2(\psi - S_5)^2 + S_3(\psi - S_5)^3$$

If  $\dot{\psi} < 0$  (unloading)  $q_s$  is modified by  $q_s = S_4 q_s$

(If  $S_5$  is equal to zero,  $q_s$  is not computed but  $q$  is modified by  $S_4$ .)

For small values of  $|\dot{\psi}|$ , (10 radians/sec), the routine interpolates between the loading and unloading characteristics.

The total torque  $q + q_s$  is returned as the function value.



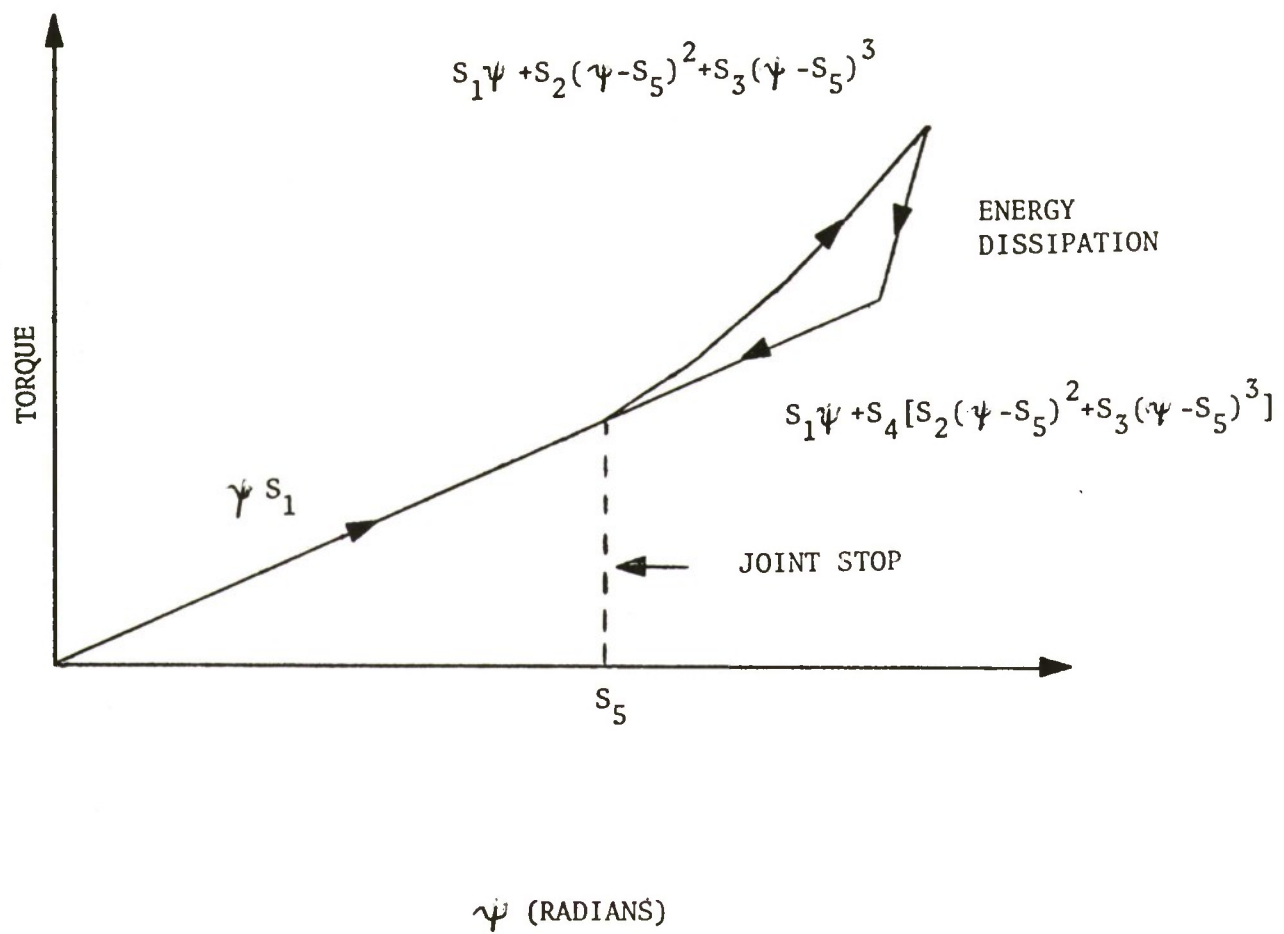
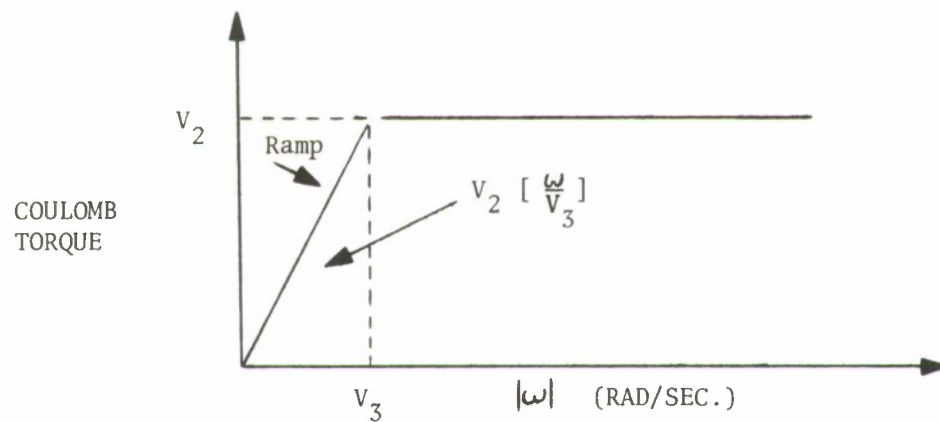


FIGURE 3 JOINT SPRING TORQUE

## Viscous and Coulomb Torques

Let  $\omega$  be the relative angular velocity. A torque is computed to oppose this velocity using the standard viscous function definition in the program. This is illustrated in Figure 4.



$$q/|\omega| = V_1 + V_2 / (\max(|\omega|, V_3))$$

$\omega$  is the relative angular velocity.

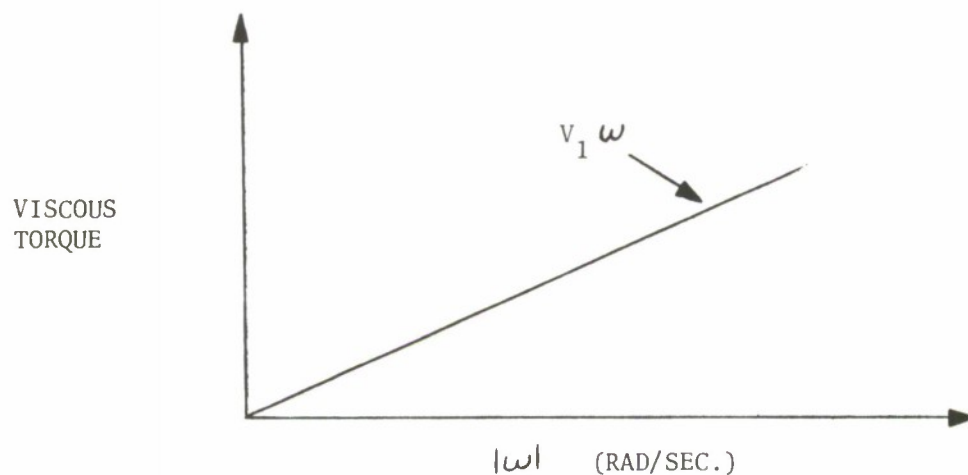


FIGURE 4 JOINT TORQUE DUE TO RELATIVE ANGULAR VELOCITY AT THE JOINT

### Section 3

#### BELT ALGORITHM

The belt routine in Version III of the Calspan 3-D program is restricted to a simple belt passing around a single segment. Although several of these belts may be used, no provision for interaction of the belts was made.

To overcome this restriction and to satisfy the requirements of the current contract, an entirely new belt algorithm has been developed and incorporated into the program.

The current version of the algorithm assumes each belt lies essentially in a plane which may be described by a set of reference points rigidly attached to segments. Thus, its use should be restricted to harnesses (several belts connected at a common junction point) which constrain the segments involved from large relative motions.

The algorithm should lend itself to significant improvements in the modeling of harnesses.

The concept of a harness is introduced in this version of the program. A harness consists of from one to several belts. Each belt is defined as the set of straight line segments connecting prescribed reference points. One end of the belt is the anchor point and the other end the junction point. See Figure 5 below.

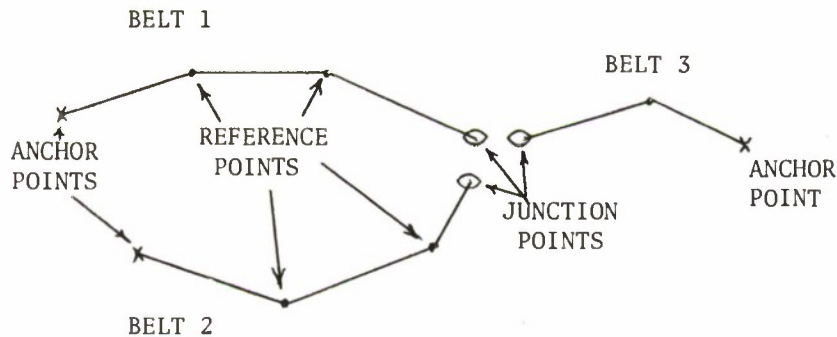


FIGURE 5 BELT HARNESS MODEL

Each reference point is fixed relative to a prescribed segment. An ellipsoid is assigned to each reference point. The ellipsoid is fixed to the same segment as the reference point. Ellipsoids associated with the anchor point and the junction point are ignored in the current version of the program hence may be specified as zero. The ellipsoid is used to determine an outward normal vector to the surface of the ellipsoid at the reference point. If the net force on the segment at this point has a positive component along this normal, the point will be ignored in computing the belt length. If no ellipsoid is specified for an interior point, this point will always be used in computing the belt length. For example, see Figure 6.

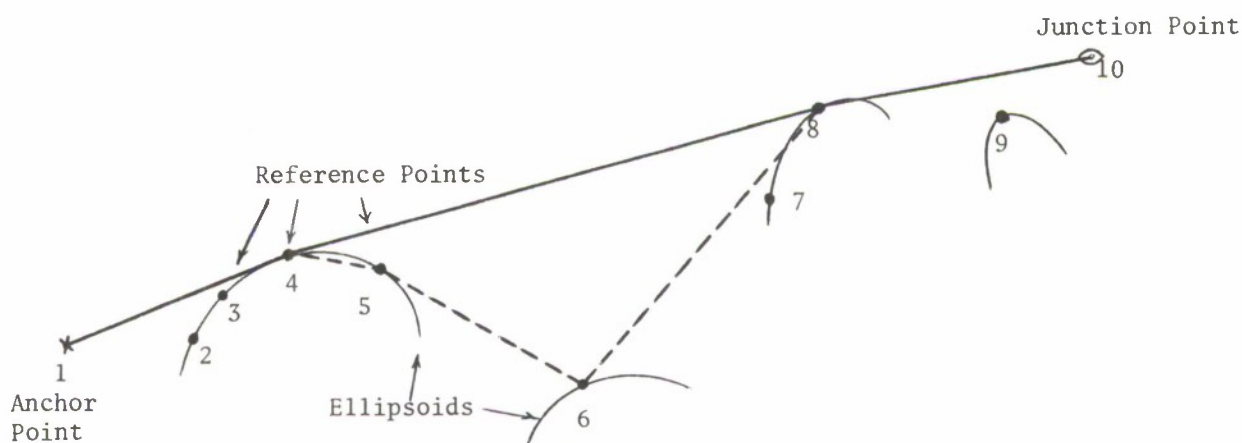


FIGURE 6 BELT LENGTH SPECIFICATION

In this example, the belt is defined by the 10 reference points illustrated. Ellipsoids associated with the interior points are represented by the curved lines. In the above configuration, the belt length would be computed as the sum of the length of the lines from 1 to 4, 4 to 8 and 8 to 10 as illustrated by the solid lines.

If no ellipsoid were specified for point 6, the belt would follow the dashed line, 1-4-5-6-8-10. The algorithm determines this belt configuration in the following manner:

1. The belt is first assumed to go from point 1 to point 2 to point 3.
2. The net force at point 2 (assuming constant tension) is found to be directed along the outward normal to the reference ellipsoid assigned to point 2 hence point 2 is dropped from consideration.
3. The belt is next assumed to go from point 1 to point 3 to point 4.
4. This is the same situation as was found in step 2 above hence point 3 is dropped.
5. The belt is next assumed to go from point 1 to point 4 to point 5.
6. The net force at point 4 is directed along the inward normal to the ellipsoid assigned to point 4 hence point 4 is accepted.
7. The belt is next assumed to go from point 4 (the last accepted point) to point 5 to point 6.
8. The net force at point 5 is found to be directed along the inward normal to the ellipsoid assigned to point 5 hence point 5 is accepted.
9. The belt is next assumed to go from point 5 to point 6 to point 7.
10. The net force at point 6 is found to be directed along the outward normal to the ellipsoid assigned to point 6 hence point 6 is dropped from consideration.
11. Point 5 was accepted because 4,5,6 were acceptable, since 6 is now rejected and the belt is assumed to go from 4 to 5 to 7.



This process is continued resulting in the following condensed steps.

12. 5 is rejected.

13. Try 4-7-8.

14. 7 rejected.

15. Try 4-8-9.

16. 8 accepted.

17. Try 8-9-10.

18. 9 rejected.

19. Since 10 is a junction point, the final belt is 1-4-8-10.

#### Computation of Belt Tension

The strain is computed as

$$\text{strain} = \frac{\text{calculated length} - \text{reference length}}{\text{reference length}}$$

The stress (tension) is computed by the standard force deflection routines available in the program using strain as the deflection parameter.

The current version of the program assumes that the tension is uniform in the belt.

## Examples

The above technique provides considerable versatility in defining belt systems. For example:

### SIMPLE LAP BELT

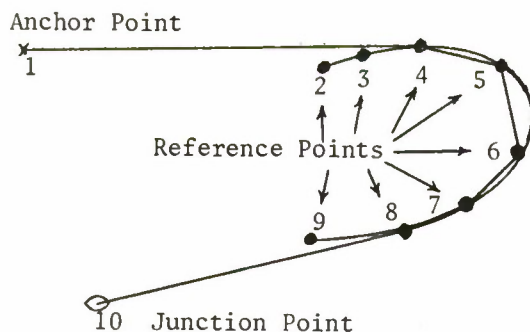


FIGURE 7 Simple Lap Belt Harness Configuration

Define a harness consisting of one belt. In this case, the junction point is actually an anchor point. All interior reference points are attached to the same segment and assigned the same reference ellipsoid.

### SHOULDER BELT AND LAP BELT

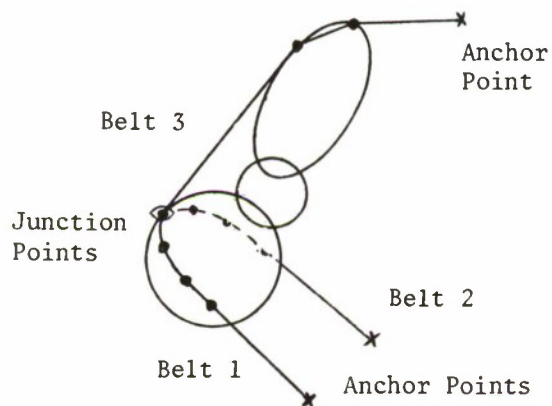


FIGURE 8 Shoulder Belt and Lap Belt Harness Configuration

Define a harness consisting of three belts with the junction points attached to a segment, which is disjoint (but need not be) from the body segments. This segment is assigned a mass and an inertia tensor and will move dynamically to achieve a force balance. (we recommend that the junction points all be located at the cg of the junction segment to prevent large angular accelerations.)

The Input Description of the program contains the details of inputting a belt system.

#### General Comments

Since there is no limitation (except storage) on the number of harnesses, belts or reference points, quite elaborate belt systems may be modeled.

The program is so written that it may be modified to include effects of belt friction and deformation of the surface at the reference points. For example, the reference points could be moved along the normal as a function of the normal force.

The belt is not constrained to lie in a plane. The algorithm, as illustrated in Figure 5, was designed on the assumption that the interior reference points lie essentially in a plane. Highly, non planar sets of points may produce unexpected results. No study has been made of this potential problem or of other unusual configurations that would cause the algorithm to fail.

The computation of frictional effects and deformation is complicated by the fact that a change in belt position or tension at one point affect all the points. Thus, the problem would require the use of techniques such as finite element methods. However, a first approximation to the effects of deformation could be made by holding the reference points fixed during the course of an integration step and at the completion of a successful integration step the points could be moved along the normal (as defined by the reference ellipsoid) as a function of the normal force computed from the current belt configuration. Alternately, the point could be moved in the direction of the net force. Storage has been allocated in the program to store a fixed reference point and a modified reference point. Perhaps the effects of friction could be approximated by allowing the modified reference point to move in a direction other than along the normal. Future study should consider these possibilities.

## Section 4

### AERODYNAMIC FORCES

Routines have been added to the program to allow the application of a specified force to any segment. The method allows any force to act on any segment. In addition, for each segment a boundary plane is specified and the force is not applied until the segment penetrates the boundary plane.

An aerodynamic pressure, a boundary plane, and an ellipsoid are associated with each segment for which it is desired to compute an aerodynamic force. The aerodynamic pressure, as a function of time, is inputted as tabular data.

As the ellipsoid penetrates the boundary plane, an estimate of the projected area normal to the pressure is made and the force and torque are computed and applied to the segment. For partial penetration, the force is applied at a point in the ellipsoid. At full penetration, the force is applied at the center of the ellipsoid.

### MATHEMATICAL FORMULATION

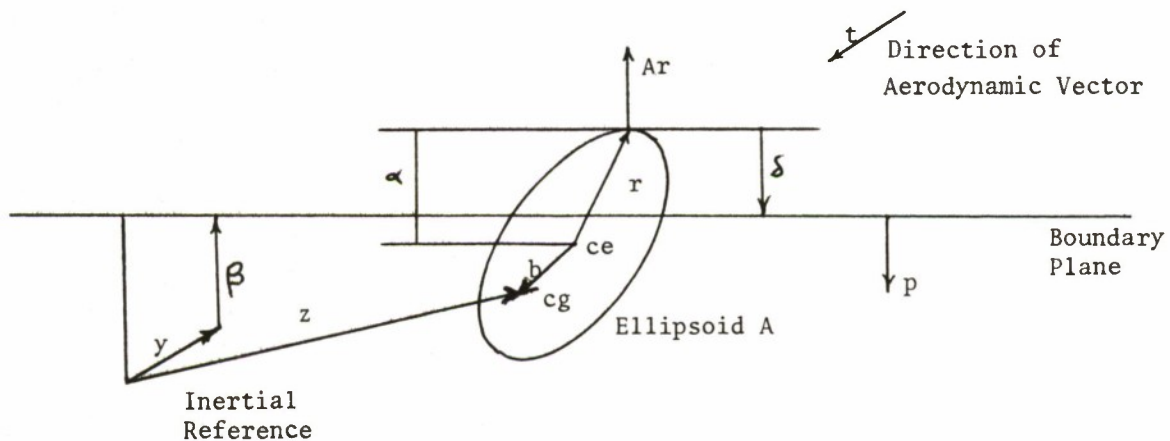


FIGURE 9 BOUNDARY PLANE PENETRATION BY ELLIPSOID

Let  $y$  location of reference point for plane  
 $z$  location of cg of segment  
 $b$  offset of center of ellipsoid from cg  
 $e$  penetration distance  
 $p$  unit vector describing outward normal to boundary plane  
 $r$  vector from center of ellipsoid to point of maximum penetration  
 $\alpha$  distance from center of ellipsoid to point of maximum penetration  
 $t$  vector describing wind (force per unit area)  
 $A$  matrix defining the ellipsoid (a 3x3 positive definite matrix.)  
 $\beta$  distance of plane from its reference point

We have the following equations:

$$r \cdot Ar = 1 \quad \text{if } r \text{ is on the ellipsoid}$$

$$p \cdot r = -\alpha$$

$$p \cdot [z + b + r] = -\beta + S + p \cdot y$$

$$Ar \quad \text{vector normal to ellipsoid at } r.$$

At a given instant in time we know  $y, z, b, p, t$  and  $A$ .

In the computer program, the ellipsoid matrix is a given constant in the reference system of the segment. All quantities are first converted to this reference system for ease of computation.

#### COMPUTATION OF PENETRATION DISTANCE

If  $r$  goes to the point of maximum penetration, then

$$Ar = c p, \text{ where } c \text{ is some constant}$$

since  $r \cdot Ar = 1$  if  $r$  is on the ellipsoid

$$r = c A^{-1} p$$

$$r \cdot Ar = c^2 p \cdot A^{-1} p = 1$$



$$\text{then } c = 1 / \sqrt{p \cdot A^{-1} p}$$

$$\text{and } r = A^{-1} p / \sqrt{p \cdot A^{-1} p}$$

The penetration distance  $\mathcal{S}$  may be computed as

$$\mathcal{S} = p \cdot [z + b + r - y] - \beta ,$$

and  $\alpha$  may be computed as

$$\alpha = p \cdot r = \sqrt{p \cdot A^{-1} p}$$

If  $\mathcal{S}$  is less than zero, no penetration has occurred.

If  $\mathcal{S}$  is greater than  $2\alpha$  the ellipsoid has fully penetrated the plane.

#### COMPUTATION OF PROJECTED AREA

If penetration has occurred, we must distinguish between three cases in the computation of the shadow (projected) area of the ellipsoid onto the plane.

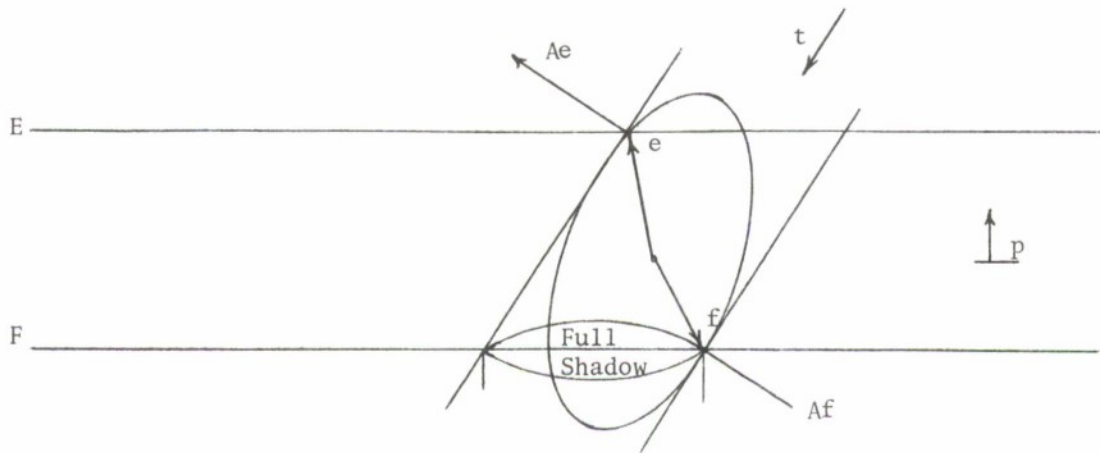


FIGURE 10 SHADOW (PROJECTED) AREA OF ELLIPSOID ONTO A PLANE

Consider the above figure where planes E and F are parallel to the boundary plane p and are such that at the points e and f which are on the ellipsoid and in the indicated planes we have  $t \cdot Ae = 0$ ,  $t \cdot Af = 0$  and the planes are positioned that  $|p \cdot e|$  and  $|p \cdot f|$  are at their maximum values (i.e. if the planes were moved further away from the center of the ellipsoid, no such points could be found.)

#### Consider the Three Cases

Case I The boundary plane is above plane E but still intersects the ellipsoid. In this case, the projected area is the area of the ellipsoid formed by the intersection with the plane p projected on a plane normal to t.

Case II The boundary plane is between planes E and F. This is a region where the projected area is made up of parts of two ellipses. One is the shadow ellipse and the other is the ellipse formed by the intersection of the ellipsoid and the plane p.

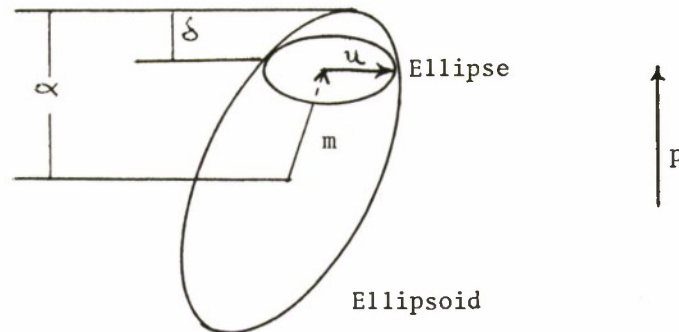
Case III The boundary plane is below plane F. In this case, the full shadow ellipse is produced and does not alter with the penetration distance or orientation of the boundary plane.

# Computation in the Above Cases

It may be shown that

$$p \cdot e = (p \cdot A^{-1} p - (p \cdot t)^2 / t \cdot A t)^{1/2} = -p \cdot f$$

Case I This case exists when  $\delta > 0$  and  $\alpha > p \cdot e + \delta$



The center of the ellipse of intersection is at m where

$$m = (\alpha - \delta) A^{-1} p / p \cdot A^{-1} p$$

FIGURE 11 Intersection Ellipsoid

The equation of a point u on this ellipse is

$$u \cdot B u = 1$$

where u is measured from the center of the ellipse hence lies in the plane of intersection, and

$$B = (I - p p \cdot) A (I - p p \cdot) / (1 - m \cdot A m)$$

$$m \cdot A m = (\alpha - \delta)^2 / p \cdot A^{-1} p$$

The matrix B is singular (has a zero eigenvalue) but the product of the two non zero eigenvalues is the reciprocal of the square of the product of the major and minor axis of the ellipse. The area is the product of  $\pi$  times the product of the major and minor axes.

We have

$$P = \text{product of eigenvalues} = [(\text{tr}(B))^2 - \text{tr}(B^2)]/2$$

where  $\text{tr}(B)$  is the trace (sum of diagonal elements) of the matrix  $B$ .  
For a matrix such as  $B$ , the product of the eigenvalues can most readily be computed as the sum of the principle minors.

Hence,

$$\text{Area} = \pi (1 - m \cdot A_m) / p^{1/2}$$

The area normal to  $t$  is then equal to  $|p \cdot t|$ .

The point of force application will be taken as the center of the ellipse (i.e. At  $m$ )

### Case III Full Shadow

This exists when  $\delta > 0$  and  $\delta > p \cdot e + \alpha = \alpha - p \cdot f$

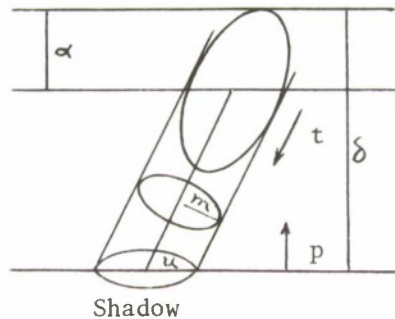


FIGURE 12 Full Shadow

At point  $u$  on the shadow ellipsoidal cone is measured from the center of the ellipse in a plane  $\perp$  to  $t$ .

$$u \cdot C u = 1$$

$$\text{where } C = A - At(At) \cdot t \cdot At$$

The product  $p$  of the nonzero eigenvalues is the sum of the principle minors of  $C$ . The projected area is then  $\text{Area} = \pi / p^{1/2}$

The force is applied at center of ellipsoid.

## Case II Mixed Region

The exact calculation here is involved since it involves the computation of areas of partial ellipses. Since the method of aerodynamic force computation is only an approximation, we decided that it is reasonable to compute the projected area and the point of force application in the following manner:

1. Referring to Figure 9, if  $\mathcal{S}$  is less than zero, no penetration has occurred so no aerodynamic force will be applied.
2. If  $\mathcal{S}$  is positive, a scale factor is computed as (Figure 10)  
$$\text{Scale} = (\alpha - \mathcal{S} + |p \cdot e|) / (\alpha + |p \cdot e|)$$

If scale is greater than one, no penetration has occurred ( $\mathcal{S} < 0$ ).  
If scale is less than zero, the ellipsoid has penetrated enough that Case III applies. In this case, scale is set to zero.
3. The full projected Area is computed by the formula in Case III  
$$\text{Area} = \pi / p^{1/2}.$$

The effective area is computed as  
$$\text{Effective Area} = (1 - \text{Scale}^2) * \text{Area}$$
4. The point of force application is computed as  
$$q = \text{Scale} * r$$

where  $r$  is the vector from the center of the ellipsoid to the point of maximum penetration (see Figure 9.)
5. The aerodynamic force is computed by interpolating the given table of pressure for the proper time and multiplying this pressure by the Area.
6. The force and torque are then applied to the segment.

## Section 5

### REFERENCES

1. Fleck, J.T., Butler, F.E., and Vogel, S.L., "An Improved Three-Dimensional Computer Simulation of Motor Vehicle Crash Victim," Calspan Technical Report No. ZQ-5180-L-1, July 1974. Vol. I Engineering Manual, Vol. II Model Validation, Vol. III User's Manual, Vol. IV Programmer's Manual.
2. Bartz, J.A., "A Three-Dimensional Computer Simulation of a Motor Vehicle Crash Victim' Phase 1 Development of the Computer Program" Calspan Technical Report No. VJ-2978-U-1, July 1971.
3. Bartz, J.A., and Butler, F.E., "A Three-Dimensional Computer Simulation of a Motor Vehicle Crash Victim' Phase 2 Validation of the Model, "Calspan Technical Report No. VJ-2978-V-2, December 1972.

## APPENDIX A

REV 12 12/19/74

INPUT DESCRIPTION FOR THE CALSPAN 3-D CRASH VICTIM SIMULATION PROGRAM  
AS SUPPLIED TO WRIGHT PATTERSON A.F.B. (CONTRACT NO. F33615-75-C-5002)

NOTE: THIS REPORT IS SUPPLIED WITH 'I' IN COLUMN 1 FOR PAGE SKIP  
CONTROL TO ALLOW FOR PRINTING ON VARIOUS COMPUTER SYSTEMS.

THE FOLLOWING SPECIAL SYMBOLS MAY DIFFER ON OTHER SYSTEMS:

"#" IS USED TO INDICATE "NOT EQUAL".  
"<" IS USED TO INDICATE "LESS THAN".  
">" IS USED TO INDICATE "GREATER THAN".  
"|" IS USED TO INDICATE "ABSOLUTE VALUE".

ANY LINE WITH A "|" AT THE RIGHT INDICATES A CHANGE MADE TO THIS  
INPUT DESCRIPTION INCLUDED IN CALSPAN REPORT NO. ZQ-5180-L-I ENTITLED  
"AN IMPROVED THREE DIMENSIONAL COMPUTER SIMULATION OF MOTOR VEHICLE  
CRASH VICTIMS" (JULY 1974).

OUTLINE OF INPUT TO THE PROGRAM :

- CARDS A - DATE AND RUN DESCRIPTION, UNITS OF INPUT AND OUTPUT,  
CONTROL OF RESTART, INTEGRATOR AND OPTIONAL OUTPUT.
- CARDS B - PHYSICAL CHARACTERISTICS OF THE SEGMENTS AND JOINTS.
- CARDS C - DESCRIPTION OF THE VEHICLE MOTION.
- CARDS D - CONTACT PLANES, BELTS, AIR BAGS, CONTACT ELLIPSOIDS,  
CONSTRAINTS, AND SYMMETRY OPTIONS.
- CARDS E - FUNCTIONS DEFINING FORCE-DEFLECTIONS, INERTIAL SPIKE,  
ENERGY ABSORPTION FACTOR, AND FRICTION COEFFICIENTS.
- CARDS F - ALLOWED CONTACTS AMONG SEGMENTS, PLANES, BELTS, AIR BAGS  
AND CONTACT ELLIPSOIDS.
- CARDS G - INITIAL ORIENTATIONS AND VELOCITIES OF THE SEGMENTS.
- CARDS H - CONTROL OF OUTPUT OF TIME HISTORY OF SELECTED SEGMENT  
MOTIONS AND JOINT PARAMETERS.



A. MAIN PROGRAM INPUT

CARD A.1.A                      FORMAT (3A4,2I4,F8.0)

DATE(1),I=1,3                  DATE OF THE RUN (12 CHARACTERS).

IRSIN                            RESTART INPUT UNIT NO. IF BLANK OR ZERO,  
ALL INPUT TO BE SUPPLIED ON CARDS A.3 TO  
CARDS H.7. IF NONZERO (SUGGESTED VALUE =4)  
INPUT WILL BE SUPPLIED FROM A PREVIOUS  
RESTART TAPE AND CARDS A.1.B,C AND A.2.

IRSOUT                           RESTART OUTPUT UNIT NO. IF NONZERO (SUGGESTED  
VALUE =3) RECORDS WILL BE WRITTEN ON THIS  
OUTPUT UNIT FOR FUTURE RESTART RUNS. AN  
INITIAL RECORD CONTAINING ALL INPUT AND  
INITIALIZATION DATA WILL BE WRITTEN PLUS A  
TIME POINT RECORD AT EVERY TIME INTERVAL AS  
SPECIFIED BY DT ON CARD A.4.

RSTIME                           RESTART TIME (SEC.) REQUIRED IF IRSIN # 0.  
SHOULD BE NONZERO AND AN INTEGER MULTIPLE  
OF DT ON CARD A.4. PROGRAM WILL READ RECORDS  
FROM THE PREVIOUS RESTART TAPE UP TO AND  
INCLUDING THIS TIME, MAKE CHANGES PER CARD  
A.2 AND CONTINUE OPERATION FROM THERE.

CARDS A.1.B - A.1.C              FORMAT (20A4/20A4)

COMENT(1),I=1,40                DESCRIPTION OF THE RUN (160 CHARACTERS ON  
TWO CARDS).

THESE CARDS REQUIRED ONLY IF IRSIN > 0 , IN WHICH CASE ALL OTHER INPUT AS SPECIFIED ON CARDS A.3 TO H.7 ARE BYPASSED. TWO SETS OF A.2 (EACH TERMINATED WITH A BLANK CARD) ARE REQUIRED. THE FIRST SET IS PROCESSED AFTER THE INITIAL INPUT RECORD IS READ FROM INPUT UNIT IRSIN AND, IF IRSOUT # 0, BEFORE THE INPUT RECORD IS WRITTEN ON OUTPUT UNIT IRSOUT. THE SECOND SET IS PROCESSED AFTER THE TIME POINT RECORD FOR TIME = RSTIME HAS BEEN READ AND, IF IRSOUT # 0, AFTER THE SAME RECORD IS WRITTEN ON OUTPUT UNIT IRSOUT, BUT BEFORE THE PROGRAM RESUMES OPERATION.

CARDS A.2.A - A.2.N      FORMAT(A8, 4I4, 2(F8.0, I8, A8) )

A.2.A	ALPHANUMERIC NAME (LEFT ADJUSTED IN FIELD) OF VARIABLE TO BE REDEFINED FOR RESTART. PROGRAM IS CAPABLE OF CHANGING ANY VARIABLE IN THE LABELED COMMON BLOCKS AS USED AFTER ALL INITIALIZATION HAS BEEN PERFORMED. THE USER SHOULD ASCERTAIN THAT CHANGING THIS VARIABLE IS VALID FOR THE PROGRAM.
INDEX(I), I=1,3	THE ARRAY INDICES, IF ANY, OF THE VARIABLE. MUST AGREE IN NUMBER AND THE VALUES MUST BE LESS THAN OR EQUAL TO THE DIMENSIONS OF THE VARIABLE. BLANK OR ZERO FOR NO DIMENSION.
I.2.A	SUPPLY 1,2 OR 3 TO INDICATE THAT THE NEW VALUE IS TO BE REAL(RR), INTEGER(II) OR ALPHANUMERIC(AA). MUST AGREE WITH THE TYPE OF THE VARIABLE WITHIN THE PROGRAM.
RR, II OR AA	NEW VALUE OF THE VARIABLE A.2.A TO BE SUPPLIED IN THE APPROPRIATE FIELD DETERMINED BY THE VALUE OF I.2.A.
RR.OLD, II.OLD OR AA.OLD	THE PREVIOUS VALUE OF THE VARIABLE A.2.A IN THE APPROPRIATE FIELD ACCORDING TO THE I.2.A VALUE. INTEGER OR ALPHANUMERIC DATA WILL BE TESTED EXACTLY, REAL DATA TO 5 SIGNIFICANT DIGITS. IF THE CURRENT VALUE IS DIFFERENT, THE PROGRAM WILL TERMINATE WITH AN ERROR MESSAGE. IF ZERO OR BLANK IS SUPPLIED, NO CHECK IS PERFORMED.

THESE A.2 CARDS WILL BE PROCESSED UNTIL A BLANK VALUE FOR A.2.A IS ENCOUNTERED. NO FURTHER INPUT IS REQUIRED.

CARD A.3	FORMAT (3A4, 3F12.0)
UNITL	UNIT OF LENGTH (4 CHARACTERS)
UNITM	UNIT OF FORCE (MASS) (4 CHARACTERS)
UNITT	UNIT OF TIME (4 CHARACTERS).

NOTE : UNITL, UNITM AND UNITT SHOULD CORRESPOND TO THE USER'S INPUTS. THROUGHOUT THIS DESCRIPTION, INCHES, POUNDS AND SECONDS (IN,LBS,SEC) ARE USED AS SAMPLE UNITS.

GRAVTY(I),I=1,3	THE X, Y AND Z COMPONENTS OF GRAVITY (IN/SEC**2).
-----------------	--

CARD A.4	FORMAT (2I4, 4F8.0)
NDINT	NUMBER OF ITERATIONS FOR FINAL CONVERGENCE TEST OF THE INTEGRATOR SUBROUTINE DINT (MINIMUM VALUE = 2, SUGGESTED VALUE = 4).
NSTEPS	NUMBER OF INTEGRATION STEPS (OR OUTPUT TIME POINTS) FOR THE INTEGRATOR ROUTINE. MAY BE ZERO TO OBTAIN INITIAL CONDITIONS.
DT	MAIN PROGRAM TIME INTERVAL FOR INTEGRATOR ROUTINE OUTPUT (SEC). TOTAL TIME OF RUN WILL BE NSTEPS*DT SECONDS WITH MAIN PROGRAM TAPE 1, PRINTER PLOT AND OPTIONAL OUTPUT PRODUCED EVERY DT SECONDS.
H0	INITIAL INTEGRATOR STEP SIZE (SEC).
HMAX	MAXIMUM INTEGRATOR STEP SIZE (SEC). FOR BEST EFFICIENCY DT SHOULD BE AN INTEGRAL MULTIPLE OF HMAX AND HMAX A POWER OF TWO MULTIPLE OF H0. (SUGGESTED VALUE = 0.001 SEC.)
HMIN	MINIMUM INTEGRATOR STEP SIZE (SEC). IF A FIXED STEP SIZE IS DESIRED, SET HMIN GREATER THAN HMAX, AND STEP SIZE WILL DOUBLE FROM H0 UNTIL HMAX IS ACHIEVED.

NPRT(I),I=1,40

AN ARRAY OF INDICATORS THAT CONTROL VARIOUS OPTIONAL DIAGNOSTIC OUTPUT FOR THE PROGRAM. A VALUE OF ZERO OR BLANK INDICATES NO OUTPUT FOR THAT PARTICULAR ITEM. IN GENERAL, A VALUE OF 1 MEANS THAT THE OUTPUT WILL BE PRODUCED EVERY TIME A PARTICULAR SUBROUTINE IS EXECUTED. HOWEVER, FOR ELEMENTS 1-6 THE VALUE INDICATES THE PRINT FREQUENCY, E.G., A VALUE OF 5 WILL PRODUCE OUTPUT EVERY 5TH EXECUTION OF THE SUBROUTINE. OUTPUT PRODUCED BY ELEMENTS 7-26 IS INTENDED FOR DIAGNOSTIC OR "CHECK OUT" PURPOSES AND IS NOT COMPLETELY LABELED. THE USER SHOULD CONSULT THE LISTING OF THE SUBROUTINE FOR A DESCRIPTION OF THE VARIABLES THAT ARE PRINTED.

## THE NPRT ARRAY

ELEMENT NO.	SUBROUTINE	OUTPUT PRODUCED
1	MAIN	TAPE 1 OUTPUT
2	MAIN	ELTIME OUTPUT
3	MAIN	SUBROUTINE PRINT OUTPUT
4	NOT USED	
5	PRIPLT	Y-Z VIEW PRINTER PLOT
6	PRIPLT	X-Z VIEW PRINTER PLOT
7	BINPUT	HA, HB
8*	DAUX	IJK,RHS,C ARRAYS
9	DAUX	SUBROUTINE PRINT OUTPUT
10	IMPULS	DIAGNOSTIC OUTPUT
11	SETUP1	U2,V1 ARRAYS
12	VISPR	DIAGNOSTIC OUTPUT
13	PRIPLT	CJOINT ARRAY
14	WINDY	WIND FORCES
15	BELTG	DIAGNOSTIC OUTPUT
16	HBELT	HARNESS-BELT FORCES
17	EDEPTH	DIAGNOSTIC OUTPUT
18	NOT USED	
19	NOT USED	
20	CHAIN	XCOMP,XVCOMP,SEGLP,SEGLV
21	AIRBAG	DIAGNOSTIC OUTPUT
22	AIRBG1	DIAGNOSTIC OUTPUT
23	AIRBG3	DIAGNOSTIC OUTPUT
24	UPDATE	ROLL-SLIDE TEST OUTPUT
25	DINT	CONVERGENCE TEST DATA
26	DINT	SUBROUTINE OUTPUT EVERY STEP

\* A VALUE OF NPRT(8) = 2 WILL PRINT ARRAYS BEFORE AND AFTER THE FIRST CALL TO SUBROUTINE FSMSOL ONLY.

B. SUBROUTINE BINPUT

CARD B.1                      FORMAT (2I6, 8X, 5A4)

NSEG                          THE NUMBER OF SEGMENTS (MAXIMUM = 20).  
NOTE: THE VEHICLE AND GROUND WILL BE ASSIGNED  
SEGMENT NUMBERS NSEG+1 AND NSEG+2.

NJNT                          THE NUMBER OF JOINTS (MAXIMUM = 21).  
NOTE: NORMALLY NJNT = NSEG-1, BUT JOINT  
NUMBERS NSEG AND NSEG+1 MAY BE USED TO  
CONNECT THE VEHICLE AND THE GROUND TO  
LOWER NUMBERED SEGMENTS.

BDYTTL(I),I=1,5              DESCRIPTION OF THE CRASH VICTIM  
(20 CHARACTERS).

CARDS B.2.A - B.2.I          FORMAT (A4, 1X, A1, 10F6.0)  
(NSEG CARDS)

EACH CARD (I) FOR I = 1, NSEG WILL CONTAIN INPUT DATA FOR THE ITH  
SEGMENT. THE SEGMENT IDENTIFYING NUMBERS (I) WILL BE REFERRED TO  
ON LATER INPUT CARDS.

SEG(I)                        AN ABBREVIATION OF THE NOMENCLATURE  
OF THE ITH SEGMENT (4 CHARACTERS).

CGS(I)                        THE PLOT SYMBOL OF THE SEGMENT C.G.  
(1 CHARACTER).

W(I)                          THE WEIGHT OF THE SEGMENT (LBS).

PHI(J,I),J=1,3              THE PRINCIPAL MOMENTS OF INERTIA OF THE  
SEGMENT ABOUT THE X, Y, AND Z  
AXES OF THE SEGMENT (LBS-SEC\*\*2-IN).  
THERE ARE NO RESTRICTIONS ON THE VALUES OF  
W(I) OR PHI(J,I), THEY MAY BE NEGATIVE OR  
ZERO. IF ANY COMPONENT IS ZERO, IT IS  
ASSUMED THAT THE SYSTEM IS SUITABLY CON-  
STRAINED SO THAT THE SYSTEM MATRIX IS NON-  
SINGULAR.

BD(J,I),J=1,3                THE X, Y, AND Z SEMIAXES OF THE  
SEGMENT CONTACT ELLIPSOID (IN).

BD(J,I),J=4,6                THE LOCATION OF THE CENTER OF THE SEGMENT  
CONTACT ELLIPSOID, WITH RESPECT TO THE  
CENTER OF GRAVITY OF THE SEGMENT, IN THE  
LOCAL BODY SEGMENT REFERENCE(IN). THESE  
PRIMARY CONTACT ELLIPSOIDS ARE GIVEN THE  
SAME IDENTIFYING NUMBER AS THE SEGMENT.  
THEY MAY BE REDEFINED WITH AN ARBITRARY  
ORIENTATION ON CARDS D.5.



CARDS B.3.A - B.3.J      FORMAT (A4, 1X, A1, 2I4, 6F6.0/ 14X, 6F6.0)  
 (2\*NJNT CARDS - 2 CARDS FOR EACH JOINT)

EACH CARD (J) FOR J = 1, NJNT WILL CONTAIN INPUT DATA FOR THE JTH JOINT. THE JOINT IDENTIFYING NUMBERS (J) WILL BE REFERRED TO ON LATER INPUT CARDS.

JOINT(J)                    AN ABBREVIATION OF THE NOMENCLATURE OF THE JTH JOINT (4 CHARACTERS).

JS(J)                      PLOT SYMBOL OF THE JOINT LOCATION (1 CHARACTER).

JNT(J)                    MAGNITUDE INDICATES THE NUMBER OF THE SEGMENT THAT IS CONNECTED TO SEGMENT J+1 BY JOINT J. IF NEGATIVE, JOINT J IS ASSOCIATED WITH A FLEXIBLE ELEMENT. IF ZERO, SEGMENT J+1 IS THE REFERENCE SEGMENT OF ANOTHER BODY. (|JNT(J)| < J+1).

IPIN(J)                    0 - THERE ARE TO BE NO CONSTRAINTS ON JOINT J.  
                              1 - JOINT J IS PINNED (HINGE).  
                              2 - JOINT J IS NOT PINNED (BALL AND SOCKET).  
                              4 - JOINT J IS AN EULER JOINT.  
                              NON-ZERO VALUES FOR IPIN MAY BE SUPPLIED AS POSITIVE OR NEGATIVE TO INDICATE THAT THE INITIAL CONDITION OF THE JOINT IS UNLOCKED (POSITIVE) OR UNLOCKED (NEGATIVE).  
                              THE INITIAL STATE OF AN EULER JOINT IS SET BY USE OF IPIN AS FOLLOWS

IPIN	IEULER	STATE
4	8	FREE
- 4	7	ALL AXES LOCKED
- 5	6	SPIN                FREE, OTHERS LOCKED
- 6	5	NUTATION        FREE, OTHERS LOCKED
- 7	4	PRECESSION     FREE, OTHERS LOCKED
- 8	3	SPIN                LOCKED, OTHERS FREE
- 9	2	NUTATION        LOCKED, OTHERS FREE
-10	1	PRECESSION     LOCKED, OTHERS FREE

( PRECESSION    ABOUT Z  
   NUTATION        ABOUT RESULTANT X  
   SPIN             ABOUT RESULTANT Z )  
 IF IPIN IS LESS THAN -3 PROGRAM WILL SET IEULER AS ABOVE AND THEN SET IPIN = -4.

SR(I,2\*J-1),I=1,3      COORDINATES OF LOCATION OF JOINT J (IN.) IN THE LOCAL REFERENCE SYSTEM OF SEGMENT JNT(J).

SR(I,2\*J),I=1,3        COORDINATES OF LOCATION OF JOINT J (IN.) IN THE LOCAL REFERENCE SYSTEM OF SEGMENT J+1.

FOLLOWING DATA IS ON 2ND CARD FOR EACH JOINT.

YPR1(I,J),I=1,3      THE YAW, PITCH AND ROLL ANGLES (DEGREES)  
SPECIFYING THE PRINCIPAL AXES OF JOINT J IN  
THE LOCAL REFERENCE SYSTEM OF SEGMENT JNT(J).  
YAW    ABOUT Z AXIS  
PITCH ABOUT RESULTANT Y AXIS  
ROLL   ABOUT RESULTANT X AXIS

YPR2(I,J),I=1,3      THE YAW, PITCH AND ROLL ANGLES (DEGREES)  
SPECIFYING THE PRINCIPAL AXES OF JOINT J IN  
THE LOCAL REFERENCE SYSTEM OF SEGMENT J+1.  
THE Z AXIS IS THE REFERENCE AXIS TO DEFINE  
FLEXURE. THE Y AXIS IS USED AS THE PIN AXIS  
EXCEPT FOR THE SPECIAL EULER JOINTS. THE XY  
PLANE IS USED FOR GLOBALGRAPHIC JOINTS WITH  
X AS THE REFERENCE AXIS.

CARDS B.4.A - B.4.J      FORMAT (2 (4F6.0, F12.0))  
 (NJNT SETS OF CARDS, ONE FOR EACH JOINT J. IF |IPIN(J)| # 4,  
 EACH SET READS VALUES FOR 3\*J-2 AND 3\*J-1 ON ONE CARD ONLY.  
 IF |IPIN(J)| = 4 , JOINT J IS AN EULER JOINT AND A SECOND CARD  
 IS NECESSARY TO READ VALUES FOR 3\*J)

SPRING(I,3\*J-2),      THE FLEXURAL SPRING CHARACTERISTICS FOR  
                   I=1,5      JOINT J. IF J IS AN EULER JOINT, THE SPRING  
                                  CHARACTERISTICS ABOUT THE PRECESSION AXIS.  
                                  IF JOINTF(J) # 0 (ON CARD F.5.A), THESE  
                                  VALUES ARE NOT USED AND SHOULD BE ZERO.

SPRING(I,3\*J-1),      THE TORSIONAL SPRING CHARACTERISTICS FOR  
                   I=1,5      JOINT J. IF J IS AN EULER JOINT, THE SPRING  
                                  CHARACTERISTICS ABOUT THE NUTATION AXIS.

SPRING(I,3\*J),      SECOND CARD OF EACH SET IS REQUIRED  
                   I=1,5      ONLY IF J IS AN EULER JOINT, THE SPRING  
                                  CHARACTERISTICS ABOUT THE SPIN AXIS.

I=1      LINEAR SPRING COEFFICIENT  
                   (IN-LBS/DEG).

I=2      QUADRATIC SPRING COEFFICIENT  
                   (IN-LBS/DEG\*\*2).

I=3      CUBIC SPRING COEFFICIENT  
                   (IN-LBS/DEG\*\*3).

I=4      ENERGY DISSIPATION COEFFICIENT  
                   (DIMENSIONLESS).  
                   A VALUE OF 1. SPECIFIES NO LOSS  
                   A VALUE OF 0. SPECIFIES MAXIMUM LOSS

I=5      JOINT STOP LOCATION WITH RESPECT TO  
                   THE CENTER OF SYMMETRY (DEG).  
                   FOR A VALUE OF ZERO THE ROUTINE WILL USE ONLY  
                   THE LINEAR SPRING COEFFICIENT AND WILL APPLY  
                   THE ENERGY DISSIPATION FACTOR



CARDS B.5.A - B.5.J      FORMAT( 5F6.0, 18X, 2F6.0)  
 (NJNT SETS OF CARDS, ONE FOR EACH JOINT J. IF |IPIN(J)| # 4,  
 VALUES FOR 3\*J-2 ARE ON ONE CARD ONLY. IF |IPIN(J)| = 4,  
 J IS AN EULER JOINT AND VALUES FOR 3\*J-1 AND 3\*J ARE REQUIRED  
 ON A SECOND AND THIRD CARD OF EACH SET.)

VISC(I,3\*J-2),      THE VISCOUS CHARACTERISTICS FOR JOINT J.  
                   I=1,7      IF J IS AN EULER JOINT, THE VISCOUS CHAR-  
                                   ACTERISTICS ABOUT THE PRECESSION AXIS.

VISC(I,3\*J-1),      THE SECOND CARD OF EACH SET IS REQUIRED  
                   I=1,7      ONLY IF J IS AN EULER JOINT, THE VISCOUS  
                                   CHARACTERISTICS ABOUT THE NUTATION AXIS.

VISC(I,3\*J)      THE THIRD CARD OF EACH SET IS REQUIRED  
                   I=1,7      ONLY IF J IS AN EULER JOINT, THE VISCOUS  
                                   CHARACTERISTICS ABOUT THE SPIN AXIS.

I=1      VISCOUS COEFFICIENT (IN-LB-SEC/DEG).

I=2      COULOMB FRICTION COEFFICIENT (IN-LB).

I=3      RELATIVE ANGULAR VELOCITY OF JOINT  
                   AT WHICH FULL COULOMB FRICTION IS  
                   APPLIED (DEG/SEC). MUST BE GREATER THAN 0.

I=4      T1: THE MAXIMUM TORQUE (IN-LBS) ALLOWED FOR A  
                   LOCKED JOINT (OR EULER AXIS). IF EXCEEDED, THE  
                   JOINT WILL UNLOCK. IF T1 = 0, THE TEST WILL  
                   NOT BE PERFORMED.

I=5      T2: THE MINIMUM TORQUE (IN-LBS)  
                   ALLOWED FOR JOINT J TO REMAIN UNLOCKED.  
                   IF T2 = 0, THE TEST WILL NOT BE PERFORMED.

I=6      T3: THE MINIMUM ANGULAR VELOCITY (RAD/SEC)  
                   NECESSARY FOR JOINT J TO REMAIN UNLOCKED.  
                   IF T3 = 0, THE TEST WILL NOT BE PERFORMED.

I=7       $E = (1+U)/2$  WHERE U IS THE CLASSICAL  
                   COEFFICIENT OF RESTITUTION TO BE USED FOR THE  
                   IMPULSE OPTION IF THE JOINT HITS THE JOINT  
                   STOP ( $0 < E < 1$  OR  $-1 < U < +1$ ). A VALUE OF  $E = 0$   
                   MEANS THAT THE IMPULSE OPTION WILL NOT BE  
                   EXERCISED FOR THIS JOINT.

CARDS B.6.A - B.6.I  
(NSEG CARDS)

FORMAT (12F6.0)

SGTEST(1,1,I)	MAGNITUDE TEST FOR THE ANGULAR VELOCITY OF SEGMENT NO. I (RAD/SEC).
SGTEST(2,1,I)	ABSOLUTE ERROR TEST FOR THE ANGULAR VELOCITY OF SEGMENT NO. I (RAD/SEC).
SGTEST(3,1,I)	RELATIVE ERROR TEST FOR THE ANGULAR VELOCITY OF SEGMENT NO. I (DIMENSIONLESS).
SGTEST(1,2,I) (2,2,I) (3,2,I)	SAME AS ABOVE, BUT FOR THE LINEAR VELOCITY OF SEGMENT NO. I (IN/SEC).
SGTEST(1,3,I) (2,3,I) (3,3,I)	SAME AS ABOVE, BUT FOR THE ANGULAR ACCELERATION OF SEGMENT NO. I (RAD/SEC**2).
SGTEST(1,4,I) (2,4,I) (3,4,I)	SAME AS ABOVE BUT FOR THE LINEAR ACCELERATION OF SEGMENT NO. I (IN/SEC**2).

THESE CONVERGENCE TESTS ARE PERFORMED IN SUBROUTINE DINT ON THE RESULTANT OF THE DERIVATIVE VECTORS. THE LINEAR VELOCITIES AND ACCELERATIONS ARE COMPUTED ONLY FOR REFERENCE SEGMENTS (I.E. SEGMENT NO. 1 AND THOSE SEGMENTS I WHERE JNT(I-1) = 0), THEREFORE ANY TEST NUMBERS SUPPLIED FOR LINEAR VELOCITIES AND ACCELERATIONS OF OTHER SEGMENTS WILL BE IGNORED. THE TESTS FOR CONVERGENCE ARE PERFORMED IN THE FOLLOWING ORDER :

- 1) IF THE MAGNITUDE TEST IS ZERO, NO TESTING IS DONE FOR THAT VARIABLE.
- 2) IF THE MAGNITUDE OF THE RESULTANT VECTOR IS LESS THAN THE MAGNITUDE TEST, THE ROUTINE HAS PASSED THE CONVERGENCE TEST FOR THAT VARIABLE.
- 3) IF THE ABSOLUTE ERROR TEST IS GREATER THAN ZERO, AND THE MAGNITUDE OF THE ABSOLUTE ERROR (DIFFERENCE BETWEEN THE PREDICTED AND COMPUTED VECTOR) IS LESS THAN THE ABSOLUTE ERROR TEST, THE ROUTINE HAS PASSED THE CONVERGENCE TEST FOR THAT VARIABLE.
- 4) IF THE RELATIVE ERROR OF THE MAGNITUDE OF THE ABSOLUTE ERROR COMPARED TO THE MAGNITUDE OF THE COMPUTED VECTOR IS GREATER THAN THE RELATIVE ERROR TEST, THE CONVERGENCE TEST HAS FAILED.

IF NFLX # 0, CARDS B.7 ARE REQUIRED. EACH FLEXIBLE ELEMENT AS DEFINED ON CARDS B.3 CONTAINS AT LEAST THREE CONNECTED SEGMENTS CONSISTING OF A REFERENCE SEGMENT, ONE OR MORE INTERIOR SEGMENTS AND A TERMINATING SEGMENT. EACH JOINT IN THE ELEMENT SHOULD HAVE A NEGATIVE VALUE FOR JNT, AND THE NUMBER OF INTERIOR SEGMENTS WILL BE ONE LESS THAN THE NUMBER OF NEGATIVE VALUES OF JNT FOR EACH ELEMENT. NFLX IS THE TOTAL NUMBER OF INTERIOR SEGMENTS OF ALL FLEXIBLE ELEMENTS.

CARD B.7.A                      FORMAT (18I4)

NFX                              THE NUMBER OF INTERIOR SEGMENTS FOR WHICH HF ARRAYS ARE TO BE SUPPLIED.

KNT(K),K=1,NFX                THE INTERIOR SEGMENT IDENTIFICATION NUMBERS IN THE ORDER OF THE HF ARRAYS TO BE SUPPLIED. IF THE VALUES OF NFX AND KNT ARE NOT CONSISTENT WITH THE NEGATIVE VALUES OF JNT ON CARDS B.3 THE PROGRAM WILL TERMINATE WITH AN APPROPRIATE ERROR MESSAGE.

CARDS B.7.B - B.7.N        FORMAT (12F6.0 )  
(4\*NFX CARDS, 4 CARDS FOR EACH SEGMENT IN THE ORDER AS THEY ARE DEFINED IN THE KNT VECTOR.)

(HF(I,J,K),J=1,12)        THE COEFFICIENTS OF THE QUADRATIC FORM  
                              ,I=1,4        FUNCTION USED TO DEFINE THE ORIENTATION OF INTERIOR SEGMENT KNT(K) WITH RESPECT TO REFERENCE SEGMENT OF THE ELEMENT.

FORM THE COLUMN VECTOR V WITH FOUR COMPONENTS Y,P,R AND 1, WHERE Y,P,R ARE THE YAW, PITCH AND ROLL OF THE TERMINATING SEGMENT RELATIVE TO THE REFERENCE SEGMENT. LET H BE A SYMMETRIC 4X4 MATRIX SUCH THAT  $F(V) = 1/2 V \cdot H V$  REPRESENTS A QUADRATIC SCALAR FUNCTION OF THE VARIABLES Y,P AND R IN RADIAN. THUS

YAW OF SEGMENT KNT(K) =  $1/2 V \cdot HF(I,J,K) V$   
PITCH OF SEGMENT KNT(K) =  $1/2 V \cdot HF(I,J+4,K) V$   
ROLL OF SEGMENT KNT(K) =  $1/2 V \cdot HF(I,J+8,K) V$         (I,J=1,4)

C. SUBROUTINE VINPUT

CARD C.1

FORMAT (20A4)

VPSTTL(I),I=1,20

DESCRIPTION OF THE CRASH VEHICLE DECELERATION  
(80 CHARACTERS).

CARD C.2

FORMAT (8F6.0, I6, 2F6.0)

ANGLE(I),I=1,3

FOR THE HALF SINE-WAVE DECELERATION  
(NATAB = 0) OR FOR THE UNIDIRECTIONAL  
DECELERATION TABULAR INPUT (NATAB > 0),  
ANGLE(1) AND ANGLE(2) REPRESENT THE  
AZIMUTH AND ELEVATION (OBLIQUE ANGLES)  
OF THE DIRECTION OF THE DECELERATION  
IMPULSE (DEG). ANGLE(3) IS NOT USED  
AND THE INITIAL YAW, PITCH AND ROLL  
OF THE VEHICLE ARE ASSUMED TO BE ZERO.  
FOR THE OMNIDIRECTIONAL TABULAR INPUT  
(NATAB < 0). THEY REPRESENT THE INITIAL  
YAW, PITCH AND ROLL OF THE VEHICLE (DEG).

VIPS

THE INITIAL VELOCITY OF THE CRASH VEHICLE.  
(IN/SEC - UNITS AS SPECIFIED ON CARD A.3)  
A NEGATIVE VALUE MAY BE SUPPLIED FOR NATAB=0  
TO INDICATE THAT THE VEHICLE WILL ACCELERATE  
FROM A VELOCITY OF ZERO TO |VIPS|.

VTIME

THE TIME DURATION OF THE DECELERATION  
IMPULSE (SEC). REQUIRED ONLY IF NATAB = 0.  
A VALUE OF ZERO IS NOT PERMITTED IF NATAB=0.

XO(I),I=1,3

THE INITIAL X, Y, AND Z COORDINATES  
OF THE VEHICLE REFERENCE ORIGIN IN  
INERTIAL REFERENCE (IN).

NATAB

INTEGER NUMBER OF TIME POINTS FOR WHICH  
VEHICLE DECELERATION DATA IS TO BE SUPPLIED.  
THE ALGEBRAIC SIGN OF NATAB DETERMINES THE  
TYPE OF VEHICLE MOTION AS FOLLOWS:

IF NATAB = 0, THE DIRECTION IMPULSE IS AN  
ANALYTICAL HALF-SINE WAVE FUNCTION THAT  
DECELERATES THE VEHICLE FROM AN INITIAL  
SPEED OF VMPH TO ZERO IN VTIME SECONDS.

IF NATAB > 0, THE VEHICLE MOTION IS  
UNIDIRECTIONAL AND ONLY THE RESULTANT LINEAR  
DECELERATION IS INPUTTED IN TABULAR FORM ON  
CARDS C.3. (NATAB SHOULD BE ODD AND MAXIMUM  
VALUE IS 99.)

IF NATAB < 0, THE VEHICLE MOTION IS ALSO  
ROTATIONAL, AND THE COMPONENTS OF BOTH  
LINEAR AND ANGULAR ACCELERATION ARE INPUTTED  
IN TABULAR FORM ON CARDS C.4. (MINIMUM  
VALUE OF NATAB IS -100.)



ATO THE BEGINNING TIME POINT FOR THE  
DECELERATION TABLE INPUT (SEC).

ADT FIXED TIME INTERVAL FOR THE DECELERATION  
TABLE INPUT (SEC).

CARDS C.3.A - C.3.N FORMAT (12F6.0)

THESE CARDS ARE REQUIRED ONLY IF NATAB > 0.

ATAB(1,I), I=1,NATAB THE NATAB VALUES OF DECELERATION  
(G'S) FOR THE CRASH VEHICLE  
FOR FIXED TIME INTERVALS

$T(I) = ATO + (I-1)*ADT$  FOR  $I=1,NATAB$ .

SUPPLY 12 VALUES PER CARD, USE AS MANY CARDS  
AS NECESSARY. SINCE A SIMPSON'S INTEGRATION  
IS USED TO COMPUTE VELOCITY AND POSITION,  
THE VALUE OF NATAB MUST BE ODD. THE LAST  
VALUE, ATAB(1,NATAB) WILL BE USED TO INTEGRATE  
FOR ANY TIME GREATER THAN  $T(NATAB-1)$ .

CARDS C.4.A - C.4.M FORMAT (10X, 6F10.0)

MATAB CARDS ARE REQUIRED ONLY IF NATAB < 0 (MATAB = -NATAB)

EACH CARD (I) WILL CONTAIN THE LINEAR AND ANGULAR ACCELERATIONS  
FOR TIME  $T(I) = ATO + (I-1)*ADT$  FOR  $I = 1,MATAB$ .

ATAB(J,I), J=1,3 THE VALUES OF THE X,Y AND Z COMPONENTS OF  
LINEAR DECELERATION (G'S) FOR TIME POINT  
 $T(I)$ . THE PROGRAM WILL INTEGRATE FOR VELOCITY  
AND POSITION BEYOND THE LAST TIME POINT  
USING THE LAST VALUES SUPPLIED.

ATAB(J,I), J=4,6 THE VALUES OF THE COMPONENTS OF ANGULAR  
ACCELERATION (DEG/SEC\*\*2) FOR TIME POINT(I).  
THE VALUES FOR THE LAST TIME POINT MUST BE  
ZERO WHICH IS ASSUMED BY PROGRAM FOR  
INTEGRATING BEYOND THE LAST TIME POINT.

D. SUBROUTINE SINPUT

CARD D.1	FORMAT (6I6)
NPL	THE NUMBER OF PLANES DESCRIBING A CONTACT PANEL OF THE VEHICLE (20 MAXIMUM).
NBLT	THE NUMBER OF BELTS USED TO RESTRAIN THE CRASH VICTIM (8 MAXIMUM).
NBAG	THE NUMBER OF AIR BAGS USED TO RESTRAIN THE CRASH VICTIM (5 MAXIMUM).
NELP	THE NUMBER OF CONTACT ELLIPSOIDS TO BE SUPPLIED ON CARDS D.5.
NQ	THE NUMBER OF CONSTRAINTS TO BE SUPPLIED ON CARDS D.6. EACH CONSTRAINT TYPE 5 WILL BE CONSIDERED AS TWO CONSTRAINTS REQUIRING TWO SETS OF CARDS (NOTE: THE PROGRAM WILL LATER INCREMENT NQ BY 1 FOR EACH NF(1) = 0 ON CARDS F.1.B AND F.3.B AND THE FINAL MAXIMUM ON NQ IS 12).
NSD	THE NUMBER OF SPRING DAMPERS TO BE SUPPLIED ON CARDS D.8 (20 MAXIMUM).

IF NPL # 0, NPL SETS OF D.2 ARE REQUIRED.

CARD D.2.A                      FORMAT (I4, 4X, 5A4)

J                      THE NUMBER IDENTIFYING THE PLANE,  
MUST BE INPUTTED AS SUCCESSIVE  
INTEGERS 1, 2, 3, ..., NPL.

PLTTL(I,J),I=1,5      A 20 CHARACTER DESCRIPTION OF THE  
JTH PANEL.

CARDS D.2.B - D.2.D          FORMAT (3F12.0)

P1(I),I=1,3            THE X,Y AND Z COORDINATES OF POINT P1 IN  
VEHICLE (OR SEGMENT TO WHICH PLANE IS  
ATTACHED) REFERENCE (IN).

P2(I),I=1,3            THE X,Y AND Z COORDINATES OF POINT P2 IN  
VEHICLE (OR SEGMENT TO WHICH PLANE IS  
ATTACHED) REFERENCE (IN).

P3(I),I=1,3            THE X,Y AND Z COORDINATES OF POINT P3 IN  
VEHICLE (OR SEGMENT TO WHICH PLANE IS  
ATTACHED) REFERENCE (IN).

WHERE P1, P2, AND P3 ARE 3 OF THE CORNERS OF A BOUNDED RECTANGULAR PLANE  
SUCH THAT THE EDGE P1P2 IS 90 DEGREES CLOCKWISE (AS VIEWED FROM THE  
EXTERNAL SURFACE) FROM THE EDGE P1P3.



IF NBLT # 0, NBLT SETS OF D.3 ARE REQUIRED.

CARD D.3.A

FORMAT (5A4)

BLTTTL(I,J),I=1,5      A 20 CHARACTER DESCRIPTION OF THE  
JTH BELT.

CARD D.3.B

FORMAT (6F12.0)

BELT(I,J),I=1,3      X,Y, AND Z COORDINATES, IN VEHICLE (OR SEGMENT  
TO WHICH BELT IS ANCHORED) REFERENCE, OF  
ANCHOR POINT A FOR THE JTH BELT (IN).

BELT(I,J),I=4,6      X,Y, AND Z COORDINATES, IN VEHICLE (OR SEGMENT  
TO WHICH BELT IS ANCHORED) REFERENCE, OF  
ANCHOR POINT B FOR THE JTH BELT (IN).

NOTE: THE PROGRAM MUST PASS A PLANE THROUGH THE THREE POINTS, ANCHOR  
POINT A, ANCHOR POINT B, AND A FIXED POINT ON THE CONTACTED BODY SEGMENT.  
IF ANCHOR POINTS A AND B COINCIDE, THEY MUST BE SEPARATED SLIGHTLY FOR  
INPUT SUCH THAT THE DESIRED BELT PLANE WILL BE DEFINED.

CARD D.3.C

FORMAT (5F12.0)

BELT(I,J),I=7,9      X, Y, AND Z COORDINATES, IN LOCAL BODY  
SEGMENT REFERENCE (BUT WITH RESPECT TO  
ELLIPSOID CENTER, NOT C.G.), OF THE  
FIXED CONTACT POINT ON THE BODY  
SEGMENT FOR THE JTH BELT (IN).

BELT(10,J)      CURRENTLY NOT USED BY THE PROGRAM.

BELT(11,J)      BELT SLACK (IN). THE SLACK, WHEN ADDED TO  
THE INITIAL GEOMETRIC LENGTH, RESULTS IN  
THE INITIAL BELT LENGTH. IF DESIRED, THE  
INITIAL BELT LENGTH MAY BE INPUTTED AS A  
NEGATIVE NUMBER AND THE PROGRAM WILL  
COMPUTE THE SLACK.

IF NBAG # 0, NBAG SETS OF D.4 ARE REQUIRED BY  
SUBROUTINE AIRBGI.

CARD D.4.A	FORMAT (5A4, I4)
BAGTTL(I,J), I=1,5	A 20 CHARACTER DESCRIPTION OF THE JTH AIR BAG.
NPANEL(J)	NUMBER OF VEHICLE CONTACT PANELS THAT ARE ALLOWED TO INTERACT WITH THE JTH AIR BAG (MAXIMUM = 4).
CARD D.4.B	FORMAT(6F12.0)
AB(I,J), I=1,3	THE X, Y AND Z SEMIAXES OF THE JTH AIR BAG WHEN FULLY INFLATED AND UNDEFORMED (IN).
BFA(I,J), I=1,3	THE X,Y AND Z COORDINATES OF THE CENTER OF THE AIR BAG CONTACT ELLIPSOID WITH RESPECT TO THE AIR BAG CENTER OF GRAVITY (IN).
CARD D.4.C	FORMAT (6F12.0)
YB,PB,RB	THE INITIAL ORIENTATION (YAW, PITCH, AND ROLL) OF THE JTH AIR BAG IN THE VEHICLE REFERENCE (DEG).
ZDEP(I,J), I=1,3	THE X, Y, AND Z COORDINATES OF THE DEPLOYMENT POINT OF THE JTH AIR BAG IN THE LOCAL REFERENCE OF THE 1ST PANEL ON CARD D.4.G (IN).
CARD D.4.D	FORMAT (6F12.0)
XBM(J)	WEIGHT OF AIR BAG MEMBRANE AND CONTENTS (LBS).
CYTD(J)	GAS SUPPLY ACTUATOR FIRING TIME AFTER THE START OF VEHICLE DECELERATION (SEC).
CYPA(J)	ATMOSPHERIC PRESSURE (PSIA).
CYSP(J)	INITIAL GAS SUPPLY PRESSURE (PSIG).
CYTO(J)	INITIAL GAS SUPPLY TEMPERATURE (DEG R).
CYVO(J)	GAS SUPPLY RESERVOIR VOLUME (IN**3).

## CARD D.4.E

FORMAT (6F12.0)

CYCD(J)

SONIC THROAT DISCHARGE COEFFICIENT  
(DIMENSIONLESS).

CYK(J)

RATIO OF SPECIFIC HEATS OF SUPPLY  
GAS (DIMENSIONLESS).

CYR(J)

SPECIFIC GAS CONSTANT (IN/DEG R).

CYAT(J)

SONIC THROAT AREA (IN\*\*2).

CYPV(J)

VENT PRESSURE OF THE EXHAUST  
ORIFICE (PSIG).

CYCDO(J)

EXHAUST ORIFICE DISCHARGE  
COEFFICIENT (DIMENSIONLESS).

## CARD D.4.F

FORMAT (5F12.0)

CYAO(J)

EXHAUST ORIFICE AREA (IN\*\*2).

SPRK(J)

SPRING CONSTANT OF A LINEAR SPRING  
USED TO SIMULATE ATTACHMENT OF THE  
BAG AT THE DEPLOYMENT POINT IN THE  
VEHICLE (LB/IN).

VSCS(J)

COEFFICIENT OF SLIDING FRICTION OF  
THE AIR BAG (DIMENSIONLESS)

CK(J)

PARAMETER USED TO STABILIZE AIR  
BAG NUMERICAL INTEGRATION (SEC\*\*-1).  
SUGGESTED VALUE = 250.

CMASS(J)

MULTIPLIER TO INCREASE OR DECREASE  
THE MASS OF THE AIR BAG TO ARTIFICIALLY  
DAMPEN THE INTEGRATED AIR BAG MOTION.

NPANEL(J) SETS OF THE FOLLOWING TWO CARDS ARE REQUIRED TO DEFINE THE ELLIPSOIDS USED TO APPROXIMATE THE CONTACT PANELS FOR THE JTH AIR BAG. THE FIRST PANEL IS THE REACTION PANEL.

CARD D.4.G

FORMAT (6F12.0)

B(I,K,J),I=1,3

X, Y, AND Z SEMIAXES FOR THE KTH PANEL FOR THE JTH AIR BAG (IN).

BFB(I,K,J),I=1,3

THE LOCATION OF THE CENTER OF THE PANEL ELLIPSOID WITH RESPECT TO ITS CENTER OF GRAVITY (IN).

CARD D.4.H

FORMAT (6F12.0)

ZR(I,K,J),I=1,3

X, Y, AND Z COORDINATES IN VEHICLE REFERENCE OF THE CENTER OF GRAVITY OF THE KTH PANEL OF THE JTH AIR BAG (IN).

YP,PP,RP

THE ORIENTATION, YAW, PITCH, AND ROLL OF THE KTH PANEL (DEG).

IF NEMP # 0, NEMP D.5 CARDS ARE REQUIRED BY SUBROUTINE SINPOT.

NOTE: NEMP IS THE NUMBER OF CONTACT ELLIPSOIDS TO BE SUPPLIED HERE, NOT THE NUMBER OF CONTACT ELLIPSOIDS IN THE PROGRAM. THE FIRST NSEG ELLIPSOIDS WERE SUPPLIED ON CARDS B.2.A - B.2.I WITH NO ANGULAR ROTATIONS. THEY MAY BE REPLACED HERE IF DESIRED.

CARDS D.5.A - D.5.J  
(NEMP CARDS)

FORMAT (I6, 9F6.0)

M

CONTACT ELLIPSOID NUMBER. MAX = 24. IF  
M < NSEG + 1, DATA WILL REPLACE INPUT SUPPLIED  
ON CARDS B.2.A - B.2.I.

P1(I), I=1,3

THE X, Y, AND Z SEMIAXES OF THE CONTACT  
ELLIPSOID (IN).

P2(I), I=1,3

THE X, Y, AND Z COORDINATES OF THE  
ELLIPSOID OFFSET FROM THE SEGMENT CENTER  
OF GRAVITY.

P3(I), I=1,3

THE YAW, PITCH AND ROLL (DEGREES) OF THE  
CONTACT ELLIPSOID FROM THE PRINCIPAL AXIS  
OF THE SEGMENT.

IF NQ # 0, NQ D.6 CARDS ARE REQUIRED BY SUBROUTINE SINPOT.

CARDS D.6.A - D.6.J  
(NQ CARDS)

FORMAT (3I6, 6F6.0)

KQTYPE(J)

TYPE NO. OF THE JTH CONSTRAINT

- 1: POINT SPECIFIED BY RK1 ON SEGMENT KQ1  
WILL BE CONSTRAINED TO BE THE SAME AS  
THE POINT SPECIFIED BY RK2 ON SEGMENT  
KQ2.
- 2: POINT SPECIFIED BY RK1 ON SEGMENT KQ1  
WILL BE CONSTRAINED TO REMAIN AT AN  
EQUAL DISTANCE ( $D > 0$ ) FROM THE POINT  
SPECIFIED BY RK2 ON SEGMENT KQ2.
- 5: TENSION ELEMENT CONSTRAINT CONNECTING  
POINT RK1 ON SEGMENT KQ1 TO POINT RK2  
ON SEGMENT RK2 (REQUIRES TWO CARDS WITH  
KQTYPE, KQ1 AND KQ2 THE SAME ON BOTH).

KQ1(J)

SEGMENT IDENTIFICATION NUMBER OF THE  
1ST SPECIFIED POINT.

KQ2(J)

SEGMENT IDENTIFICATION NUMBER OF THE  
2ND SPECIFIED POINT.

RK1(I,J),I=1,3

COORDINATES OF SPECIFIED POINT ON  
SEGMENT KQ1 (IN). IF KQTYPE = 5, THE SECOND  
CARD WILL CONTAIN THE EFFECTIVE MASSES MA,  
MB AND MAB (LB.SEC\*\*2/IN) IN PLACE OF RK1.

RK2(I,J),I=1,3

COORDINATES OF SPECIFIED POINT ON  
SEGMENT KQ2 (IN). IF KQTYPE = 5, THE SECOND  
CARD WILL CONTAIN THE SPRING CONSTANT K  
(LB/IN), THE VISCOUS DAMPING CONSTANT D  
(LB SEC/IN) AND THE REFERENCE LENGTH L (IN)  
IN PLACE OF RK2.



CARD D.7 IS ALWAYS REQUIRED. SUPPLY BLANK CARD FOR NORMAL 3D MOTION.

CARD D.7                      FORMAT (18I4)              IF NSEG>18, USE 2 CARDS.

NSYM(J),J=1,NSEG              CONTROLS SYMMETRY OPTION OF BODY SEGMENTS  
AS FOLLOWS :

NSYM(J) = 0 :              NORMAL THREE DIMENSIONAL MOTION FOR BODY  
SEGMENT J.

NSYM(J) = J :              MOTION OF BODY SEGMENT J WILL BE RESTRICTED  
TO THE X-Z PLANE WITH NO LATERAL MOTION,  
HENCE IT WILL BE TWO DIMENSIONAL.

NSYM(J) = K :              BODY SEGMENTS J AND K ARE TO REMAIN SYMMETRICAL  
WITH NO LATERAL MOTION. THE MOTION OF EACH WILL  
BE REPLACED WITH THEIR AVERAGE AND RESTRICTED  
TO THE LOCAL X-Z PLANE. NSYM(K) MUST EQUAL J.

NSYM(J) = -K :              BODY SEGMENTS J AND K ARE TO REMAIN MIRROR  
SYMMETRICAL WITH RESPECT TO THE X-Z PLANE.  
EQUAL BUT OPPOSITE LATERAL MOTION IS  
PERMITTED. NSYM(K) MUST EQUAL -J.

NOTE : IN THE ABOVE SYMMETRY OPTIONS, THE USER MUST TAKE EXTREME  
CARE THAT ALL INPUT WILL ALLOW THE SYMMETRY TO EXIST.

IF NSD # 0, NSD D.8 CARDS ARE REQUIRED BY SUBROUTINE SINPOT.

CARDS D.8.A - D.8.J              FORMAT (2I3, IIF6.0)  
(NSD CARDS)

MSDM(J)                      SEGMENT IDENTIFICATION NUMBERS (M AND N)  
MSDN(J)                      TO WHICH THE JTH SPRING DAMPER IS ATTACHED.

APSDM(I,J),I=1,3              COORDINATES OF ATTACHMENT POINTS IN LOCAL  
APSDN(I,J),I=1,3              SEGMENT REFERENCE ON SEGMENTS M AND N FOR  
THE JTH SPRING DAMPER (IN.)

ASD(I,J),I=1,5              COEFFICIENTS OF QUADRATIC FUNCTIONS TO  
I=1 : D0 (IN)              COMPUTE THE SPRING FORCE (FS) AND THE  
I=2 : A1 (LB/IN)              VISCOUS FORCE (FD) FOR THE JTH SPRING  
I=3 : A2 (LB/IN\*\*2)              DAMPER USING THE RELATIONSHIPS  
I=4 : B1 (LB SEC/IN)  
I=5 : B2 (LB SEC\*\*2/IN\*\*2)

$$FS = (D-D0) * (|A1| + A2 * |D-D0|)$$
$$FD = DV * (B1 + B2 * |DV|)$$

WHERE D AND DV ARE THE DISTANCE AND ITS TIME  
DERIVATIVE BETWEEN THE POINTS APSDM AND APSDN.  
IF A1 < 0. AND (D-D0) < 0.,  
PROGRAM WILL SET FS= 0., I.E. THIS WILL ACT AS  
TENSION ELEMENT.



# E. SUBROUTINE CINPUT (FUNCTIONS INPUT)

THESE FUNCTIONS ARE REFERRED TO BY NUMBER IN THE NF ARRAYS REQUIRED ON CARDS F.1.B, F.2.B, F.3.B AND F.4.B. THEY ARE USED TO DEFINE THE FORCE DEFLECTION, INERTIAL SPIKE, R (ENERGY ABSORPTION) FACTOR, G (DEFLECTION) FACTOR AND FRICTION COEFFICIENT FUNCTIONS.

EACH FUNCTION MAY BE SUBDIVIDED, IF DESIRED, INTO TWO SEPARATE PARTS, F1 AND F2, WHERE

F1(D) IS DEFINED FOR  $0 \leq D \leq D_1$

F2(D) IS DEFINED FOR  $|D_1| \leq D \leq |D_2|$ .

IN ADDITION, EACH PART OF EACH FUNCTION MAY BE DEFINED IN EITHER OF THREE FUNCTIONAL FORMS: CONSTANT VALUE, TABULAR DATA, OR A FIFTH DEGREE POLYNOMIAL. THE EXISTENCE AND FORM OF EACH FUNCTION PART IS DETERMINED BY THE SUPPLIED VALUES OF  $D_0$ ,  $D_1$ , AND  $D_2$  AS FOLLOWS:

F1	F2	$D_0$	$D_1$	$D_2$
—	—	—	—	—
CONSTANT	-	0	0	$F1 = D2$
TABULAR	-	$D_0 \geq 0$	$D_1 < 0$	0
POLYNOMIAL	-	$D_0 \geq 0$	$D_1 > 0$	0
TABULAR	POLYNOMIAL	$D_0 \geq 0$	$D_1 < 0$	$D_2 > 0$
POLYNOMIAL	TABULAR	$D_0 \geq 0$	$D_1 > 0$	$D_2 < 0$
POLYNOMIAL	POLYNOMIAL	$D_0 \geq 0$	$D_1 > 0$	$D_2 > 0$

THE CONSTANT FORM IS APPLICABLE TO F1 ONLY BECAUSE THE ROUTINES ASSUME

IF  $D > |D_2|$  THEN  $F(D) = F(|D_2|)$  FOR  $D_2 \neq 0$  OR

IF  $D > |D_1|$  THEN  $F(D) = F(|D_1|)$  FOR  $D_2 = 0$ .

THE CASE OF BOTH F1 AND F2 BEING TABULAR IS UNNECESSARY.

A MAXIMUM OF 50 FUNCTIONS MAY BE SUPPLIED TO THE PROGRAM. THESE FUNCTIONS MAY BE OF THE TYPES DESCRIBED ON EITHER CARDS E.1-E.4, CARDS E.6 OR CARDS E.7.

CARD E.1

I

FORMAT (I4, 4X, 5A4)

THE FUNCTION IDENTIFYING NUMBER. THESE NUMBERS NEED NOT BE SUPPLIED IN NUMERIC ORDER. IF THE SAME NUMBER IS USED MORE THAN ONCE, A WARNING WILL BE PRINTED AND THE LAST ONE SUPPLIED WILL BE USED. THE END OF THE FUNCTION INPUT IS INDICATED BY SUPPLYING A SINGLE CARD WITH I > 50.

KTITLE

A 20 CHARACTER ALPHANUMERIC  
TITLE DESCRIBING THE FUNCTION.

CARD E.2

FORMAT (5F12.0)

- D0 THE LOWER ABSCISSA VALUE OF THE FIRST PART OF THE FUNCTION, F1. D0 MUST BE NON-NEGATIVE (UNITS ARE IN. EXCEPT FOR THE BELT STRESS-STRAIN FUNCTIONS WHERE THEY ARE IN/IN).
- D1 THE MAGNITUDE OF D1 IS THE UPPER ABSCISSA VALUE OF F1 AND THE LOWER ABSCISSA VALUE OF F2, IF ANY.  $D1 < 0$  INDICATES F1 IS TABULAR,  $D1 > 0$  INDICATES F1 IS A POLYNOMIAL, AND  $D1 = 0$  INDICATES  $F1 = D2$ , A CONSTANT.
- D2 IF  $D1 = 0$ , D2 IS THE CONSTANT VALUE OF F1. OTHERWISE, THE MAGNITUDE OF D2 IS THE UPPER ABSCISSA VALUE OF F2. IF  $D2 = 0$ , F2 IS NOT DEFINED; IF D2 IS NEGATIVE, F2 IS TABULAR; AND IF D2 IS POSITIVE, F2 IS A POLYNOMIAL.
- D3 IF THE FUNCTION IS TO BE USED FOR AN INERTIAL SPIKE, D3 REPRESENTS THE ABSCISSA VALUE FOR WHICH THE INERTIAL SPIKE IS TO BE IGNORED IF UNLOADING OCCURS AFTER DEFLECTION EXCEEDS D3. IF THE FUNCTION IS TO BE USED FOR A COEFFICIENT OF FRICTION,  $D3 = (1+U)/2$  WHERE U IS THE COEFFICIENT OF RESTITUTION FOR THE IMPULSE OPTION ( $0 < D3 < 1$  OR  $-1 < U < +1$ ). A VALUE OF  $D3 = 0$  MEANS THAT THE IMPULSE OPTION WILL NOT BE USED FOR THOSE CONTACTS USING THIS FUNCTION. WHEN THE GLOBALGRAPHIC OPTION IS USED, A FRICTION FUNCTION IS DEFINED AND THE VALUE OF D3 IS USED TO SPECIFY THE IMPULSE. (SEE CARD B.5.)
- D4 IF THE FUNCTION IS TO BE USED AS A FORCE DEFLECTION FUNCTION BY SUBROUTINE PLELP,  $D4=RHO$ , THE SCALAR THAT DETERMINES THE POINT OF FORCE APPLICATION. SUPPLY ZERO FOR POINT OF MAXIMUM PENETRATION, ONE FOR CENTER OF INTERSECTION ELLIPSE. IF USED AS THE FRICTION FUNCTION FOR A ROLL-SLIDE CONSTRAINT, D4 IF THE COEFFICIENT OF STATIC FRICTION TO BE USED FOR THE ROLL CONSTRAINT.

THE DEFINITIONS OF F1 AND F2, IF THEY EXIST, ARE NOW SUPPLIED ON CARD E.3 FOR THE FIFTH DEGREE POLYNOMIAL DEFINITION, OR ON CARDS E.4 FOR THE TABULAR DEFINITION.

CARD E.3

FORMAT (6F12.0)

A0,A1,A2,A3,A4,A5

COEFFICIENTS OF FIFTH-DEGREE POLYNOMIAL

$$F = A0 + A1*X + A2*X**2 + A3*X**3 + A4*X**4 + A5*X**5$$

(UNITS ARE DEPENDENT ON USE OF FUNCTION.)

CARD E.4.A

FORMAT (I6)

NPI

THE NUMBER OF DATA POINTS TO BE SUPPLIED TO IDENTIFY THE FUNCTION IF IT IS DEFINED IN TABULAR FORM.

CARDS E.4.B - E.4.N

FORMAT (6F12.0)

(X(I),Y(I),I=1,NPI)

THE ABSCISSA AND ORDINATE VALUES OF THE DATA POINTS USED TO DEFINE THE TABULAR FORM OF THE FUNCTION. THE PROGRAM WILL LINEARLY INTERPOLATE TO DETERMINE INTERMEDIATE VALUES. SUPPLY 3 POINTS PER CARD; USE AS MANY CARDS AS REQUIRED. (UNITS ARE DEPENDENT ON USE OF FUNCTION.)

SUBROUTINE KINPUT (WIND FORCE AND JOINT RESTORING FORCE FUNCTIONS)

CARD E.5 IS ALWAYS REQUIRED AFTER THE END-OF-DATA CARD E.1 (I > 50).  
MAY BE BLANK TO DESIGNATE NO FUNCTIONS ON CARDS E.6 OR E.7.

CARD E.5                      FORMAT (2I6)

NWINDF                      THE NUMBER OF WIND FORCE FUNCTIONS TO BE  
                             SUPPLIED ON CARDS E.6.A-E.6.N. MAY BE ZERO.

NJNTF                      THE NUMBER OF JOINT RESTORING FORCE FUNCTIONS  
                             TO BE SUPPLIED ON CARDS E.7.A-E.7.N. MAY  
                             BE BLANK OR ZERO.

NWINDF SETS OF CARDS E.6.A - E.6.N ARE REQUIRED.

CARD E.6.A                      FORMAT (I4, 4X, 5A4)

I,KTITLE                      SAME AS CARD E.1 EXCEPT THAT EACH FUNCTION  
                             NUMBER (I) MUST BE LESS THAN 51 AND MUST BE  
                             DISTINCT FROM THOSE SUPPLIED ON CARDS E.1.

CARD E.6.B                      FORMAT (5F12.0)

DO,D1,D2,D3,D4                CURRENTLY NOT USED BY PROGRAM.

CARD E.6.C                      FORMAT (I6)

NTMPTS                      THE NUMBER OF TIME POINTS OR CARDS REQUIRED  
                             TO DEFINE THIS FUNCTION ON CARDS E.6.D-E.6.N.

CARDS E.6.D - E.6.N  
(NTMPTS CARDS)                FORMAT (4F12.0)

T                              TIME (SEC.) SINCE INITIAL PENETRATION OF  
                             BOUNDARY PLANE. VALUES SHOULD BE IN ASCENDING  
                             ORDER WITH FIRST VALUE EQUAL TO ZERO.

FX,FY,FZ                      THE X,Y AND Z COMPONENTS OF FORCE PER UNIT  
                             AREA (LBS./IN.\*\*2) IN INERTIAL REFERENCE  
                             DUE TO THE WIND BLAST FORCE AT TIME T. THE  
                             PROGRAM WILL USE LINEAR INTERPOLATION ON T.  
                             IF LAST VALUE OF T IS EXCEEDED, THE LAST  
                             VALUES OF FX,FY AND FZ WILL BE USED.

NJNTF (FROM CARD E.5) SETS OF CARDS E.7.A - E.7.N ARE REQUIRED.

CARD E.7.A                      FORMAT (I4, 4X, 5A4)

I,KTITLE                      SAME AS CARD E.1 EXCEPT THAT EACH FUNCTION  
NUMBER (I) MUST BE LESS THAN 51 AND MUST BE  
DISTINCT FROM THOSE SUPPLIED ON CARDS E.1  
OR CARDS E.6.A.

CARD E.7.B                      FORMAT (5F12.0)

D0,D1,D2,D3,D4                CURRENTLY NOT USED BY PROGRAM.

CARD E.7.C                      FORMAT (2I6)

NTHETA                        MAGNITUDE INDICATES THE NUMBER OF COLUMNS  
IN THE TWO DIMENSIONAL INPUT DATA MATRIX  
TO BE SUPPLIED ON CARDS E.7.D-E.7.N. THE  
MINIMUM VALUE IS 2. IF POSITIVE, THE NTHETA  
ENTRIES IN EACH ROW WILL BE TABULAR DATA FOR  
EQUALLY SPACED VALUES OF THE JOINT FLEXURE  
ANGLE (THETA) BETWEEN 0 AND 180 DEGREES.  
IF NEGATIVE, THE ENTRIES WILL REPRESENT THE  
COEFFICIENTS OF A (-NTHETA-1) ORDER  
POLYNOMIAL IN (THETA-THETA0)

NPHI                            NUMBER OF ROWS OF MATRIX OF DATA TO BE SUPPLIED  
ON CARDS E.7.D-E.7.N. EACH ROW REPRESENTS  
EQUALLY SPACED VALUES OF THE JOINT AZIMUTH  
ANGLE (PHI) BETWEEN -180 AND +180 DEGREES,  
BUT DOES NOT INCLUDE THE LAST ROW SINCE THE  
PROGRAM ASSUMES DATA FOR PHI(NPHI+1)=180 ARE  
THE SAME AS FOR PHI(1)=-180. MINIMUM = 1.

CARDS E.7.D - E.7.N            FORMAT (5F12.0)  
(NPHI SETS OF CARDS. USE EXTRA CARDS PER SET IF |NTHETA| > 5.)

THETA0                        THE VALUE OF THE "DEAD BAND" ZONE FOR THIS  
VALUE OF PHI (DEGREES). IF THE FLEXURE  
ANGLE (THETA) IS LESS THAN THETA0, THE  
JOINT RESTORING FORCE WILL BE ZERO.

F(J),J=2,NTHETA                FOR NTHETA POSITIVE, TABULAR VALUES OF THE  
JOINT RESTORING FORCE FOR FLEXURE ANGLES

THETA(J) = (J-1)\*180/(NTHETA-1) DEGREES

VALUES OF ZERO SHOULD BE SUPPLIED FOR  
THETA < THETA0.

FOR NTHETA NEGATIVE, THE COEFFICIENTS OF A  
POLYNOMIAL IN (THETA-THETA0) OF ORDER ONE  
LESS THAN THE MAGNITUDE OF NTHETA. F(J) IS  
THE COEFFICIENT OF (THETA-THETA0)\*\*(J-1)  
WHERE (THETA-THETA0) IS EXPRESSED IN RADIANS.  
F(1) IS ASSUMED TO BE ZERO.



F. SUBROUTINE FINPUT (ALLOWED CONTACTS AND ASSOCIATED FUNCTIONS)

IF NPL # 0, F.1 IS REQUIRED.

CARD F.1.A                      FORMAT (18I4)              IF NPL>18, USE 2 CARDS.

MNPL(J),J=1,NPL              FOR PLANE J, THE NUMBER OF SEGMENTS FOR WHICH SEGMENT-PLANE CONTACT IS ALLOWED. NPL IS THE NUMBER OF PLANES FROM CARD D.1. THE VALUE OF ANY MNPL FOR PLANE J MAY BE ZERO AND THE MAXIMUM VALUE IS 5. HOWEVER IF IT IS REQUIRED TO HAVE MORE THAN 5 SEGMENTS CONTACT THE SAME PLANE, SET UP TWO OR MORE IDENTICAL PLANES AND PERMIT A MAXIMUM OF 5 SEGMENTS TO CONTACT EACH PLANE.

FOR EACH PLANE J, MNPL(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.1.B - F.1.N              FORMAT (9I4)

NJ                      THE PLANE NUMBER FOR WHICH CONTACT IS ALLOWED. NJ MUST CORRESPOND TO J ABOVE. THERE MUST BE MNPL(J) CARDS WITH THIS SAME NJ. IF MNPL(J) = 0, NO NJ = J SHOULD BE PRESENT.

NS(1)                      THE SEGMENT NUMBER TO WHICH PLANE J IS ATTACHED. IF VEHICLE, SUPPLY NSEG+1, IF GROUND, SUPPLY NSEG+2.

NS(2)                      THE SEGMENT NUMBER (DETERMINED BY THE CARD NUMBER 1 UNDER CARD B.2.A FOR WHICH CONTACT WITH THE NJTH PLANE IS ALLOWED.

NS(3)                      THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH THE SEGMENT NS(2).



NF(1) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE FORCE-DEFLECTION FUNCTION FOR THIS CONTACT. IF NF(1) = 0, A ROLLING - SLIDING CONSTRAINT OPTION WILL BE EXERCISED BY THE PROGRAM FOR THIS CONTACT WHICH DOES NOT REQUIRE NF(2), NF(3) OR NF(4) BUT DOES REQUIRE A FRICTION COEFFICIENT FUNCTION TO BE DEFINED BY NF(5). THE VALUE OF D3 ON CARD E.2 OF THIS FUNCTION SHOULD BE 0.5 (NON-ZERO TO ACTIVATE THE IMPULSE AND TO SET THE NORMAL COMPONENT OF RELATIVE VELOCITY TO ZERO AFTER THE IMPULSE HAS BEEN APPLIED). ALSO THE INITIAL POSITIONS ON CARDS G.2 MUST BE SUCH THAT CONTACT DOES NOT EXIST AT TIME = 0.

NF(2) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE INERTIAL SPIKE FUNCTION FOR THIS CONTACT. IF NF(2) = 0, NO INERTIAL SPIKE EXISTS.

NF(3) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE R (ENERGY-ABSORPTION) FACTOR FUNCTION. IF NF(3) = 0, A DEFAULT VALUE OF R = 1 IS ASSUMED.

NF(4) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE G (DEFLECTION) FACTOR FUNCTION. IF NF(4) = 0, A DEFAULT VALUE OF G = 0 IS ASSUMED.

NF(5) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE FRICTION COEFFICIENT FUNCTION.

IF NBLT # 0, F.2 IS REQUIRED.

CARD F.2.A                      FORMAT (8I4)

MNBLT(J), J=1, NBLT      FOR BELT J, THE NUMBER OF SEGMENTS FOR WHICH SEGMENT-BELT INTERACTION IS ALLOWED. NBLT IS THE NUMBER OF BELTS FROM CARD D.1. EACH MNBLT MAY HAVE A VALUE OF 0 OR 1 ONLY.

FOR EACH BELT J, MNBLT(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.2.B - F.2.N              FORMAT (9I4)

NJ                      THE BELT NUMBER TO BE CONTACTED, MUST CORRESPOND TO J ABOVE. THERE MUST BE MNBLT(J) CARDS WITH THE SAME NJ. IF MNBLT(J) = 0, NO NJ = J SHOULD BE PRESENT.

NS(1)                      THE SEGMENT NUMBER TO WHICH BELT NJ IS ATTACHED. IF VEHICLE, SUPPLY NSEG+1, IF GROUND, SUPPLY NSEG+2.

NS(2)                      THE SEGMENT NUMBER (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A) FOR WHICH INTERACTION WITH THE NJTH BELT IS ALLOWED.

NS(3)                      THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH THE SEGMENT NS(2).

NF(1)                      THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE FORCE-DEFLECTION FUNCTION FOR THIS CONTACT. THE ABSCISSA FOR THIS FUNCTION SHOULD BE STRAIN (IN/IN).

NF(I), I=2,4                      SAME DEFINITION AS ON CARD F.1.B ABOVE.

NF(5)                      IF NON-ZERO, FULL BELT FRICTION IS ASSUMED, I.E., FORCES ARE COMPUTED FOR EACH HALF OF THE BELT SEPARATELY. IF ZERO, ZERO BELT FRICTION IS ASSUMED, I.E., BELT TENSION IS THE SAME AT BOTH BELT ANCHOR POINTS.

A BLANK F.3.A CARD IS REQUIRED FOR NO SEGMENT-SEGMENT CONTACTS.

CARD F.3.A                      FORMAT (18I4)    IF NSEG>18, USE TWO CARDS.

MNSEG(J),J=1,NSEG            FOR SEGMENT J, THE NUMBER OF SEGMENTS FOR WHICH SEGMENT-SEGMENT CONTACT IS ALLOWED. NSEG IS THE NUMBER OF SEGMENTS FROM CARD B.1. EACH SEGMENT CONTACT, A VERSUS B, MAY BE INPUTTED EITHER WAY EXCEPT WHERE AN INTERIOR CONTACT IS DESIRED (SEE NS(3) ). ANY OR ALL VALUES OF MNSEG MAY BE ZERO. THE MAXIMUM VALUE FOR EACH MNSEG IS 5.

FOR EACH SEGMENT J, MNSEG(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.3.B - F.3.N            FORMAT (9I4)

NJ                              THE SEGMENT NUMBER TO BE CONTACTED, MUST CORRESPOND TO J ABOVE. THERE MUST BE MNSEG(J) CARDS WITH THIS SAME NJ. IF MNSEG(J) = 0, NO NJ = J SHOULD BE PRESENT.

NS(1)                          THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH SEGMENT NJ.

NS(2)                          THE SEGMENT NUMBER (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A) FOR WHICH CONTACT WITH THE NJTH SEGMENT IS ALLOWED.

NS(3)                          THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH THE SEGMENT NS(2). IF NEGATIVE, AN INTERIOR CONTACT WILL BE ASSUMED WITH ELLIPSOID NS(1) INSIDE NS(3).

NF(I),I=1,5                    SAME DEFINITIONS AS ON CARD F.1.B ABOVE.

IF NJNT > 0, F.4.A IS REQUIRED.

SUPPLY IGLOB=1 FOR GLOBALGRAPHIC OPTION, OTHERWISE SUPPLY 0 OR BLANK

CARD F.4.A                      FORMAT (18I4)    IF NJNT>18, USE TWO CARDS.

IGLOB(J),J=1,NJNT    FOR EACH JOINT J, SUPPLY I FOR IGLOB(J) IF  
IPIN(J) IS +3 OR -3 ON CARDS B.3.A - B.3.J;  
OTHERWISE SUPPLY ZERO OR BLANK. ONE CARD  
F.4.J MUST BE SUPPLIED BELOW FOR EACH J FOR  
WHICH IGLOB(J) =1.

CARDS F.4.B - F.4.J            FORMAT (9I4)

NJ                      THE IDENTIFICATION NUMBER FOR A GLOBALGRAPHIC  
JOINT, MUST CORRESPOND TO J ABOVE AND CARDS  
MUST BE SUPPLIED IN ASCENDING ORDER ON NJ.

NS(I),I=1,3            CURRENTLY NOT USED BY PROGRAM.

NF(1)                   THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE  
THE TORQUE-DEFLECTION FOR THIS GLOBALGRAPHIC  
JOINT. THE ORDINATE FOR THIS FUNCTION SHOULD  
BE TORQUE (IN. LB.) AND THE ABSCISSA IS THE  
ANGULAR DEFLECTION (RADIAN) INTO THE STOP.

NF(2)                   THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE  
THE HERRON FORMULAS FOR T (JOINT STOP ANGLE  
IN RADIAN) AND ITS DERIVATIVE TP WITH RES-  
PECT TO PHI BOTH AS FUNCTIONS OF PHI (THE  
JOINT ANGLE FROM THE REFERENCE AXIS IN RAD-  
IAN). NORMALLY THEY WILL BE COMPUTED BY

$$T = P1 + SP*P2$$
$$TP = P1' + CP*P2 + SP*P2'$$

WHERE P1,P2 ARE THE 5TH DEGREE POLYNOMIAL  
EVALUATIONS OF COS(PHI) USING THE  
TWO POLYNOMIALS F1 AND F2 OBTAINED BY  
SETTING BOTH D1,D2 > 0 ON CARD E.2;

P1',P2' ARE THEIR DERIVATIVES WITH  
RESPECT TO PHI;

AND CP,SP ARE COS(PHI) AND SIN(PHI).

IF D1,D2 ARE NOT BOTH POSITIVE, T AND TP  
WILL BE EVALUATED AS FUNCTIONS OF PHI IN  
RADIAN (0 < PHI < 2\*PI) AS SPECIFIED ON  
CARDS E.1 - E.4 FOR FUNCTION NF(2).

SAME DEFINITIONS AS ON CARD F.1.B ABOVE

IF NJNT > 0, CARD F.5.A IS ALWAYS REQUIRED BUT MAY BE BLANK.

CARD F.5.A                      FORMAT (I8I4) USE TWO CARDS IF NJNT > I8.

JOINTF(J),J=I,NJNT    FOR EACH JOINT (J), THE FUNCTION IDENTIFICATION NUMBER AS SUPPLIED ON CARDS E.7.A TO BE USED BY SUBROUTINE VISPR TO COMPUTE THE JOINT RESTORING FORCE BY FUNCTION FINTERP. IF ZERO, THE VALUES OF SPRING(1,3\*J-2) AS SUPPLIED ON CARDS B.4.A WILL BE USED USING FUNCTION EJOINT.

IF NBAG # 0, NBAG CARDS OF THE FOLLOWING MUST BE SUPPLIED. SINCE THE AIR BAG ROUTINES DO NOT USE THE FORCE-DEFLECTION FUNCTIONS, THIS INPUT HAS DIFFERENT FORMATS THAN THE ABOVE ALLOWED CONTACTS.

CARDS F.6.A - F.6.N            FORMAT (2I4, 20I2)

K                      THE AIR BAG NUMBER CORRESPONDING TO THE INDEX J UNDER CARDS D.4 ABOVE. K MUST BE IN NUMERIC ORDER K = 1 TO NBAG, WHERE NBAG IS THE NUMBER OF AIR BAGS DEFINED ON CARD D.I.

NK                     THE NUMBER OF SEGMENTS ALLOWED TO CONTACT THE KTH AIR BAG. THE MAXIMUM VALUE IS 10. IF NK = 0, THE REMAINDER OF THE CARD IS BLANK.

MBAG(2,I,K),  
MBAG(3,I,K),I=1,NK    THE SEGMENT NUMBERS (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A) EACH FOLLOWED BY THE NUMBER OF THE ASSOCIATED CONTACT ELLIPSOID FOR WHICH CONTACT FORCES WITH THE KTH AIR BAG WILL BE COMPUTED.



CARD F.7.A IS ALWAYS REQUIRED. INSERT A BLANK CARD IF NO WIND FORCE CALCULATIONS ARE TO BE PERFORMED.

CARD F.7.A                      FORMAT (I8I4) USE TWO CARDS IF NSEG > 18.

MWSEG(1,J), J=1,NSEG FOR EACH SEGMENT J, SUPPLY ZERO IF NO WIND FORCE CALCULATIONS ARE TO BE PERFORMED. OTHERWISE, SUPPLY A VALUE OF ONE TO INDICATE WIND FORCES ARE TO BE PERFORMED.

SUPPLY CARD F.7.B FOR EACH SEGMENT (J) WHERE MWSEG(1,J) = 1.

CARD F.7.B                      FORMAT (5I4)

JJ                              THE SEGMENT IDENTIFICATION NUMBER FROM CARDS B.2.A FOR WHICH WIND FORCE CALCULATIONS ARE TO BE PERFORMED. MUST CORRESPOND TO J FROM CARD F.7.A AND BE SUPPLIED IN ASCENDING ORDER.

MWSEG(2,J)                    THE NUMBER OF THE CONTACT ELLIPSOID TO BE ASSOCIATED WITH SEGMENT NUMBER JJ.

MWSEG(3,J)                    THE SEGMENT IDENTIFICATION NUMBER (NSEG+1 FOR THE VEHICLE, NSEG+2 FOR THE GROUND) ASSOCIATED WITH PLANE NUMBER MWSEG (4,J).

MWSEG(4,J)                    THE PLANE IDENTIFICATION NUMBER FROM CARD D.2.A THROUGH WHICH IF SEGMENT J PASSES, WIND FORCE CALCULATIONS WILL BE PERFORMED.

MWSEG(5,J)                    THE FUNCTION NUMBER FROM CARD E.6.A FOR THE WIND FORCE FUNCTION TO BE USED.

F.8 SUBROUTINE HINPUT - CARD INPUT FOR HARNESS-BELT SYSTEMS.

CARD F.8.A IS ALWAYS REQUIRED. INSERT BLANK CARD IF NO HARNESS-BELT SYSTEMS ARE DESIRED.

CARD F.8.A                      FORMAT (6I4)

NHRNSS                      NUMBER OF HARNESS-BELT SYSTEMS TO BE  
SUPPLIED ON CARDS F.8.B-F.8.D. MAY BE ZERO  
OR BLANK. MAXIMUM VALUE = 5.

NBLTPH(I),                  NUMBER OF INDIVIDUAL BELTS FOR EACH HARNESS  
I=1,NHRNSS                  NO. I. MAY BE ZERO OR BLANK. MAXIMUM VALUE  
OF SUM OF ALL NBLTPH IS 20.

CARD F.8.A IS FOLLOWED BY NHRNSS SETS OF CARDS F.8.B - F.8.D.

CARD F.8.B                      FORMAT (18I4) USE TWO CARDS IF NBLTPH(I)>18.

NPTSPB(J),                  THE NUMBER OF REFERENCE POINTS INCLUDING  
J=1,NBLTPH(I)                  ANCHOR POINTS FOR BELT NO. J OF HARNESS  
NO. I. MAY BE ZERO OR BLANK. THE MAXIMUM  
VALUE OF THE SUM OF ALL NPTSPB FOR ALL  
HARNESS-BELT SYSTEMS IS 100.

EACH CARD F.8.B IS FOLLOWED BY NBLTPH(I) SETS OF CARDS F.8.C - F.8.D.

CARD F.8.C                      FORMAT (5I4, F12.6)

NFBLT(L,J),L=1,5              THE IDENTIFICATION NUMBERS OF THE 5 FUNCTIONS  
TO BE USED FOR BELT NO. J. THESE CORRESPOND  
TO I AS SUPPLIED ON CARDS E.1 OF THE FUNCTION  
DEFINITIONS. THESE FUNCTIONS ARE IDENTICAL TO  
THOSE DEFINED BY NF(I) - NF(5) ON CARDS F.2.B  
EXCEPT THAT THE COEFFICIENT OF FRICTION AS  
SPECIFIED BY NF(5) IS NOT CURRENTLY USED.

XLONG(J)                      BELT SLACK (IN). THE SLACK. WHEN ADDED TO  
THE INITIAL GEOMETRIC LENGTH, RESULTS IN  
THE INITIAL BELT LENGTH. IF DESIRED, THE  
INITIAL BELT LENGTH MAY BE SUPPLIED AS A  
NEGATIVE NUMBER AND THE PROGRAM WILL  
COMPUTE THE SLACK.



EACH CARD F.8.C IS FOLLOWED BY NPTSP8(J) CARDS F.8.D SPECIFYING THE REFERENCE POINTS (K) TO BE USED FOR BELT NO. J OF HARNESS NO. I.

CARD F.8.D

FORMAT (2I6, 3F12.6)

IBAR(1,K)

THE IDENTIFICATION NUMBER OF THE SEGMENT ASSOCIATED WITH REFERENCE POINT K.

IBAR(2,K)

THE IDENTIFICATION NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH POINT K. IF ZERO, PROGRAM WILL ASSUME BELT IS RIGIDLY ATTACHED TO THAT POINT (AS FOR ANCHOR POINTS ATTACHED TO THE VEHICLE).

BAR(L,K),L=1,3

THE X,Y AND Z COORDINATES OF REFERENCE POINT K IN THE LOCAL COORDINATE SYSTEM OF SEGMENT NO. IBAR(1,K). THE PROGRAM WILL ASSUME THAT BELT J WILL RUN THROUGH THE POINTS IN THE ORDER THEY ARE SUPPLIED. HOWEVER IF A CONTACT ELLIPSOID IS SPECIFIED BY IBAR(2,K) AND THE THE FORCES ARE SUCH AS TO PULL THE BELT AWAY FROM THE SURFACE, THIS POINT WILL BE IGNORED THAT TIME POINT.

# G. SUBROUTINE INITIAL

CARD G.I

FORMAT (3F10.0, 5I4)

ZPLT(I), I=1,3

THE X, Y, AND Z PLOT COORDINATES  
(FOR SUBROUTINE PRIPLT) OF THE  
ORIGIN OF THE VEHICLE REFERENCE  
SYSTEM.  $0 < X < 61$   
 $0 < Y < 61$   
 $0 < Z < 121$

I1, J1, I2, J2

NOT USED BY THE CURRENT PROGRAM.

I3

IF ZERO, SEGMENT AND ANGULAR VELOCITIES ARE  
NOT SUPPLIED ON THE FOLLOWING CARDS BUT ARE  
SET EQUAL TO THE INITIAL VEHICLE VELOCITY.  
IF I3  $\neq$  0, SEGLV AND WMGDEG MUST BE SUPPLIED.

ONE G.2 CARD MUST BE SUPPLIED FOR EACH REFERENCE SEGMENT (I.E.,  
SEGMENT NO. 1 AND FOR EACH SEGMENT J+I WHERE JNT(J) = 0 ON CARDS  
B.3) IN ASCENDING SEGMENT NUMBER SEQUENCE.

CARDS G.2.A - G.2.M

FORMAT (6F10.0)

SEGLP(I, J), I=1,3

THE INITIAL X, Y, AND Z COORDINATES OF THE  
JTH BODY SEGMENT IN INERTIAL REFERENCE (IN).

SEGLV(I, J), I=1,3

THE INITIAL X, Y, AND Z COMPONENTS OF VELOCITY  
OF THE JTH BODY SEGMENT IN INERTIAL REFER-  
ENCE (IN/SEC). THESE FIELDS MAY BE LEFT BLANK  
IF I3 = 0 ON CARD G.1 IN WHICH CASE THE  
INITIAL VELOCITY OF THE VEHICLE WILL BE USED.

CARDS G.3.A - G.3.N  
(NSEG CARDS)

FORMAT (6F10.0)

YPR(I, J), I=1,3

THE INITIAL YAW, PITCH AND ROLL ANGLES OF  
THE JTH BODY SEGMENT (DEGREES).

NOTE: THE DIRECTION COSINE MATRICES OF THE BODY SEGMENTS ARE INITIALLY  
COMPUTED BY ASSUMING THE ORDER OF THE ROTATING ANGLES IS REVERSED,  
I.E., ROLL, PITCH, YAW.  
(ROLL ABOUT X, PITCH ABOUT Y, AND YAW ABOUT Z.)

WMGDEG(I, J), I=1,3

THE INITIAL COMPONENTS OF ANGULAR VELOCITY  
ABOUT THE LOCAL X, Y AND Z AXES OF THE JTH  
BODY SEGMENT (DEG/SEC). IF I3 = 0 ON CARD  
G.1, THE INITIAL ANGULAR VELOCITY OF THE  
VEHICLE WILL BE CONVERTED TO THE SEGMENT  
REFERENCE AND WILL BE USED.

## H. SUBROUTINE HEDING

THIS SUBROUTINE PROVIDES INPUT TO CONTROL THE DESIRED TIME HISTORY OUTPUT OF SELECTED SEGMENT LINEAR AND ANGULAR ACCELERATIONS, VELOCITIES, AND DISPLACEMENTS, AND JOINT PARAMETERS.

### H.1 SEGMENT LINEAR ACCELERATIONS (K = 1)

CARD H.1.A	FORMAT (2I6, 3F12.6)
NSG(K)	THE NUMBER OF SELECTED POINTS ON THE VARIOUS BODY SEGMENTS FOR WHICH TIME HISTORIES ARE DESIRED. THE MAXIMUM VALUE FOR NSG(K) IS 20. IF NSG(K) IS 0, INSERT 2 BLANK CARDS. IF NSG(K) IS 1, A SINGLE BLANK CARD SHOULD FOLLOW CARD H.1.K.
MSG(1,K)	THE SEGMENT NUMBER AS DETERMINED BY INDEX I ON CARDS B.2.A - B.2.N OF THE FIRST POINT.
XSG(I,1,K), I=1,3	THE X, Y, AND Z COORDINATES IN SEGMENT REFERENCE OF THE FIRST POINT (INCHES).

FOLLOWED BY NSG(K)-1 CARDS OF THE FOLLOWING (J = 2, NSG(K) )

CARDS H.1.B - H.1.N	FORMAT (1I2, 3F12.6)
MSG(J,K)	SAME AS ABOVE BUT FOR THE JTH POINT.
XSG(I,J,K), I=1,3	SAME AS ABOVE BUT FOR THE JTH POINT.

### H.2 SEGMENT LINEAR VELOCITIES (K = 2)

CARDS H.2.A - H.2.N	FORMAT (2I6, 3F12.6/(1I2, 3F12.6))
DESCRIPTION SAME AS FOR H.1.	

### H.3 SEGMENT LINEAR DISPLACEMENTS (K = 3)

CARDS H.3.A - H.3.N	FORMAT (2I6, 3F12.6/(1I2, 3F12.6))
DESCRIPTION SAME AS FOR H.1.	

#### H.4 SEGMENT ANGULAR ACCELERATIONS (K = 4)

CARD H.4

FORMAT (12I6/1I2, 3I6)

NSG(K)

THE NUMBER OF SELECTED BODY SEGMENTS FOR WHICH TIME HISTORIES ARE DESIRED. INSERT BLANK CARD IF NONE ARE DESIRED (NSEG MAXIMUM).

MSG(J,K),J=1,KSG  
WHERE KSG=NSG(K)

THE SEGMENT NUMBERS AS DETERMINED BY INDEX I ON CARDS B.2.A - B.2.N. IF NSG(K) > 11, USE THE SECOND CARD, LEAVING THE FIRST FIELD OF 6 COLUMNS BLANK. IF NSG(K) = 11, A SECOND CARD, COMPLETELY BLANK, SHOULD FOLLOW THIS CARD.

#### H.5 SEGMENT ANGULAR VELOCITIES (K = 5)

CARD H.5

FORMAT (12I6/1I2, 3I6)

DESCRIPTION SAME AS FOR H.4.

#### H.6 SEGMENT ANGULAR DISPLACEMENTS (K = 6)

CARD H.6

FORMAT (12I6/1I2, 3I6)

DESCRIPTION SAME AS FOR H.4.

#### H.7 JOINT PARAMETERS (K = 7)

CARD H.7

FORMAT (12I6/1I2, 2I6)

NSG(K)

THE NUMBER OF SELECTED JOINTS FOR WHICH TIME HISTORIES ARE DESIRED. INSERT BLANK CARD IF NONE ARE DESIRED (NJNT MAXIMUM).

MSG(J,K),J=1,KSG  
WHERE KSG=NSG(K)

THE JOINT NUMBERS AS DETERMINED BY INDEX J ON CARDS B.3.A - B.3.J. IF NSG(K) > 11, USE A SECOND CARD LEAVING THE FIRST FIELD OF 6 COLUMNS BLANK. IF NSG(K) = 11, A SECOND CARD, COMPLETELY BLANK, SHOULD FOLLOW THIS CARD.

## APPENDIX B

The listing of 21 subroutines that follow represent the changes or additions that were made to the computer program contained in Volume IV, Programmer's Manual of Calspan Report No. ZQ-5180-L-1, "An Improved Three Dimensional Computer Simulation of Motor Vehicle Crash Victims," July 1974 to fulfill the requirements of Wright Patterson AFB Contract No. F33615-75-C-5002. Any subroutine not contained herein remains unchanged from the above mentioned report.

The following is a list of the included subroutines and a summary of the changes that have been made to them.

1. SUBROUTINE CINPUT: Statement numbers have been renumbered for readability and previous version has been subdivided into new SUBROUTINE CINPUT and SUBROUTINE FINPUT. Calls to new subroutines KINPUT and HINPUT have been added.
2. SUBROUTINE CONTCT: Card No.'s 140-160 and 780-1050 have been added to control the calling of SUBROUTINE WINDY and SUBROUTINE HBELT.
3. SUBROUTINE DINT: Card No.'s 530 and 2150-2170 have been modified to simplify program logic and are equivalent to previous version.
4. SUBROUTINE ELTIME: Card No.'s 210 and 220 have been modified to include SUBROUTINE WINDY and SUBROUTINE HBELT for N=35 and 36.
5. FUNCTION EVALFD: Extensive modifications have been made to accomodate abscissas that exceed the range of tabular function definitions.
6. SUBROUTINE FINPUT: New subroutine that is actually the second half of previous SUBROUTINE CINPUT that controlled the input specifying allowed contacts between body segments with vehicle panels, belts, airbags and other body segments. New code has been inserted at card no.'s 2100-2280 for new input card F.5 defining joint functions to be used. Old input cards F.5 have been renamed F.6 and new code has been inserted at card no.'s 2540-2800 for input cards F.7 controlling the new wind force calculations.

## APPENDIX B (Continued)

7. SUBROUTINE FLXSEG: Card No.'s 130 and 140 have been interchanged to properly control the call to SUBROUTINE ELTIME.
8. FUNCTION FNTERP: New subroutine that computes the restoring torque of a joint by double linear interpolation on the flexure angle ( $\theta$ ) and azimuth angle ( $\phi$ ).
9. SUBROUTINE HBELT: New subroutine that computes the forces and torques of individual belt sections of the harness-belt systems.
10. SUBROUTINE HINPUT: New subroutine that controls the input of cards F.8.A-F.8.D containing the setup and control of the harness-belt system.
11. SUBROUTINE IMPULS: Card No.'s 1810 and 1820 have been modified to properly control call to SUBROUTINE ELTIME.
12. SUBROUTINE KINPUT: New subroutine that controls the input of cards E.5, E.6 and E.7 containing the definitions of the wind force and joint restoring force functions.
13. SUBROUTINE OUTPUT: Card No.'s 1280-1300 have been modified to print the joint angles in degrees for the new joint functions.
14. SUBROUTINE PLELP: Comments in card no.'s 50 and 60 have been corrected.
15. SUBROUTINE RSTART: Card No.'s 630-640, 1480-1580, 1630-1640, 1770, 1890, 1970, 2060, 2150, 2170-2180, 2930 and 4410-4620 have been modified or added to insert JOINTF in COMMON/DESCRP/ and to include COMMON/HARNESS/ and COMMON/KALEPS/.
16. SUBROUTINE SEARCH: Several additions and modifications have been made to accomodate the changes made to SUBROUTINE RSTART.



## APPENDIX B (Continued)

17. SUBROUTINE UPDATE: Card No.'s 360-370, 1020-1210 have been added to call SUBROUTINE UPDFDC for each belt of harness-belt systems and card no. 2400 has been modified to set initial state of rolling-sliding constraint.
18. SUBROUTINE VEHPOS: Card No.'s 410-440 and 1100-1110 have been modified to extrapolate beyond last entry in vehicle position input tables.
19. SUBROUTINE VINPUT: Card No.'s 560, 600 and 750-810 have been modified to permit input of negative VIPS on input card C.2 and delete the restriction that the last acceleration on card C.3 be zero.
20. SUBROUTINE VISPR: Card No.'s 190, 310, 560-570, 600-870, 930, 1090-1100, 1190-1230, 1350-1410, 1450, 1470-1480, 1500, 1560, 1580, 1650-1670, 1800, 1830-1840, 1990-2000 and 2020 have been added or modified to include the necessary logic for the new joint functions.
21. SUBROUTINE WINDY: New subroutine that computes the forces and torques of a wind blast acting on specified body segments.



	SUBROUTINE CINPUT	CINPC010
C		REV 12 12/18/74CINP0020
C	CONTROLS THE CARD INPUT OF THE FORCE-DEFLECTION, INERTIAL SPIKE,	CINP0030
C	R FACTOR, G FACTOR AND FRICTION COEFFICIENT FUNCTION DEFINITIONS	CINP0040
C		CINP0050
	IMPLICIT REAL*8(A-H,O-Z)	CINP0060
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)	CINP0070
	COMMON/TEMPVS/JTITL(5,51),NF(5),NS(3),KTITL(31)	CINP0080
	REAL JTITL,KTITL	CINP0090
	IS = 0	CINP0100
	DO 10 I = 1,50	CINP0110
10	NTI(I) = 0	CINP0120
	J1 = 1	CINP0130
C		CINP0140
C	INPUT CARD E.1 - FUNCTION NO. AND TITLE, IF NO. > 50 SKIP OUT.	CINP0150
C		CINP0160
	11 READ (5,12) I,(KTITL(J),J = 1,5)	CINP0170
	12 FORMAT (I4,4X,5A4)	CINP0180
	IF (I.GT.50) GO TO 30	CINP0190
	DO 13 J = 1,5	CINP0200
	13 JTITL(J,I) = KTITL(J)	CINP0210
C		CINP0220
C	HAS FUNCTION NO. BEEN ALREADY USED?	CINP0230
C		CINP0240
	IF (NTI(I).NE.0) WRITE(6,14) I	CINP0250
	14 FORMAT('O FUNCTION NO.',I4,' HAS ALREADY BEEN INPUTTED AND WILL BE	CINP0260
	*REPLACED BY NEXT FUNCTION')	CINP0270
	NTI(I) = J1	CINP0280
	J2 = J1+4	CINP0290
C		CINP0300
C	INPUT CARD E.2	CINP0310
C		CINP0320
	READ (5,15) (TAB(J),J = J1,J2)	CINP0330
15	FORMAT (6F12.0)	CINP0340
	IS = 1-IS	CINP0350
	IF (IS.EQ.0) WRITE (6,16)	CINP0360
16	FORMAT(/////)	CINP0370
	WRITE (6,17) IS,I,(JTITL(J,I),J=1,5),I,NTI(I),(TAB(J),J=J1,J2)	CINP0380
17	FORMAT(I1,'FUNCTION NO.',I4,4X,5A4,20X,'NTI(' ,I2,' ) =' ,I5,45X	CINP0390
	* 'CARDS E'//10X,'D0',13X,'D1',13X,'D2',13X,'D3',13X,'D4'/5F15.4//)	CINP0400
	D0 = TAB(J1)	CINP0410
	D1 = TAB(J1+1)	CINP0420
	D2 = TAB(J1+2)	CINP0430
	J1 = J2+1	CINP0440
	IF (D1) 22,18,20	CINP0450
C		CINP0460
C	FUNCTION IS CONSTANT D2 FOR ALL D.	CINP0470
C		CINP0480
	18 WRITE (6,19) D2	CINP0490
	19 FORMAT(7X,'FUNCTION IS CONSTANT',F12.6)	CINP0500

C	GO TO 11	CINP0510
C	5TH ORDER POLYNOMIAL ... 1ST FUNCTION	CINP0520
C	INPUT CARD E.3	CINP0530
C		CINP0540
		CINP0550
20	J2 = J1+5	CINP0560
	READ(5,15)(TAB(J),J = J1,J2)	CINP0570
	WRITE(6,21) (TAB(J),J = J1,J2)	CINP0580
21	FORMAT(7X,'FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL'//	CINP0590
*	8X,'A0',13X,'A1',13X,'A2',13X,'A3',13X,'A4',13X,'A5',13X/C	CINP0600
*	6F15.6//)	CINP0610
	J1 = J2+1	CINP0620
	GO TO 25	CINP0630
C		CINP0640
C	TABLE LOAD ... 1ST FUNCTION	CINP0650
C	INPUT CARDS E.4.A-E.4.N	CINP0660
C		CINP0670
22	READ(5,23) NPI	CINP0680
23	FORMAT (12I6)	CINP0690
	TAB(J1) = NPI	CINP0700
	J1 = J1+1	CINP0710
	J2 = J1+2*NPI-1	CINP0720
	READ(5,15)(TAB(J),J = J1,J2)	CINP0730
	WRITE (6,24) NPI, (TAB(J) ,J = J1, J2)	CINP0740
24	FORMAT(7X,'FIRST PART OF FUNCTION - ',I4,' TABULAR POINTS'//	CINP0750
*	8X,'D',16X,'F(D)' /(F15.6,F15.4))	CINP0760
	J1 = J2+1	CINP0770
C		CINP0780
C	CHECK FOR SECOND FUNCTION	CINP0790
C		CINP0800
25	IF(D2) 28,11,26	CINP0810
C		CINP0820
C	SECOND FUNCTION ... 5TH ORDER POLYNOMIAL	CINP0830
C	INPUT CARD E.3	CINP0840
C		CINP0850
		CINP0860
26	J2 = J1+5	CINP0870
	READ(5,15)(TAB(J),J = J1,J2)	CINP0880
	WRITE (6,27) (TAB(J),J = J1,J2)	CINP0890
27	FORMAT(7X,'SECOND PART OF FUNCTION - 5TH DEGREE POLYNOMIAL'//	CINP0900
*	8X,'B0',13X,'B1',13X,'B2',13X,'B3',13X,'B4',13X,'B5',13X/C	CINP0910
*	6F15.6//)	CINP0920
	J1 = J2+1	CINP0930
	GO TO 11	CINP0940
C		CINP0950
C	SECOND FUNCTION ... TABLE LOAD	CINP0960
C	INPUT CARDS E.4.A-E.4.N	CINP0970
C		CINP0980
28	READ(5,23) NPI	CINP0990
	TAB(J1) = NPI	CINP1000
	J1 = J1+1	

J2 = J1+2*NPI-1	CINP1010
READ(5,15)(TAB(J),J = J1,J2)	CINP1020
WRITE(6,29) NPI, (TAB(J), J = J1,J2)	CINP1030
29 FORMAT(7X,'SECOND PART OF FUNCTION - ',I4,' TABULAR POINTS'//	CINP1040
*       8X,'D',16X,'F(D)' / (F15.6,F15.4))	CINP1050
J1 = J2+1	CINP1060
GO TO 11	CINP1070
30 MXTB1 = J1-1	CINP1080
CALL KINPUT	CINP1090
CALL FINPUT	CINP1100
CALL HINPUT	CINP1110
RETURN	CINP1120
END	CINP1130

	SUBROUTINE CONTC1	CONT0010
		REV 12 12/19/74
C		CONT0020
C	CONTROLS THE CALLING OF SUBROUTINES REQUIRED TO COMPUTE THOSE	CONT0030
C	EXTERNAL FORCES AND TORQUES ACTING ON THE BODY SEGMENTS.	CONT0040
C		CONT0050
	IMPLICIT REAL*8 (A-H,O-Z)	CONT0060
	COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)	CONT0070
	COMMON/JBARTZ/ MNPL( 20),MNBLT( 8),MNSEG( 22),MNBAG( 6),	CONT0080
	* MPL(3,5,20),MBLT(3,5,8),MSEG(3,5,22),MBAG(3,10,6),	CONT0090
	* NTPL(5,20),NTBLT(5,8),NTSEG(5,22)	CONT0100
	COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),	CONT0110
	* NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21)	CONT0120
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NT1(50),NTAB(500),TAB(2000)	CONT0130
	COMMON/KALEPS/WTIME(30),IWIND(30),MWSEG(5,22)	CONT0140
	COMMON/HRNESS/ BAR(6,100) , XLONG(20), IBAR(2,100), NTHRNS(20),	CONT0150
	* NHRNSS, NBLTPH(5), NFBLT(5,20), NPTSPB(20)	CONT0160
	CALL ELTIME(1,12)	CONT0170
	NPSF = 0	CONT0180
	NBSF = 0	CONT0190
	NSSF = 0	CONT0200
	IF (NPL.LE.0) GO TO 21	CONT0210
C		CONT0220
C	CALL PLELP ROUTINE FOR EACH ALLOWED PLANE-SEGMENT CONTACT.	CONT0230
C		CONT0240
	DO 20 J=1,NPL	CONT0250
	IF(MNPL(J).EQ.0) GO TO 20	CONT0260
	KPL = MNPL(J)	CONT0270
	DO 19 I=1,KPL	CONT0280
	NPSF = NPSF+1	CONT0290
	M1 = MPL(1,1,J)	CONT0300
	M2 = MPL(2,1,J)	CONT0310
	M3 = MPL(3,1,J)	CONT0320
	NT = NTPL(I,J)	CONT0330
	JT = NTAB(NT)	CONT0340
	TAB(JT) = 0.0	CONT0350
	19 CALL PLELP(M2,M3,M1,J,NT)	CONT0360
	20 CONTINUE	CONT0370
	21 IF(NBLT.LE.0) GO TO 41	CONT0380
C		CONT0390
C	CALL BELTRT ROUTINE FOR EACH ALLOWED BELT-SEGMENT CONTACT.	CONT0400
C		CONT0410
	DO 30 J=1,NBLT	CONT0420
	IF(MNBLT(J).EQ.0) GO TO 30	CONT0430
	KBLT = MNBLT(J)	CONT0440
	DO 29 I=1,KBLT	CONT0450
	NBSF = NBSF+1	CONT0460
	M1 = MBLT(1,1,J)	CONT0470
	M2 = MBLT(2,1,J)	CONT0480
	M3 = MBLT(3,1,J)	CONT0490
	NT = NTBLT(1,J)	CONT0500

	JT = NTAB(NT)	CONT0510
	TAB(JT) = 0.0	CONT0520
	NF = NTAB(NT+5)	CONT0530
	IF (NF.NE.0) JT = NTAB(NT+6)	CONT0540
	IF (NF.NE.0) TAB(JT) = 0.0	CONT0550
	29 CALL BELTRT(M2,M3,M1,J,NT)	CONT0560
	30 CONTINUE	CONT0570
C		CONT0580
C	CALL SEGSEG ROUTINE FOR EACH ALLOWED SEGMENT-SEGMENT CONTACT.	CONT0590
C		CONT0600
	41 DO 50 J=1,NSEG	CONT0610
	IF (MNSEG(J).EQ.0) GO TO 50	CONT0620
	KSEG = MNSEG(J)	CONT0630
	DO 49 I=1,KSEG	CONT0640
	NSSF = NSSF+1	CONT0650
	M1 = MSEG(1,I,J)	CONT0660
	M2 = MSEG(2,I,J)	CONT0670
	M3 = MSEG(3,I,J)	CONT0680
	NT = NTSEG(I,J)	CONT0690
	JT = NTAB(NT)	CONT0700
	TAB(JT) = 0.0	CONT0710
	49 CALL SEGSEG(J,M1,M2,M3,NT)	CONT0720
	50 CONTINUE	CONT0730
C		CONT0740
C	CALL AIRBAG ROUTINE FOR ALLOWED BAG-SEGMENT CONTACTS, IF ANY.	CONT0750
C		CONT0760
	IF (NBAG.NE.0) CALL AIRBAG	CONT0770
C		CONT0780
C	CALL WINDY ROUTINE FOR WIND FORCES ON EACH SEGMENT.	CONT0790
C		CONT0800
	DO 60 J=1,NSEG	CONT0810
	IF (MWSEG(1,J).EQ.0) GO TO 60	CONT0820
	M1 = MWSEG(2,J)	CONT0830
	M2 = MWSEG(3,J)	CONT0840
	M3 = MWSEG(4,J)	CONT0850
	NT = MWSEG(5,J)	CONT0860
	CALL WINDY (J,M1,M2,M3,NT)	CONT0870
	60 CONTINUE	CONT0880
C		CONT0890
C	CALL HBELT ROUTINE FOR EACH HARNESS-BELT SYSTEM.	CONT0900
C		CONT0910
	IF (NHRNSS.LE.0) GO TO 99	CONT0920
	J1 = 1	CONT0930
	K1 = 1	CONT0940
	DO 70 I=1,NHRNSS	CONT0950
	IF (NBLTPH(I).LE.0) GO TO 70	CONT0960
	J2 = J1 + NBLTPH(I) -1	CONT0970
	DO 69 J=J1,J2	CONT0980
	IF (NPTSPB(J).LE.0) GO TO 69	CONT0990
	K2 = K1 + NPTSPB(J) -1	CONT1000

CALL HBELT(NPTSPB(J),IBAR(1,K1),BAR(1,K1),NTHRNS(J),XLONG(J))	CONT1010
K1 = K2+1	CONT1020
69 CONTINUE	CONT1030
J1 = J2+1	CONT1040
70 CONTINUE	CONT1050
99 CALL ELTIME(2,12)	CONT1060
RETURN	CONT1070
END	CONT1080



C	SUBROUTINE DINT(IN,N,DTPR,H0,HMAX,HMIN,/T/,X,DER,NOINT)	OINT0010
C		REV 12 10/25/74DINT0020
C	EXECUTIVE ROUTINE USED FOR PERFORMING AN INTEGRATION	OINT0030
C	STEP BETWEEN PRINT TIME POINTS.	OINT0040
C		OINT0050
C	ARGUMENTS	OINT0060
C	IN: INTEGRATION STEP NUMBER	DINT0070
C	N: NO OF VARIABLES TO BE SUPPLIED AS INPUT TO ROUTINE	OINT0080
C	OR COMPUTED BY SUBROUTINE PDAUX WHEN K=0 (MAX=120).	OINT0090
C	DTPR: PRINT TIME INTERVAL DESIRED	DINT0100
C	H0: INITIAL INTEGRATION STEP SIZE	OINT0110
C	HMAX: MAXIMUM INTEGRATION STEP SIZE	DINT0120
C	HMIN: MINIMUM STEP SIZE	OINT0130
C	T: TIME	DINT0140
C	X: ARRAY OF STATE VARIABLES	DINT0150
C	DER: ARRAY OF DERIVATIVES OF STATE VARIABLES	DINT0160
C	NOINT: NUMBER OF ESTIMATES OF INTEGRATION PARAMETERS	OINT0170
C	TO BE MADE AT THE END OF ANY INTERMEDIATE TIME STEP.	DINT0180
C		OINT0190
	IMPLICIT REAL*8 (A-H,O-Z)	DINT0200
	COMMON/CONTRL/ NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRNO,NPRT(40)	OINT0210
	COMMON/INTEST/ SGTEST(3,4,22),XTEST(264)	DINT0220
	COMMON/CNSNTS/ PI, RADIANT,G,THIRD,EPS1,EPS4,EPS6,EPS8,	OINT0230
	* EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)	OINT0240
	COMMON/COINT/ E(3,120),F(5,120),GG(5,120),Y(5,120),U(5,120)	DINT0250
	* ,H,HPRINT,TSAVE,TPRINT,TSTART,ICNT,IDBL,IFLAG	DINT0260
	DIMENSION X(120),DER(120)	DINT0270
C		DINT0280
C		DINT0290
	CALL ELTIME(1,3)	OINT0300
	IF (IN.NE.0) GO TO 3	DINT0310
C		DINT0320
C	FIRST TIME IN ROUTINE, PERFORM INITIALIZATION STEP .	DINT0330
C		OINT0340
	H = H0	DINT0350
	HPRINT = H	OINT0360
	IDBL=3	DINT0370
	ICNT = 0	OINT0380
	TPRINT = T	OINT0390
	CALL OUTPUT(0)	OINT0400
	K = 0	DINT0410
	CALL PDAUX(X,DER,N,K)	DINT0420
	IF (N.GT.120) WRITE (6,9) N	DINT0430
	9 FORMAT('0 NUMBER OF VARIABLES IN SUBROUTINE DINT IS',I6,	DINT0440
	* ' AND EXCEEDS THE ARRAY SIZES OF 120. PROGRAM TERMINATED.')	OINT0450
	IF (N.GT.120) STOP	OINT0460
	DO 1 1=1,N	DINT0470
	F(1,I) = X(I)	OINT0480
	F(2,I) = DER(I)	OINT0490
	F(3,I) = 0.	DINT0500



	F(4,I) = 0.	DINT0510
	1 F(5,I) = 0.	DINT0520
	GO TO 65	DINT0530
C		DINT0540
C	START OF NEW PRINT POINT INTERVAL.	DINT0550
C		DINT0560
	3 TPRINT = TPRINT+DTPR	DINT0570
	H = HPRINT	DINT0580
C		DINT0590
C	ENTRY TO ADVANCE INTEGRATDR.	DINT0600
C		DINT0610
	4 K = 1	DINT0620
	CALL UPDATE(K)	DINT0630
	IF (K.EQ.1) GO TO 2	DINT0640
C		DINT0650
C	RECALL PDAUX FOR IMPULSE IF K = -1	DINT0660
C		DINT0670
	IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT0680
	CALL PDAUX(X,DER,N,K)	DINT0690
	IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT0700
	H = H0	DINT0710
	ICNT = 0	DINT0720
	K = 1	DINT0730
	DO 6 I=1,N	DINT0740
	F(1,I) = X(I)	DINT0750
	F(2,I) = DER(I)	DINT0760
	F(3,I) = 0.0	DINT0770
	F(4,I) = 0.0	DINT0780
	6 F(5,I) = 0.0	DINT0790
	2 HPRINT = H	DINT0800
	IF (T+H*EPS8.GE.TPRINT) H = TPRINT-T	DINT0810
C		DINT0820
C	ENTRY TO BACKUP INTEGRATDR, CONVERGENCE TEST FAILED.	DINT0830
C		DINT0840
	5 D1 = 0.5*H	DINT0850
	D12=D1+D1	DINT0860
	D123=H-D1	DINT0870
	TSTART=T	DINT0880
	T=TSTART+D1	DINT0890
	DO 10 I=1,N	DINT0900
	DO 10 J=1,5	DINT0910
	U(J,I)=0.	DINT0920
	Y(J,I)=0.	DINT0930
	10 GG(J,I) = F(J,I)	DINT0940
	CALL DZP(N,X,GG,E,D1,1)	DINT0950
	IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT0960
	CALL PDAUX(X,DER,N,K)	DINT0970
	IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT0980
	DO 20 I=1,N	DINT0990
	W=X(I)-GG(1,I)	DINT1000

Z=DER(I)-GG(2,I)	DINT1010
Y(1,I)=Y(1,I)+W	DINT1020
Y(2,I)=Y(2,I)+Z	DINT1030
Y(3,I)=Y(3,I)+W**2	DINT1040
Y(4,I)=Y(4,I)+Z*W	DINT1050
20 GG(2,I)=DER(I)	DINT1060
CALL DZP(N,X,GG,E,D1,0)	DINT1070
K = 2	DINT1080
IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT1090
CALL PDAUX(X,DER,N,K)	DINT1100
IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT1110
T=TSTART+H	DINT1120
H1 = EPS1/H	DINT1130
DO 30 I=1,N	DINT1140
GG(2,I)=F(2,I)	DINT1150
W=X(I)-GG(1,I)	DINT1160
Z=DER(I)-GG(2,I)	DINT1170
Y(1,I)=Y(1,I)+W	DINT1180
Y(2,I)=Y(2,I)+Z	DINT1190
Y(3,I)=Y(3,I)+W**2	DINT1200
Y(4,I)=Y(4,I)+Z*W	DINT1210
Y(5,I)=Y(3,I)-.5*Y(1,I)**2	DINT1220
U(5,I)=Y(4,I)-.5*Y(1,I)*Y(2,I)	DINT1230
Z=0.	DINT1240
IF(Y(5,I).NE.0.)Z=U(5,I)/Y(5,I)	DINT1250
IF (Z.GT.H1) Z = H1	DINT1260
GG(5,I)=Z	DINT1270
ZYZ = (Y(2,I)-Z*Y(1,I))/D12	DINT1280
GG(4,I) = 0.5*GG(4,I)	DINT1290
30 GG(3,I) = ZYZ - D1*GG(4,I)	DINT1300
CALL DZP(N,X,GG,E,H,1)	DINT1310
K = 3	DINT1320
IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT1330
CALL PDAUX(X,DER,N,K)	DINT1340
IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT1350
DO 44 L=1,NDINT	DINT1360
ZL=L	DINT1370
ZH=ZL*H	DINT1380
DO 40 I=1,N	DINT1390
W=X(I)-GG(1,I)	DINT1400
Z=DER(I)-GG(2,I)	DINT1410
IF (DABS(W).LT.EPS24) W=0.0	DINT1420
IF (DABS(Z).LT.EPS24) Z=0.0	DINT1430
U(1,I)=U(1,I)+W	DINT1440
U(2,I)=U(2,I)+Z	DINT1450
U(3,I)=U(3,I)+W**2	DINT1460
U(4,I)=U(4,I)+W*Z	DINT1470
Z=GG(5,I)	DINT1480
IF(L.EQ.1)GO TO 35	DINT1490
Z=0.	DINT1500

	FX=Y(5,I)+U(3,I)-U(1,I)**2/ZL	DINT1510
	IF (FX.NE.0.) Z=(U(5,I)+U(4,I)-U(1,I)*U(2,I)/ZL)/FX	DINT1520
	IF (Z.GT.H1) Z = H1	DINT1530
35	GG(5,I)=Z	DINT1540
	W=(Y(2,I)-Z*Y(1,I))/D12	DINT1550
	Z=(U(2,I)-Z*U(1,I))/ZH	DINT1560
	GG(3,I)=(H*W-D1*Z)/D123	DINT1570
40	GG(4,I)=(Z-W)/D123	DINT1580
	M=1	DINT1590
	IF (L.EQ.1) M=0	DINT1600
	CALL DZP(N,X,GG,E,H,M)	DINT1610
	IF (L.EQ.NDINT.OR.NPRT(26).NE.0) CALL OUTPUT(0)	DINT1620
	IF (L.EQ.NDINT) K = 4	DINT1630
	CALL PDAUX(X,DER,M,K)	DINT1640
44	IF (L.NE.NDINT.AND.NPRT(26).NE.0) CALL OUTPUT(1)	DINT1650
C		DINT1660
C	TEST FOR CONVERGENCE	DINT1670
C		DINT1680
	IF (K.LT.0) GO TO 47	DINT1690
	DO 46 II=1,N,3	DINT1700
	IF (XTEST(II).LE.0.0) GO TO 46	DINT1710
	TE = 0.0	DINT1720
	TT = 0.0	DINT1730
	I2 = II+2	DINT1740
	DO 45 I=II,I2	DINT1750
	Z=GG(5,I)*(X(I)-GG(1,I))+GG(2,I)+H*(GG(3,I)+H*GG(4,I))	DINT1760
	TE = TE+(DER(I)-Z)**2	DINT1770
45	TT = TT+DER(I)**2	DINT1780
	IF (NPRT(25).NE.0) WRITE (6,48) T,II,TT,TE,(XTEST(I),I=II,I2)	DINT1790
	IF (TT.LT.XTEST(II)) GO TO 46	DINT1800
	IF (XTEST(II+1).GT.0.0 .AND. TE.LT.XTEST(II+1)) GO TO 46	DINT1810
	IF (TE.GE.XTEST(II+2)*TT) GO TO 47	DINT1820
46	CONTINUE	DINT1830
C		DINT1840
C	CONVERGENCE SUCCESSFUL	DINT1850
C		DINT1860
	GO TO 60	DINT1870
C		DINT1880
C	CONVERGENCE FAILED, TEST TO DIVIDE H.	DINT1890
C		DINT1900
47	IF (NPRT(25).EQ.0) WRITE (6,48) T,II,TT,TE,(XTEST(I),I=II,I2)	DINT1910
48	FORMAT('0 DINT CONV. TEST',F10.6,I6,5G16.8)	DINT1920
	WRITE (6,49) T,H	DINT1930
49	FORMAT('0 TEST FAILED AT TIME =',F10.6,' FOR H =',F10.6)	DINT1940
	ICNT = 0	DINT1950
	IF (H.LE.HMIN) GO TO 61	DINT1960
	IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT1970
	T = T-H	DINT1980
	H = H*0.5	DINT1990
	K = 2	DINT2000

```

      GO TO 5
60 IF (H.GT.0.74*HPRINT) ICNT = ICNT+1
61 DO 63 I=1,N
      F(1,I) = X(I)
      F(2,I) = DER(I)
      F(3,I) = GG(3,I) +2.0*H*GG(4,I)
      F(4,I) = GG(4,I)
63 F(5,I) = GG(5,I)
      IF(ICNT.LT.IDBL) GO TO 65
      ICNT = 0
      H = H*2.0
      IF (H.GT.HMAX) H=HMAX
      HPRINT = 2.0*HPRINT
      IF (HPRINT.GT.HMAX) HPRINT = HMAX
65 CALL UPDATE(2)
      CALL OUTPUT(1)
      IF (TPRINT-T.GE.EPS8) GO TO 4
      CALL ELTIME(2,3)
      RETURN
      END

```

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DINT2010
DINT2020
DINT2030
DINT2040
DINT2050
DINT2060
DINT2070
DINT2080
DINT2090
DINT2100
DINT2110
DINT2120
DINT2130
DINT2140
DINT2150
DINT2160
DINT2170
DINT2180
DINT2190
DINT2200

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	SUBROUTINE ELTIME(L,N)	ELTI0010
		REV 12 12/19/74
C	COUNTS THE NUMBER OF TIMES CERTAIN BASIC SUBROUTINES ARE CALLED	ELTI0020
C	AND ACCOUNTS FOR ALL COMPUTER CPU TIME USED BY THESE ROUTINES.	ELTI0030
C		ELTI0040
C	ARGUMENTS L: 1 INDICATES CALL IS AT START OF ROUTINE	ELTI0050
C	2 INDICATES CALL IS AT END OF ROUTINE.	ELTI0060
C	N: THE SUBROUTINE IDENTIFICATION NUMBER.	ELTI0070
C		ELTI0080
C	ASSUMES FUNCTION LTIME(I) IS GIVING ELAPSED CPU TIME IN INTEGER	ELTI0090
C	UNITS OF 0.01 SECONDS SINCE FUNCTION LTIME(0) WAS CALLED.	ELTI0100
C		ELTI0110
C	COMMON/GBTIME/NT(40),MTIN(40),NC(40),IND(40),NSUB	ELTI0120
	REAL*8 SUB(40)/	ELTI0130
	* 8H MAIN3D ,8H INPUT ,8H DINT ,8H PRIPLT ,8H DZP ,	ELTI0140
	* 8H PDAUX ,8H UPDATE ,8H OUTPUT ,8H DAUX ,8H SETUP1 ,	ELTI0150
	* 8H CHAIN ,8H CONTCT ,8H VISPR ,8H DAUX11 ,8H DAUX12 ,	ELTI0160
	* 8H DAUX22 ,8H DAUX31 ,8H DAUX32 ,8H DAUX33 ,8H FSMSOL ,	ELTI0170
	* 8H PLELP ,8H BELTRT ,8H SEGSEG ,8H AIRBAG ,8H RSTART ,	ELTI0180
	* 8H SETUP2 ,8H IMPULS ,8H IMPLS2 ,8H AIRBG3 ,8H DAUX55 ,	ELTI0190
	* 8H EJOINT ,8H SPDAMP ,8H DAUX44 ,8H FLXSEG ,8H WINDY ,	ELTI0200
	* 8H HBELT ,8H ,8H ,8H ,8H ,8H /	ELTI0210
	IF (N.GT.1) GO TO 20	ELTI0220
	IF (L.GT.1) GO TO 40	ELTI0230
C		ELTI0240
C	INITIAL CALL AT BEGINNING OF MAIN PROGRAM.	ELTI0250
C		ELTI0260
	MTIN(I) = LTIME(0)	ELTI0270
	DO 11 I=1,40	ELTI0280
	IND(I) = 0	ELTI0290
	NC(I) = 0	ELTI0300
	MTIN(I) = -1	ELTI0310
11	NT(I) = 0	ELTI0320
	NSUB = 1	ELTI0330
	IND(I) = 1	ELTI0340
	NC(I) = 1	ELTI0350
	MTIN(I) = 0	ELTI0360
	GO TO 99	ELTI0370
C		ELTI0380
C	CALL AT BEGINNING OF NTH SUBROUTINE.	ELTI0390
C		ELTI0400
	20 IF (L.GT.1) GO TO 30	ELTI0410
	MTIN(N) = LTIME(I)	ELTI0420
	IF (NC(N).NE.0) GO TO 21	ELTI0430
	NSUB = NSUB+1	ELTI0440
	IND(NSUB) = N	ELTI0450
21	NC(N) = NC(N)+1	ELTI0460
	GO TO 99	ELTI0470
C		ELTI0480
C	CALL AT END OF NTH SUBROUTINE.	ELTI0490
		ELTI0500

C	30	MTOUT = LTIME(1)	ELTI0510
		NDIFF = MTOUT-MTIN(N)	ELTI0520
		MTIN(N) = -1	ELTI0530
		IF (NDIFF.EQ.0) GO TO 32	ELTI0540
		NT(N) = NT(N) + NDIFF	ELTI0550
		DO 31 I=1,40	ELTI0560
		IF (MTIN(I).NE.-1) MTIN(I) = MTIN(I) + NDIFF	ELTI0570
	31	CONTINUE	ELTI0580
	32	GO TO 99	ELTI0590
C			ELTI0600
C		SUBSEQUENT CALLS FROM MAIN PROGRAM, PRINT SUMMARY TABLE.	ELTI0610
C			ELTI0620
	40	NTSUM = LTIME(1)	ELTI0630
		NT(1) = NTSUM - MTIN(1)	ELTI0640
		TIME = FLOAT(NTSUM)/100.0	ELTI0650
		WRITE (6,41) TIME	ELTI0660
	41	FORMAT('1 ELAPSED CPU TIME =',F10.2,' SECONDS'//	ELTI0670
		* ' SUB CALLS TIME % '//)	ELTI0680
		PCSUM = 0.0	ELTI0690
		NTSUM = 0	ELTI0700
		DO 42 I=1,NSUB	ELTI0710
		J = IND(I)	ELTI0720
		PC = FLOAT(NT(J))/TIME	ELTI0730
		PCSUM = PCSUM + PC	ELTI0740
		NTSUM = NTSUM + NT(J)	ELTI0750
	42	WRITE (6,43) SUB(J),NC(J),NT(J),PC	ELTI0760
	43	FORMAT(A10,2I10,F10.2)	ELTI0770
		WRITE (6,44) NTSUM,PCSUM	ELTI0780
	44	FORMAT('0TOTAL',14X,I10,F10.2)	ELTI0790
	99	RETURN	ELTI0800
		END	ELTI0810
			ELTI0820



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C      DOUBLE PRECISION FUNCTION EVALFD (D,N,L)                                EVAL0010
C                                                                                   REV 10 09/26/74EVAL0020
C      EVALUATE FUNCTION THAT IS DEFINED AT LOCATION N OF TAB ARRAY              EVAL0030
C      FOR ABSCISSA VALUE D.  EVALUATES DERIVATIVE, FUNCTION OR INTEGRAL        EVAL0040
C      AS L EQUALS 0, 1, OR 2.  TAB ARRAY IS DEFINED AS FOLLOWS:                EVAL0050
C      TAB(N)      -  D0 (D0 MUST BE NON-NEGATIVE)                             EVAL0060
C      TAB(N+1)    -  D1 (F1 DEFINED FOR D0 < D < D1)                         EVAL0070
C      TAB(N+2)    -  D2 (F2 DEFINED FOR D1 < D < D2)                         EVAL0080
C      TAB(N+3)    -  (NOT CURRENTLY USED)                                     EVAL0090
C      TAB(N+4)    -  (NOT CURRENTLY USED)                                     EVAL0100
C      TAB(N+5)    -  START OF DEFINITION OF 1ST PART OF FUNCTION (F1)         EVAL0110
C      WHICH IS FOLLOWED BY DEFINITION OF 2ND PART OF FUNCTION (F2),             EVAL0120
C      IF ANY.                                                                    EVAL0130
C      2ND PART OF FUNCTION EXISTS IF D2 IS NON-ZERO.                          EVAL0140
C      SIGN OF D1 DETERMINES FORM OF DEFINITION FOR 1ST PART OF                EVAL0150
C      THE FUNCTION.                                                              EVAL0160
C                                                                               EVAL0170
C      D1 ZERO INDICATES THAT FUNCTION IS CONSTANT D2 FOR ALL D.               EVAL0180
C                                                                               EVAL0190
C      D1 POSITIVE INDICATES THAT TAB(N+5)-TAB(N+10) CONTAINS                  EVAL0200
C      A0,A1,...A5.  THE COEFFICIENTS OF A 5TH ORDER POLYNOMIAL.              EVAL0210
C                                                                               EVAL0220
C      D1 NEGATIVE INDICATES THAT TAB(N+5) CONTAINS NP (REAL)                 EVAL0230
C      FOLLOWED BY  D(1), F(1), D(2), F(2) ..., D(NP), F(NP)                   EVAL0240
C                                                                               EVAL0250
C      WARNING- TABULAR FUNCTION MUST BE DEFINED FOR WHOLE RANGE,              EVAL0260
C      THAT IS, FROM D0 TO D1 INCLUSIVE,OR D1 TO D2 INCLUSIVE.                 EVAL0270
C                                                                               EVAL0280
C                                                                               EVAL0290
C      SIMILARLY, THE SIGN OF D2 (IF NON-ZERO) DETERMINES FORM OF              EVAL0300
C      DEFINITION OF 2ND PART OF FUNCTION, IF ANY.                             EVAL0310
C                                                                               EVAL0320
C                                                                               EVAL0330
C      IF D < D0      FUNCTION = 0                                              EVAL0340
C      IF D > |D1|    AND  D2=0      FUNCTION = F1(|D1|)                        EVAL0350
C      IF D > |D2|    AND  D2#0      FUNCTION = F2(|D2|)                        EVAL0360
C                                                                               EVAL0370
C      IMPLICIT REAL*8(A-H,O-Z)                                                EVAL0380
C      COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)      EVAL0390
C      F = 0.0                                                                    EVAL0400
C      IOUTR = 0                                                                    EVAL0410
C      D0 = TAB(N)                                                                    EVAL0420
C      IF (D.LT.D0) GO TO 40                                                        EVAL0430
C      D1 = TAB(N+1)                                                                    EVAL0440
C      D2 = TAB(N+2)                                                                    EVAL0450
C      IF (D1.NE.0.0) GO TO 26                                                        EVAL0460
C      IF (L-1) 40,24,25                                                            EVAL0470
24  F = D2                                                                    EVAL0480
    GO TO 40                                                                    EVAL0490
25  F= (D-D0)*D2                                                                EVAL0500

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GO TO 40	EVAL0510
C	EVAL0520
C COMPUTE INDEX OF F1 DEFINITION	EVAL0530
C	EVAL0540
26 NP = N+5	EVAL0550
IF (L.EQ.2) GO TO 41	EVAL0560
C	EVAL0570
C DERIVATIVES AND FUNCTIONS HERE, INTEGRALS HAVE OTHER LOGIC	EVAL0580
C	EVAL0590
IF (D.LT.DABS(D1)) GO TO 31	EVAL0600
IF (D2.NE.0.0) GO TO 32	EVAL0610
C	EVAL0620
C D .GE.  D1  , D2 = 0	EVAL0630
C	EVAL0640
30 IF (D1.LE.0.0) GO TO 33	EVAL0650
C	EVAL0660
C IOUTR.EQ.1 INDICATES D BEYOND RANGE. DERIVATIVE = 0.	EVAL0670
C IOUTR.EQ.0 INDICATES D.LE.  D1 . COMPUTE POLY DERIVATIVE	EVAL0680
C	EVAL0690
IF (D.GT.DABS(D1)) IOUTR = 1	EVAL0700
X = D1	EVAL0710
GO TO 37	EVAL0720
C	EVAL0730
C D0 < D <  D1	EVAL0740
C	EVAL0750
31 IF (D1.LT.0.0) GO TO 35	EVAL0760
X = D	EVAL0770
GO TO 37	EVAL0780
C	EVAL0790
C D .GE.  D1 , D2 NON-ZERO, USE F2	EVAL0800
C	EVAL0810
32 MP = 6	EVAL0820
C	EVAL0830
C COMPUTE INDEX OF F2 DEFINITION	EVAL0840
C	EVAL0850
IF (D1.LT.0.0) MP = 2.0 * TAB(NP)+1.0	EVAL0860
NP = NP+MP	EVAL0870
IF (D.LT.DABS(D2)) GO TO 34	EVAL0880
29 IF (D2.LT.0.0) GO TO 33	EVAL0890
C	EVAL0900
C IOUTR.EQ.1 INDICATES D BEYOND RANGE. DERIVATIVE = 0.	EVAL0910
C IOUTR.EQ.0 INDICATES D.LE.  D2 . COMPUTE POLY DERIVATIVE	EVAL0920
C	EVAL0930
IF (D.GT.DABS(D2)) IOUTR = 1	EVAL0940
C	EVAL0950
C D .GE. D2 (POSITIVE), EVALUATE F2 FOR D2	EVAL0960
C	EVAL0970
X = D2	EVAL0980
GO TO 37	EVAL0990
C	EVAL1000

C	D EXCEEDS TABULAR DEFINITION, SET F = F(NP)	EVAL1010
C	IF TABLE DEFINITION EXTENDS BEYOND RANGE, USE TABLE VALUES	EVAL1020
C		EVAL1030
	33 MB = TAB(NP)	EVAL1040
	NB = NP+MB+MB	EVAL1050
	IF (D .LE. TAB(NB-1)) GO TO 35	EVAL1060
	IF (L.EQ.1) F=TAB(NB)	EVAL1070
	GO TO 40	EVAL1080
C		EVAL1090
C	D1  .LE. D <  D2	EVAL1100
C		EVAL1110
	34 IF (D2.LT.0.0) GO TO 35	EVAL1120
	X = D	EVAL1130
	GO TO 37	EVAL1140
C		EVAL1150
C	EVALUATE F FROM TABULAR DEFINITION	EVAL1160
C		EVAL1170
	35 MB = TAB(NP)	EVAL1180
	K1 = NP+3	EVAL1190
	K2 = NP+MB+MB	EVAL1200
	DO 36 K=K1,K2,2	EVAL1210
	IF (D.GT.TAB(K)) GO TO 36	EVAL1220
	IF (L-1) 28,27,40	EVAL1230
C		EVAL1240
C	EVALUATE DERIVATIVE FROM TABLE	EVAL1250
C		EVAL1260
	28 F = (TAB(K+1)-TAB(K-1))/(TAB(K)-TAB(K-2))	EVAL1270
	GO TO 40	EVAL1280
C		EVAL1290
C	EVALUATE FUNCTION FROM TABLE	EVAL1300
C		EVAL1310
	27 R2 = TAB(K)-TAB(K-2)	EVAL1320
	R1 = (D-TAB(K-2))/R2	EVAL1330
	R2 = (TAB(K)-D)/R2	EVAL1340
	F = R1*TAB(K+1)+R2*TAB(K-1)	EVAL1350
	GO TO 40	EVAL1360
	36 CONTINUE	EVAL1370
	IF (L.EQ.1) F = TAB(K2)	EVAL1380
	GO TO 40	EVAL1390
	37 IF (IOUTR.EQ.1 .AND. L.EQ.0 ) GO TO 40	EVAL1400
	IF (L-1) 38,39,40	EVAL1410
C		EVAL1420
C	EVALUATE DERIVATIVE OF 5TH DEGREE POLYNOMIAL	EVAL1430
C		EVAL1440
	38 F = TAB(NP+1)+X*(2.0*TAB(NP+2)+X*(3.0*TAB(NP+3)+X*(4.0*TAB(NP+4)+	EVAL1450
	* X*5.0*TAB(NP+5)))	EVAL1460
	GO TO 40	EVAL1470
C		EVAL1480
C	EVALUATE 5TH DEGREE POLYNOMIAL	EVAL1490
C		EVAL1500

39	F =	TAB(NP) + X*(TAB(NP+1)+X*(TAB(NP+2)	EVAL1510
	*	+X*(TAB(NP+3)+X*(TAB(NP+4)+X*TAB(NP+5))))	EVAL1520
	GO TO	40	EVAL1530
C			EVAL1540
C	L=2:	COMPUTE INTEGRAL OF FUNCTION FROM D0 TO D.	EVAL1550
C			EVAL1560
41	IF (D.EQ.D0)	GO TO 40	EVAL1570
	X0 =	D0	EVAL1580
	X1 =	D1	EVAL1590
	DO 50	I=1,2	EVAL1600
	IF (X1)	43,49,42	EVAL1610
42	A0 =	TAB(NP)	EVAL1620
	A1 =	TAB(NP+1)/2.0	EVAL1630
	A2 =	TAB(NP+2)/3.0	EVAL1640
	A3 =	TAB(NP+3)/4.0	EVAL1650
	A4 =	TAB(NP+4)/5.0	EVAL1660
	A5 =	TAB(NP+5)/6.0	EVAL1670
	NP =	NP+6	EVAL1680
	X =	X0	EVAL1690
	IF (X.NE.0.0)	F=F-X*(A0+X*(A1+X*(A2+X*(A3+X*(A4+X*A5))))	EVAL1700
	X =	DMIN1(D,X1)	EVAL1710
	IF (X.NE.0.0)	F=F+X*(A0+X*(A1+X*(A2+X*(A3+X*(A4+X*A5))))	EVAL1720
	IF (D.LE.X1)	GO TO 40	EVAL1730
	IF (I.EQ.1.AND.D2.NE.0.0)	GO TO 49	EVAL1740
C			EVAL1750
C	NOTE -	NP WAS UPDATED NP=NP+6 BEFORE THIS, READY FOR SECOND PASS	EVAL1760
C			EVAL1770
	F = F +	(D-X1)*(TAB(NP-6)+X1*(TAB(NP-5)+X1*(TAB(NP-4)	EVAL1780
	*	+X1*(TAB(NP-3)+X1*(TAB(NP-2)+X1*TAB(NP-1))))	EVAL1790
	GO TO	40	EVAL1800
43	MB =	TAB(NP)	EVAL1810
	K1 =	NP+3	EVAL1820
	K2 =	NP+MB+MB	EVAL1830
	NP =	K2+1	EVAL1840
	DL =	DMIN1(D,DABS(X1))	EVAL1850
	DO 44	K=K1,K2,2	EVAL1860
	IF (X0.GE.TAB(K))	GO TO 44	EVAL1870
	Z1 =	DMAX1(X0,TAB(K-2))	EVAL1880
	Z2 =	DMIN1(DL,TAB(K))	EVAL1890
	FYX =	TAB(K-1)*TAB(K) - TAB(K+1)*TAB(K-2)	EVAL1900
	FY =	TAB(K+1) - TAB(K-1)	EVAL1910
	F = F +	(FYX + 0.5*FY*(Z1+Z2)) *(Z2-Z1)/ (TAB(K)-TAB(K-2))	EVAL1920
	IF (Z2.NE.DL)	GO TO 44	EVAL1930
	IF (I.EQ.1.AND.D2.NE.0.0)	GO TO 49	EVAL1940
	IF (Z2. EQ. D)	GO TO 40	EVAL1950
	F = F +	(D-Z2)*(FYX+Z2*FY)/ (TAB(K)-TAB(K-2))	EVAL1960
	GO TO	40	EVAL1970
44	CONTINUE		EVAL1980
49	X0 =	DABS(D1)	EVAL1990
50	X1 =	D2	EVAL2000

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40 EVALFD = F  
  RETURN  
  END
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EVAL2010  
EVAL2020  
EVAL2030
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C          SUBROUTINE FINPUT                                FINP0010
C                                                     REV 12 12/18/74FINP0020
C          CONTROLS CARD INPUT SPECIFYING THE ALLOWED CONTACTS OF THE CRASH FINP0030
C          VICTIM BODY SEGMENTS WITH VEHICLE PANELS, BELTS, AIRBAGS AND OTHERFINP0040
C          BODY SEGMENTS ALONG WITH THE ASSOCIATED FUNCTIONS TO BE USED FOR FINP0050
C          EACH CONTACT. FINP0060
C          ALSO SETS UP TABLES TO CONTROL TIME HISTORY INFORMATION FOR FINP0070
C          EACH FUNCTION FOR EACH ALLOWED CONTACT. FINP0080
C                                                     FINP0090
C          IMPLICIT REAL*8(A-H,O-Z) FINP0100
C          COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40) FINP0110
C          COMMON/JBARTZ/ MNPL( 20),MNBLT( 8),MNSEG( 22),MNBAG( 6), FINP0120
C          *          MPL(3,5,20),MBLT(3,5,8),MSEG(3,5,22),MBAG(3,10,6), FINP0130
C          *          NTPL(5,20),NTBLT(5,8),NTSEG(5,22) FINP0140
C          COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000) FINP0150
C          COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),BLTTTL(5,8)FINP0160
C          *          ,PLTTL(5,20),BAGTTL(5,6),SEG(22),JOINT(21) FINP0170
C          *          ,CGS(21),JS(21) FINP0180
C          REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT FINP0190
C          LOGICAL*1 CGS,JS FINP0200
C          COMMON/CSTRNT/A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24) FINP0210
C          *          ,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12) FINP0220
C          *          ,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12) FINP0230
C          *          ,NQ,KQ1(12),KQ2(12),KQTYPE(12) FINP0240
C          COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42) FINP0250
C          *          ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63) FINP0260
C          *          ,VISC(7,63),JNT(21),IPIN(21),MS,ISING(22) FINP0270
C          *          ,IGLOB(21),JOINTF(21) FINP0280
C          COMMON/CEULER/ IEULER(22),HIR(3,3,21),ANG(3,21),ANGD(3,21), FINP0290
C          *          FE(3,21),TQE(3,31),CONST(3,21) FINP0300
C          COMMON/KALEPS/WTIME(30),IWIND(30),MWSEG(5,22) FINP0310
C          COMMON/TEMPVS/JTITL(5,51),NF(5),NS(3),KTITL(31) FINP0320
C          REAL BLANK /'  ' /,JTITL,KTITL FINP0330
C          REAL SURFCE(2,3) /'  PL ', 'ANE ', ' BE ', 'LT ', ' SEG ', 'MENT' / FINP0340
C          MXNTI = 50 FINP0350
C          J1 = MXTB1+1 FINP0360
C                                                     FINP0370
C          INPUT ALLOWED CONTACTS AND FUNCTIONS BY REF. NO. FINP0380
C                                                     FINP0390
C          NT = 1 FINP0400
C          WRITE (6,31) FINP0410
C          31 FORMAT('1 ALLOWED CONTACTS AND ASSOCIATED FUNCTIONS') FINP0420
C          DO 61 I=1,4 FINP0430
C          IJK = 0 FINP0440
C          GO TO (32,34,35,36),I FINP0450
C          32 IF (NPL.LE.0) GO TO 61 FINP0460
C                                                     FINP0470
C          INPUT NO. OF SEGMENTS TO CONTACT EACH PLANE. FINP0480
C          INPUT CARD F.1.A FINP0490
C                                                     FINP0500

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	READ (5,33) (MNPL(J),J=1,NPL)	FINP0510
33	FORMAT(18I4)	FINP0520
	NJJ = NPL	FINP0530
	GO TO 37	FINP0540
34	IF (NBLT.LE.0) GO TO 61	FINP0550
C		FINP0560
C	INPUT NO. OF SEGMENTS TO CONTACT EACH BELT.	FINP0570
C	INPUT CARD F.2.A	FINP0580
C		FINP0590
	READ (5,33) (MNBLT(J),J=1,NBLT)	FINP0600
	NJJ = NBLT	FINP0610
	GO TO 37	FINP0620
35	IF (NSEG.LE.0) GO TO 61	FINP0630
C		FINP0640
C	INPUT NO. OF SEGMENTS TO CONTACT EACH SEGMENT.	FINP0650
C	INPUT CARD F.3.A	FINP0660
C		FINP0670
	READ (5,33) (MNSEG(J),J=1,NSEG)	FINP0680
	NJJ = NSEG	FINP0690
	GO TO 37	FINP0700
36	IF (NJNT.LE.0) GO TO 61	FINP0710
C		FINP0720
C	INPUT CARD F.4.A	FINP0730
C	SUPPLY IGLOB(J)=1 FOR EACH GLOBALGRAPHIC JOINT J=1,NJNT	FINP0740
C		FINP0750
	READ (5,33) (IGLOB(J),J=1,NJNT)	FINP0760
	NJJ = NJNT	FINP0770
C		FINP0780
C	START OF LOOP TO READ CONTACTS FOR PLANES (I=1), BELTS (I=2),	FINP0790
C	SEGMENTS (I=3) AND FUNCTIONS FOR GLOBALGRAPHIC JOINTS (I=4).	FINP0800
C		FINP0810
37	DO 60 J=1,NJJ	FINP0820
	IF (I.EQ.1) NK = MNPL(J)	FINP0830
	IF (I.EQ.2) NK = MNBLT(J)	FINP0840
	IF (I.EQ.3) NK = MNSEG(J)	FINP0850
	IF (I.EQ.4) NK = IGLOB(J)	FINP0860
	IF (NK.LE.0) GO TO 60	FINP0870
	DO 59 K=1,NK	FINP0880
	IF (IJK.EQ.0) WRITE (6,38) I	FINP0890
38	FORMAT('0',119X,'CARDS F.',I1)	FINP0900
	IF (IJK.EQ.0 .AND. I.NE.4) WRITE (6,39) SURFCE(1,I),SURFCE(2,I)	FINP0910
39	FORMAT('0',3X,2A4,8X,'SEGMENT',2X,'FORCE DEFLECTION',6X,'INERTIAL	FINP0920
	*SPIKE',10X,'R FACTOR',13X,'G FACTOR',10X,'FRICTION COEF.')	FINP0930
	IF (IJK.EQ.0 .AND. I.EQ.4) WRITE (6,40)	FINP0940
40	FORMAT('0',5X,'JOINT (GLOBALGRAPHIC)',2X,'TORQUE DEFLECTION',6X,'HF	FINP0950
	*ERRON FORMULA',10X,'R FACTOR',13X,'G FACTOR',10X,'FRICTION COEF.')	FINP0960
	IJK = 1	FINP0970
C		FINP0980
C	INPUT CONTACT SURFACE NO., SEGMENT NO., AND FUNCTION NOS.	FINP0990
C	INPUT CARD F.(I).(K)	FINP1000

C	READ (5,33) NJ,NS,NF	FINP1010
	WRITE (6,41) NJ,NS,NF	FINP1020
41	FORMAT('0',I7,'-',I3,I11,'-',I3,I8,4I21)	FINP1030
	IF (NJ.NE.J) WRITE (6,42)	FINP1040
42	FORMAT(' FINPUT INPUT ERROR. PROGRAM TERMINATED.')	FINP1050
	IF (NJ.NE.J) STOP	FINP1060
	NLT = 1	FINP1070
	DO 43 JJ = 1,31	FINP1080
43	KTITLE(JJ) = BLANK	FINP1090
	GO TO (44,46,48,49),I	FINP1100
C		FINP1110
C	PLACE SEGMENT NO. AND INDEX TO NTAB ARRAY INTO M- AND NT- ARRAYS.	FINP1120
C		FINP1130
44	MPL(1,K,J) = NS(1)	FINP1140
	MPL(2,K,J) = NS(2)	FINP1150
	MPL(3,K,J) = NS(3)	FINP1160
	NTPL(K,J) = NT	FINP1170
	DO 45 JJ = 1,5	FINP1180
45	KTITLE(JJ) = PLTTL (JJ,J)	FINP1190
	GO TO 50	FINP1200
46	MBLT(1,K,J) = NS(1)	FINP1210
	MBLT(2,K,J) = NS(2)	FINP1220
	MBLT(3,K,J) = NS(3)	FINP1230
	NTBLT(K,J) = NT	FINP1240
	DO 47 JJ = 1,5	FINP1250
47	KTITLE(JJ) = BLTTTL (JJ,J)	FINP1260
C		FINP1270
C	SET UP TWO TABLES FOR FULL BELT FRICTION	FINP1280
C		FINP1290
	IF (NF(5).NE.0) NLT = 2	FINP1300
	GO TO 50	FINP1310
48	MSEG(1,K,J) = NS(1)	FINP1320
	MSEG(2,K,J) = NS(2)	FINP1330
	MSEG(3,K,J) = NS(3)	FINP1340
	NTSEG(K,J) = NT	FINP1350
	KTITLE (3) = SEG(J)	FINP1360
	GO TO 50	FINP1370
C		FINP1380
C	NOTE: GLOBALGRAPHIC JOINT WILL SAVE NT IN IGLOB ARRAY	FINP1390
C		FINP1400
49	IGLOB(J) = NT	FINP1410
	KTITLE(2) = JOINT(J)	FINP1420
C		FINP1430
C	SET UP POINTERS TO TAB ARRAY IN NTAB ARRAY.	FINP1440
C		FINP1450
50	NFJ = NS(2)	FINP1460
	IF (NFJ.GT.0) KTITLE(6) = SEG(NFJ)	FINP1470
	DO 52 JJ = 1,5	FINP1480
	IF (NF(JJ).LE.0) GO TO 52	FINP1490
		FINP1500

NFJ = NF(JJ)	FINP1510
DO 51 KK = 1,5	FINP1520
KJ = 5*JJ+KK+1	FINP1530
51 KTITLE(KJ) = JTITLE(KK,NFJ)	FINP1540
52 CONTINUE	FINP1550
WRITE (6,53) KTITLE	FINP1560
53 FORMAT(1X,5A4,1X,A4,5(1X,5A4))	FINP1570
DO 58 NL = 1,NLT	FINP1580
NTAB(NT) = J1	FINP1590
NT = NT+1	FINP1600
DO 56 L=1,5	FINP1610
NX = NF(L)	FINP1620
NTAB(NT) = 0	FINP1630
IF (NX.EQ.0) GO TO 55	FINP1640
NTAB(NT) = NTI(NX)	FINP1650
IF (NTI(NX).NE.0) GO TO 56	FINP1660
WRITE(6,54) NX	FINP1670
54 FORMAT ('0 FUNCTION NO.',I4,' HAS NOT BEEN DEFINED. PROGRAM TERMINATED.')	FINP1680
STOP	FINP1690
55 IF (L.NE.1) GO TO 56	FINP1700
	FINP1710
IF FORCE DEFLECTION FUNCTION NO. IS ZERO,	FINP1720
SET UP FOR ROLLING CONSTRAINT	FINP1730
	FINP1740
NQ = NQ+1	FINP1750
NTAB(NT) = -NQ	FINP1760
KQTYPE(NQ) = -4	FINP1770
KQ1(NQ) = NS(2)	FINP1780
KQ2(NQ) = NS(1)	FINP1790
IF (I.NE.3) GO TO 56	FINP1800
KQ1(NQ) = J	FINP1810
KQ2(NQ) = NS(2)	FINP1820
56 NT = NT+1	FINP1830
	FINP1840
INITIALIZE TAB ARRAY TO ZERO EXCEPT FOR DMAX, DINER, FDMAX.	FINP1850
	FINP1860
J2 = J1+19	FINP1870
DO 57 JJ=J1,J2	FINP1880
57 TAB(JJ) = 0.0	FINP1890
NX = NTAB(NT-5)	FINP1900
IF (NX.LT.0) GO TO 58	FINP1910
TAB(J1+8) = DABS(TAB(NX+1))	FINP1920
IF (TAB(NX+2).NE.0.0) TAB(J1+8) = DABS(TAB(NX+2))	FINP1930
TAB(J1+10) = EVALFD(TAB(J1+8),NX,1)	FINP1940
NX = NTAB(NT-4)	FINP1950
IF (NX.LE.0) GO TO 58	FINP1960
TAB(J1+9) = DABS(TAB(NX+1))	FINP1970
IF (TAB(NX+2).NE.0.0) TAB(J1+9) = DABS(TAB(NX+2))	FINP1980
58 J1 = J2+1	FINP1990
	FINP2000

59	CONTINUE	FINP2010
60	CONTINUE	FINP2020
61	CONTINUE	FINP2030
	MXNT8 = NT-I	FINP2040
	MXTB2 = J1-1	FINP2050
	IF (MXTB2.GT.2000) WRITE (6,62) MXTB2	FINP2060
62	FORMAT('O ERROR IN SUBROUTINE FINPUT, SIZE OF TAB ARRAY =',I8//	FINP2070
	* ' PROGRAM TERMINATED')	FINP2080
	IF (MXTB2.GT.2000) STOP	FINP2090
C		FINP2100
C	INPUT CARD F.5 - JOINT FUNCTIONS TO BE USED.	FINP2110
C		FINP2120
	IF (NJNT.LE.0) GO TO 81	FINP2130
	READ (5,33) (JOINTF(J),J=I,NJNT)	FINP2140
	IJK = 0	FINP2150
	DO 80 J=1,NJNT	FINP2160
	IF (JOINTF(J).EQ.0) GO TO 80	FINP2170
	IF (IJK.EQ.0) WRITE (6,77)	FINP2180
77	FORMAT('1',119X,'CARD F.5'/	FINP2190
	* ' THE FOLLOWING JOINT RESTORING FORCE FUNCTIONS AS DEFINED	FINP2200
	*ON CARDS E.7 WILL BE USED.'//4X,'JOINT',10X,'FUNCTION'//)	FINP2210
	JF = JOINTF(J)	FINP2220
	IJK = 1	FINP2230
	WRITE (6,78) J,JOINT(J),JF,(JTITLE(I,JF),I=1,5)	FINP2240
78	FORMAT(I6,'-',A4,I10,'-',5A4)	FINP2250
	IF (NTI(JF).EQ.0) WRITE (6,42)	FINP2260
	IF (NTI(JF).EQ.0) STOP	FINP2270
80	CONTINUE	FINP2280
C		FINP2290
C	INPUT CONTACT SEGMENTS FOR AIRBAG, IF ANY.	FINP2300
C		FINP2310
81	IF (NBAG.LE.0) GO TO 69	FINP2320
	IJK = 0	FINP2330
	DO 68 J=1,NBAG	FINP2340
C		FINP2350
C	INPUT CARD F.6.(J)	FINP2360
C		FINP2370
	READ (5,63) K,NK,(MBAG(2,I,J),MBAG(3,I,J),I=1,NK)	FINP2380
63	FORMAT(2I4,20I2)	FINP2390
	MNBAG(J) = NK	FINP2400
	IF (NK.EQ.0) GO TO 68	FINP2410
	IF (IJK.EQ.0) WRITE (6,64)	FINP2420
64	FORMAT(///5X,'AIRBAG',4X,'VS.',4X,'SEGMENTS',90X,'CARDS F.6')	FINP2430
	IF (K.NE.J) WRITE (6,42)	FINP2440
	IF (K.NE.J) STOP	FINP2450
	WRITE (6,65) J,(MBAG(2,I,J),MBAG(3,I,J),I=1,NK)	FINP2460
65	FORMAT('O NO.',I2,12X,I0(I3,'-',I3))	FINP2470
	DO 66 I=1,NK	FINP2480
	K = MBAG(2,I,J)	FINP2490
66	KTITLE(I) = SEG(K)	FINP2500

WRITE (6,67) (BAGTTL(I,J),I=1,5),(KTITLE(I),I=1,NK)	FINP2510
67 FORMAT(1X,5A4,10(3X,A4))	FINP2520
68 CONTINUE	FINP2530
C INPUT CARDS F.7.A-F.7.B FOR SUBROUTINE WINDY.	FINP2540
C	FINP2550
C	FINP2560
69 READ (5,33) (MWSEG(1,J),J=1,NSEG)	FINP2570
IPAGE = 0	FINP2580
DO 73 J=1,NSEG	FINP2590
IWIND(J) = 0	FINP2600
WTIME(J) = 0.0	FINP2610
IF (MWSEG(1,J).EQ.0) GO TO 73	FINP2620
IF (IPAGE.EQ.0) WRITE (6,70)	FINP2630
70 FORMAT('1 SEGMENT WIND FORCES',99X,'CARDS F.7'//	FINP2640
* ' SEGMENT-ELLIPSOID SEGMENT-PLANE',	FINP2650
* 17X,'WIND FORCE FUNCTION')	FINP2660
IPAGE = 1	FINP2670
READ (5,33) (MWSEG(I,J),I=1,5)	FINP2680
WRITE (6,71) (MWSEG(I,J),I=1,5)	FINP2690
71 FORMAT('0',I7,' -',I3,I14,' -',I3,I30)	FINP2700
IF (MWSEG(1,J).NE.J) WRITE (6,42)	FINP2710
IF (MWSEG(1,J).NE.J) STOP	FINP2720
M3 = MWSEG(3,J)	FINP2730
M4 = MWSEG(4,J)	FINP2740
M5 = MWSEG(5,J)	FINP2750
WRITE (6,72) SEG(J),SEG(M3),(PLTTL(I,M4),I=1,5)	FINP2760
* , (JTITLE(I,M5),I=1,5)	FINP2770
72 FORMAT(5X,A4,15X,A4,' -',5A4,2X,5A4)	FINP2780
73 CONTINUE	FINP2790
RETURN	FINP2800
END	FINP2810



	SUBROUTINE FLXSEG	FLXS0010
		REV 12 10/25/74FLXS0020
	IMPLICIT REAL*8(A-H,O-Z)	FLXS0030
	COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)	FLXS0040
	* ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)	FLXS0050
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8),NFLX	FLXS0060
	COMMON/CNSNTS/ PI, RADIANT,G,THIRD,EPS1,EPS4,EPS6,EPS8,	FLXS0070
	* EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)	FLXS0080
	COMMON/TEMPVS/ TT(3,3), THN(4), CN1(3,3), CN(3,3), WNM1(3),	FLXS0090
	* THND(4), PTD(3), WCSN(3), RHSN(3), RHS1(3),	FLXS0100
	* RHS2(3), GF(3,4), GC(3,3), CGC(3,3), THA(3),	FLXS0110
	* THAD(3), THADEG(3), DN2N1(3,3), RMG(3)	FLXS0120
	IF (NFLX.EQ.0) GO TO 99	FLXS0130
	CALL ELTIME(1,34)	FLXS0140
	IFX = 1	FLXS0150
11	N1 = NFLEX(1,IFX)	FLXS0160
	N3 = NFLEX(3,IFX)	FLXS0170
	CALL DOTT(D(1,1,N3),D(1,1,N1),TT,3,3,3)	FLXS0180
	THN(1) = DATAN2(TT(1,2),TT(1,1))	FLXS0190
	THN(2) = -DARSIN(TT(1,3))	FLXS0200
	THN(3) = DATAN2(TT(2,3),TT(3,3))	FLXS0210
	THN(4) = 1.0	FLXS0220
	CT22 = 1.0-TT(1,3)**2	FLXS0230
	CT2 = DSQRT(CT22)	FLXS0240
	ST2 = -TT(1,3)	FLXS0250
	CT1 = TT(1,1)/CT2	FLXS0260
	ST1 = TT(1,2)/CT2	FLXS0270
	CN1(1,1) = -TT(1,1)*TT(1,3)/CT22	FLXS0280
	CN1(1,2) = -TT(1,2)*TT(1,3)/CT22	FLXS0290
	CN1(1,3) = 1.0	FLXS0300
	CN1(2,1) = -ST1	FLXS0310
	CN1(2,2) = CT1	FLXS0320
	CN1(2,3) = 0.0	FLXS0330
	CN1(3,1) = TT(1,1)/CT22	FLXS0340
	CN1(3,2) = TT(1,2)/CT22	FLXS0350
	CN1(3,3) = 0.0	FLXS0360
	CALL DOT(TT,WMEG(1,N3),WNM1,3,1,3)	FLXS0370
	DO 12 I=1,3	FLXS0380
12	WNM1(I) = WNM1(I) - WMEG(I,N1)	FLXS0390
	CALL MAT(CN1,WNM1,THND,3,3,1,3,3,3)	FLXS0400
	THND(4) = 0.0	FLXS0410
	CALL CROSS(WMEG(1,N1),WNM1,WCSN)	FLXS0420
	RHSN(1) = ( (-THND(1)*ST1*ST2 + THND(2)*CT1/CT2)*WNM1(1)	FLXS0430
	* +( THND(1)*CT1*ST2 + THND(2)*ST1/CT2)*WNM1(2) )/CT2	FLXS0440
	RHSN(2) = -THND(1)*(CT1*WNM1(1) + ST1*WNM1(2))	FLXS0450
	RHSN(3) = ( (-THND(1)*ST1 + THND(2)*CT1*ST2/CT2)*WNM1(1)	FLXS0460
	* +( THND(1)*CT1 + THND(2)*ST1*ST2/CT2)*WNM1(2) )/CT2	FLXS0470
13	N2 = NFLEX(2,IFX)	FLXS0480
	M = 0	FLXS0490
	DO 15 I=1,3	FLXS0500





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      RHS1(2) = RHS1(2) + THAD(1)*(CN(1,2)*RHS2(2)+CN(2,2)*CSC*RHS2(3)) FLXS1010
*      + THAD(2)*CN(1,2)*CSS*RHS2(3) FLXS1020
      RHS1(3) = RHS1(3) - THAD(2)*CSC*RHS2(3) FLXS1030
      CALL MAT(GF, RHSN, RHS2, 3,3,1,3,3,3) FLXS1040
      M = 1 FLXS1050
      DO 30 I=1,3 FLXS1060
      CALL MAT(HF(1,M,IFX), THND, PTD, 3,3,1,4,3,3) FLXS1070
      RHS2(I) = RHS2(I) + XDY(PTD,CN1,WNM1) FLXS1080
30  M = M+4 FLXS1090
      CALL MAT(CN, RHS2, PTD, 3,3,1,3,3,3) FLXS1100
      DO 35 I=1,3 FLXS1110
35  RHS1(I) = RHS1(I) + PTD(I) FLXS1120
      CALL DOT(D(1,1,N1),RHS1,V4(1,IFX),3,1,3) FLXS1130
      IF (IFX.EQ.NFLX) GO TO 98 FLXS1140
      IFX = IFX+1 FLXS1150
      IF (NFLEX(1,IFX).EQ.N1 .AND. NFLEX(3,IFX).EQ.N3) GO TO 13 FLXS1160
      GO TO 11 FLXS1170
98  CALL ELTIME(2,34) FLXS1180
99  RETURN FLXS1190
      END FLXS1200

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C      DOUBLE PRECISION FUNCTION FINTERP(THETA,PHI,NT)                                FNT00010
C                                                                                   REV 12 12/06/74 FNT00020
C      COMPUTES THE RESTORING TORQUE OF A JOINT AS A FUNCTION OF THE                FNT00030
C      FLEXURE ANGLE (THETA) AND THE AZIMUTH ANGLE (PHI) AS DEFINED BY              FNT00040
C      FUNCTION NO. NT                                                              FNT00050
C                                                                                   FNT00060
C      ASSUMES  C < THETA < PI                                                    FNT00070
C              -PI < PHI < PI                                                    FNT00080
C              DATA IN TAB ARRAY CONTAINS NTHETA,NPHI FOLLOWED BY                FNT00090
C              TWO DIMENSIONAL ARRAY OF FUNCTIONAL VALUES (NTHETA > 0)          FNT00100
C              OR POLYNOMIAL COEFFICIENTS (NTHETA < 0) FOR EQUALLY                FNT00110
C              SPACED VALUES OF PHI.                                             FNT00120
C                                                                                   FNT00130
C              THETA(I) = (I-1)*PI/(NTHETA-1) FOR I=1,NTHETA                    FNT00140
C              PHI(J) = -PI + (J-1)*2*PI/NPHI FOR J=1,NPHI                      FNT00150
C              F(THETA,PI) = F(THETA,-PI)                                       FNT00160
C                                                                                   FNT00170
C      SUBROUTINE EVALUATES G1(THETA) = F(THETA,PHI(J) )                        FNT00180
C              G2(THETA) = F(THETA,PHI(J+1))                                    FNT00190
C              FOR PHI(J) < PHI < PHI(J+1)                                       FNT00200
C      BY LINEAR INTERPOLATION OR POLYNOMIAL EVALUATION AND THEN LINEAR          FNT00210
C      INTERPOLATES BETWEEN G1 AND G2 TO OBTAIN F(THETA,PHI).                  FNT00220
C      IF F < 0, F IS SET TO ZERO, THEREFORE A DEAD BAND IS OBTAINED            FNT00230
C      BY NEGATIVE VALUES IN THE TABLE.                                       FNT00240
C                                                                                   FNT00250
C      IMPLICIT REAL*8 (A-H,O-Z)                                                FNT00260
C      COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS1,EPS4,EPS6,EPS8,                    FNT00270
C      *      EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3) FNT00280
C      COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NT1(50),NTAB(500),TAB(2000) FNT00290
C      IERROR = 0                                                                FNT00300
C      IF (PHI.LT.-PI) IERROR = 1                                                FNT00310
C      IF (PHI.GT. PI) IERROR = 2                                                FNT00320
C      IF (THETA.LT.0.0) IERROR = 3                                              FNT00330
C      IF (THETA.GT.PI) IERROR = 4                                              FNT00340
C      IF (IERROR.NE.0) WRITE (6,11) IERROR,THETA,PHI,NT                      FNT00350
11 11 FORMAT('0 IMPROPER ARGUMENTS TO FUNCTION FINTERP. ERROR CODE =',I4/ FNT00360
C      *      '0 THETA =',G25.15, ' PHI =',G25.15,' NT =',I6) FNT00370
C      IF (IERROR.NE.0) STOP                                                    FNT00380
C      NF = NT1(NT) + 5                                                         FNT00390
C      NTHETA = TAB(NF)                                                         FNT00400
C      NPHI   = TAB(NF+1)                                                       FNT00410
C                                                                                   FNT00420
C      DETERMINE INDEX AND INTERPOLATION PARAMETERS FOR PHI.                   FNT00430
C                                                                                   FNT00440
C      XNP = (PHI+PI)/(2.0*PI)*TAB(NF+1)                                       FNT00450
C      NP1 = XNP                                                                FNT00460
C      NP2 = NP1+1                                                              FNT00470
C      IF (NP2.GE.NPHI) NP2 = 0                                                 FNT00480
C      RP2 = XNP - DFLOAT(NP1)                                                  FNT00490
C      RP1 = 1.0 - RP2                                                         FNT00500

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	NTH = IABS(NTHETA)	FNTE0510
	IP1 = NF+1+NP1*NTH	FNTE0520
	IP2 = NF+1+NP2*NTH	FNTE0530
C		FNTE0540
C	DETERMINE INDEX AND INTERPOLATION PARAMETERS FOR THETA.	FNTE0550
C		FNTE0560
	IF (NTHETA.LT.0) GO TO 20	FNTE0570
	XNT = THETA/PI*(TAB(NF)-1.0)	FNTE0580
	NT1 = XNT	FNTE0590
	RT2 = XNT - DFLOAT(NT1)	FNTE0600
	RT1 = 1.0 - RT2	FNTE0610
	IT1 = IP1 + NT1	FNTE0620
	IT2 = IP2 + NT1	FNTE0630
	G1 = RT1*TAB(IT1+1) + RT2*TAB(IT1+2)	FNTE0640
	G2 = RT1*TAB(IT2+1) + RT2*TAB(IT2+2)	FNTE0650
	GO TO 23	FNTE0660
C		FNTE0670
C	COMPUTE FOR POLYNOMIALS IN THETA FOR FIXED PHI.	FNTE0680
C		FNTE0690
	20 NPOLY = -NTHETA-1	FNTE0700
	IT1 = IP1 + NPOLY + 2	FNTE0710
	IT2 = IP2 + NPOLY + 2	FNTE0720
	THETA1 = THETA - TAB(IP1+1)	FNTE0730
	THETA2 = THETA - TAB(IP2+1)	FNTE0740
	G1 = 0.0	FNTE0750
	G2 = 0.0	FNTE0760
	DO 21 I=1,NPOLY	FNTE0770
	IT1 = IT1-1	FNTE0780
	IT2 = IT2-1	FNTE0790
	G1 = THETA1*(TAB(IT1)+G1)	FNTE0800
	21 G2 = THETA2*(TAB(IT2)+G2)	FNTE0810
	23 FNTERP = RP1*G1 + RP2*G2	FNTE0820
	IF (FNTERP.LT.0.0) FNTERP = 0.0	FNTE0830
	RETURN	FNTE0840
	END	FNTE0850

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C          SUBROUTINE HBELT(NSECT,IBAR,BAR,NT,XLONG)
C
C          REV 12 12/19/74
C          COMPUTES THE FORCES AND TORQUES OF INDIVIDUAL BELT SECTIONS AND
C          ADDS THEM TO THE U1 AND U2 ARRAYS FOR CONTACTING SEGMENTS.
C          ARGUMENTS:
C          NSECT      - NO. OF REFERENCE POINTS ON BELT
C          IBAR(1,J)  - SEGMENT NO. ASSOCIATED WITH POINT J
C          (2,J)      - ELLIPSOID NO. (J=1,NSECT)
C          BAR (1,J)  - INPUT REFERENCE POINT
C          (4,J)      - CONTACT POINT
C          NT         - INDEX TO FORCE DEFLECTION FUNCTION
C          XLONG      - REFERENCE LENGTH
C
C          IMPLICIT REAL*8(A-H,O-Z)
C          DIMENSION BAR(6,10),IBAR(2,10)
C          COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)
C          COMMON/VPOSTN/TIME
C          COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
C          *          ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
C          COMMON/CNTRSRF/ PL(17,20),GAB(8,3),BELT(20,8),TPTS(6,8),BD(24,25)
C          COMMON/TEMPVS/T1(3),T2(3),T3(3),T4(3),T5(3),T6(3),T7(3),T8(3),
C          *          ZNR(3),ZW(3,101),ZY(3,100),DS(100),JF(101)
C          CALL ELTIME(1,36)
C          LL = 0
C          DO 20 K=1,NSECT
C
C          COMPUTE ZW(K) - THE LOCATION OF POINT(K) IN INERTIAL REFERENCE.
C
C          KK = IBAR(1,K)
C          CALL DOT(D(1,1,KK),BAR(4,K),T1,3,1,3)
C          DO 11 J=1,3
C          11  ZW(J,K) = SEGLP(J,KK) + T1(J)
C             IF (K.EQ.1) GO TO 20
C             LL = LL+1
C          12  JJ = JF(LL)
C
C          COMPUTE VECTOR ZY(LL) AND LENGTH DS(LL) FOR BELT SECTION LL
C          BETWEEN POINTS K=JF(LL+1) AND JJ=JF(LL).
C
C          DSS = 0.0
C          DO 13 J=1,3
C          ZY(J,LL) = ZW(J,K) - ZW(J,JJ)
C          13  DSS = DSS + ZY(J,LL)**2
C             DS(LL) = DSQRT(DSS)
C             IF (LL.EQ.1) GO TO 20
C
C          COMPUTE DPR - DOT PRODUCT BETWEEN ZY(LL) AND ZY(LL-1)
C
C          KK = IBAR(1,JJ)
C          MM = IBAR(2,JJ)

```



	IF (MM.EQ.0) GO TO 20	HBEL0510
	DO 14 J=1,3	HBEL0520
14	T2(J) = BAR(J+3,JJ) - BD(J+3,MM)	HBEL0530
	CALL MAT(BD(7,MM),T2,T3,3,3,1,3,3,3)	HBEL0540
	CALL DOT(D(1,1,KK),T3,ZNR,3,1,3)	HBEL0550
	DPR = 0.0	HBEL0560
	DO 15 J=1,3	HBEL0570
15	DPR = DPR + ZNR(J)*(ZY(J,LL)/DS(LL) - ZY(J,LL-1)/DS(LL-1))	HBEL0580
	IF (DPR.LT.0.0) GO TO 20	HBEL0590
C		HBEL0600
C	POSITIVE DPR INDICATES BELT IS PULLING AWAY FROM POINT JJ. REMOVE	HBEL0610
C	POINT FROM FUTURE CONSIDERATION AND DECREASE LL - NO. OF LENGTHS.	HBEL0620
C		HBEL0630
	LL = LL-1	HBEL0640
	GO TO 12	HBEL0650
20	JF(LL+1) = K	HBEL0660
C		HBEL0670
C	COMPUTE XLG - TOTAL LENGTH OF THE LL BELT SECTIONS.	HBEL0680
C		HBEL0690
	XLG = 0.0	HBEL0700
	DO 30 L=1,LL	HBEL0710
30	XLG = XLG + DS(L)	HBEL0720
C		HBEL0730
C	NEGATIVE XLONG INDICATES INITIAL SLACK IN BELT.	HBEL0740
C		HBEL0750
	IF (XLONG.LT.0.0) XLONG = XLG-XLONG	HBEL0760
C		HBEL0770
C	COMPUTE FRC - TOTAL FORCE OF BELT AND APPLY IT TO ALL SEGMENTS.	HBEL0780
C		HBEL0790
	STRAIN = (XLG-XLONG)/XLONG	HBEL0800
	FRC = FRCDFL(STRAIN,NT,1)	HBEL0810
	IF (FRC.LE.0.0) GO TO 99	HBEL0820
	IF (NPRT(16).NE.0) WRITE (6,31) TIME,XLG,STRAIN,FRC,LL	HBEL0830
31	FORMAT('O SUB HBELT',F13.6,3G18.7,16)	HBEL0840
	DO 40 L=1,LL	HBEL0850
	L1 = JF(L)	HBEL0860
	L2 = JF(L+1)	HBEL0870
	K1 = 1BAR(1,L1)	HBEL0880
	K2 = 1BAR(1,L2)	HBEL0890
	CALL MAT(D(1,1,K1),ZY(1,L),T4,3,3,1,3,3,3)	HBEL0900
	CALL MAT(D(1,1,K2),ZY(1,L),T5,3,3,1,3,3,3)	HBEL0910
	CALL CROSS(BAR(4,L1),T4,T6)	HBEL0920
	CALL CROSS(BAR(4,L2),T5,T7)	HBEL0930
	FR = FRC/DS(L)	HBEL0940
	IF (NPRT(16).NE.0) WRITE (6,32) L1,K1,K2,DS(L),FR,(ZY(J,L),J=1,3)	HBEL0950
32	FORMAT(6X,316,5G18.7)	HBEL0960
	DO 40 J=1,3	HBEL0970
	U1(J,K1) = U1(J,K1) + FR*ZY(J,L)	HBEL0980
	U2(J,K1) = U2(J,K1) + FR*T6(J)	HBEL0990
	U1(J,K2) = U1(J,K2) - FR*ZY(J,L)	HBEL1000



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40 U2(J,K2) = U2(J,K2) - FR*T7(J)
99 CALL ELTIME(2,36)
   RETURN
   END
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HBEL1010
HBEL1020
HBEL1030
HBEL1040
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	SUBROUTINE HINPUT	HINP0010
		REV 12 12/19/74HINP0020
C	CONTROLS THE INPUT OF CARDS F.8.A - F.8.D CONTAINING THE SETUP AND	HINP0030
C	CONTROL OF THE HARNESS BELT SYSTEM.	HINP0040
C		HINP0050
C		HINP0060
	IMPLICIT REAL*8(A-H,O-Z)	HINP0070
	COMMON/HARNESS/ BAR(6,100) , XLONG(20), IBAR(2,100), NTHRNS(20),	HINP0080
	* NHRNSS, NBLTPH(5), NFBLT(5,20), NPTSPB(20)	HINP0090
	COMMON/TEMPVS/JTITL(5,51),NF(5),NS(3),KTITL(31)	HINP0100
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)	HINP0110
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),BLTTTL(5,8)	HINP0120
	* ,PLTTL(5,20),BAGTTL(5,6),SEG(22),JOINT(21)	HINP0130
	* ,CGS(21),JS(21)	HINP0140
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTL,PLTTL,BAGTTL,SEG,JOINT	HINP0150
	LOGICAL*1 CGS,JS	HINP0160
C		HINP0170
C	INPUT CARD F.8.A	HINP0180
C	NHRNSS - NO. OF HARNESS-BELT SYSTEMS	HINP0190
C	NBLTPH - NO. OF BELTS PER HARNESS	HINP0200
C		HINP0210
	READ (5,11) NHRNSS,(NBLTPH(I),I=1,NHRNSS)	HINP0220
	11 FORMAT(18I4)	HINP0230
	IF (NHRNSS.LE.0) GO TO 99	HINP0240
	WRITE (6,12) NHRNSS,(NBLTPH(I),I=1,NHRNSS)	HINP0250
	12 FORMAT('1 HARNESS-BELT SYSTEM INPUT',93X,'CARDS F.8'//	HINP0260
	* ' NO. OF HARNESSES =' ,I4//	HINP0270
	* ' NO. OF BELTS PER HARNESS =' ,5I6)	HINP0280
	J1 = 1	HINP0290
	K1 = 1	HINP0300
	JJ1 = MXTB2 + 1	HINP0310
	NT = MXNTB + 1	HINP0320
	DO 90 I=1,NHRNSS	HINP0330
	IF (NBLTPH(I).LE.0) GO TO 90	HINP0340
	J2 = J1 + NBLTPH(I) -1	HINP0350
C		HINP0360
C	INPUT CARD F.8.B - NPTSPB - NO. OF POINTS PER BELT.	HINP0370
C		HINP0380
	READ (5,11) (NPTSPB(J),J=J1,J2)	HINP0390
	WRITE (6,13) I,(NPTSPB(J),J=J1,J2)	HINP0400
	13 FORMAT('0 FOR HARNESS NO.',I3,' NO. OF POINTS PER BELT =' ,20I4)	HINP0410
	DO 80 J=J1,J2	HINP0420
	IF (NPTSPB(J).EQ.0) GO TO 80	HINP0430
C		HINP0440
C	INPUT CARD F.8.C - 5 FUNCTION NOS AND LENGTH OF EACH BELT.	HINP0450
C		HINP0460
	READ (5,14) (NFBLT(L,J),L=1,5),XLONG(J)	HINP0470
	14 FORMAT(5I4,F12.6)	HINP0480
	WRITE (6,15) I,J,(NFBLT(L,J),L=1,5),XLONG(J)	HINP0490
	15 FORMAT('0 HARNESS NO.',I3,' BELT NO.',I3,' FUNCTION NOS.',5I6,	HINP0500

	*	' REFERENCE LENGTH =' ,G16.8///	HINP0510
	*	' HARNESS BELT POINT SEGMENT ELLIPSOID ',	HINP0520
	*	9X,'REFERENCE POINT' /	HINP0530
	*	3X,'NO.',5X,'NO.',3X,'NO.',5X,'NO.',5X,'NO.',6X,	HINP0540
	*	6X,'X',9X,'Y',9X,'Z',3X / )	HINP0550
C			HINP0560
C		CHANGE SIGN OF XLONG FOR INITIAL CALL TO HBELT.	HINP0570
C			HINP0580
		XLONG(J) = -XLONG(J)	HINP0590
C			HINP0600
C		SET UP POINTERS IN NTAB AND INITIAL VALUES OF TAB FOR BELT J	HINP0610
C		AS WAS DONE FOR OTHER CONTACTS IN SUBROUTINE FINPUT.	HINP0620
C			HINP0630
		NTHRNS(J) = NT	HINP0640
		NTAB(NT) = JJ1	HINP0650
		NT = NT+1	HINP0660
		DO 17 L=1,5	HINP0670
		NTAB(NT) = 0	HINP0680
		NX = NFBLT(L,J)	HINP0690
		IF (NX.EQ.0) GO TO 17	HINP0700
		NTAB(NT) = NTI(NX)	HINP0710
		IF (NTI(NX).GT.0) GO TO 17	HINP0720
		WRITE (6,16) NX	HINP0730
	16	FORMAT('0 FUNCTION NO.',I4,' HAS NOT BEEN DEFINED.',	HINP0740
	*	' PROGRAM TERMINATED.')	HINP0750
		STOP	HINP0760
	17	NT = NT+1	HINP0770
		JJ2 = JJ1+19	HINP0780
		DO 18 JJ=JJ1,JJ2	HINP0790
	18	TAB(JJ) = 0.0	HINP0800
		NX = NTAB(NT-5)	HINP0810
		IF (NX.LT.0) GO TO 19	HINP0820
		TAB(JJ1+8) = DABS(TAB(NX+1))	HINP0830
		IF (TAB(NX+2).NE.0.0) TAB(JJ1+8) = DABS(TAB(NX+2))	HINP0840
		TAB(JJ1+10) = EVALFD(TAB(JJ1+8),NX,1)	HINP0850
		NX = NTAB(NT-4)	HINP0860
		IF (NX.LE.0) GO TO 19	HINP0870
		TAB(JJ1+9) = DABS(TAB(NX+1))	HINP0880
		IF (TAB(NX+2).NE.0.0) TAB(JJ1+9) = DABS(TAB(NX+2))	HINP0890
	19	JJ1 = JJ2+1	HINP0900
		K2 = K1 + NPTSPB(J) - 1	HINP0910
		DO 70 K=K1,K2	HINP0920
C			HINP0930
C		INPUT CARD F.8.D	HINP0940
C			HINP0950
		READ (5,21) (IBAR(L,K),L=1,2),(BAR(L,K),L=1,3)	HINP0960
		WRITE (6,22) I,J,K,(IBAR(L,K),L=1,2),(BAR(L,K),L=1,3)	HINP0970
	21	FORMAT(2I6,3F12.6)	HINP0980
	22	FORMAT(I5,I8,I6,2I8,7X,3F10.3)	HINP0990
		DO 23 L=1,3	HINP1000

23 BAR(L+3,K) = BAR(L,K)	HINP1010
70 CONTINUE	HINP1020
K1 = K2+1	HINP1030
80 CONTINUE	HINP1040
J1 = J2+1	HINP1050
90 CONTINUE	HINP1060
MXNTB = NT-1	HINP1070
MXTB2 = JJ1-1	HINP1080
IF (MXTB2.GT.2000) WRITE (6,62) MXTB2	HINP1090
62 FORMAT('0 ERROR IN SUBROUTINE HINPUT, SIZE OF TAB ARRAY =',I8//	HINP1100
*          ' PROGRAM TERMINATED.')	HINP1110
IF (MXTB2.GT.2000) STOP	HINP1120
99 RETURN	HINP1130
END	HINP1140

	SUBROUTINE IMPULS(I1,I2,I3)	IMPUG010
		REV 12 10/25/74 IMPUG020
C	ARGUMENTS: I1 = 1 - IMPULS FOR PLELP.	IMPUG030
C	3 - IMPULS FOR SEGSEG.	IMPUG040
C	4 - IMPULS FOR VIS PR OR EJOINT	IMPUG050
C	I2 = INDEX OF CONTACTING SEGMENT OR JOINT AXIS	IMPUG060
C	I3 = PLANE, SEGMENT, OR JOINT NUMBER	IMPUG070
C		IMPUG080
C		IMPUG090
	IMPLICIT REAL*8 (A-H,O-Z)	IMPUG100
	COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)	IMPUG110
	COMMON/VPOSTN/ TIME,XU(3),XDOT(3),XCOMP(3),XVCOMP(3),AX(3),	IMPUG120
*	ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,	IMPUG130
*	NATAB,NACLR,DVEH(3,3),WMEG(3),WMEGD(3),XACOMP(3),	IMPUG140
*	THET(3),ZPLT(3)	IMPUG150
	COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)	IMPUG160
*	,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)	IMPUG170
	COMMON/CMATRX/V1(3,21),V2(3,21),V3(3,12),B12(3,3,42),A22(3,3,42)	IMPUG180
*	,F(3,21),TQ(3,21),WJ(21)	IMPUG190
	COMMON/DESCRP/ PH1(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)	IMPUG200
*	,HT(3,3,42),RPH1(3,22),RW(22),SPRING(5,63)	IMPUG210
*	,VISC(7,63),JNT(21),IP1N(21),NS,ISING(22)	IMPUG220
*	,IGLOB(21)	IMPUG230
	COMMON/JBARTZ/ MNPL( 20),MNBLT( 8),MNSEG( 22),MNBAG( 6),	IMPUG240
*	MPL(3,5,20),MBLT(3,5,8),MSEG(3,5,22),MBAG(3,10,6),	IMPUG250
*	NTPL(5,20),NTBLT(5,8),NTSEG(5,22)	IMPUG260
	COMMON/CSTRNT/A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24)	IMPUG270
*	,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12)	IMPUG280
*	,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12)	IMPUG290
*	,NQ,KQ1(12),KQ2(12),KQTYPE(12)	IMPUG300
	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8),NFLX	IMPUG310
	COMMON/TABLES/MXNT1,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)	IMPUG320
	COMMON/TEMPVI/ TT1(3),R11(3),R21(3),CREST,JSTUP(4,2,21)	IMPUG330
	DIMENSION TEMP(3),DWR1(3),DWR2(3),DWR3(3),DWR4(3),VREL(3),DV(3)	IMPUG340
	IF (TIME.EQ.0.0) GO TO 99	IMPUG350
		IMPUG360
C	SPECIAL SETUP FOR CALL TO SUBROUTINE DAUX	IMPUG370
C	REPLACE SETUP WITH U1,U2,V1,V2,V3 = 0.	IMPUG380
C	ASSUME OTHER ARRAYS FROM PREVIOUS CALL TO DAUX.	IMPUG390
C		IMPUG400
	CALL ELTIME(1,27)	IMPUG410
	CALL OUTPUT(0)	IMPUG420
	KQTEST = 0	IMPUG430
	NT = 0	IMPUG440
	IF (I1.EQ.1) NT = NTPL (I2,I3)	IMPUG450
	IF (I1.EQ.3) NT = NTSEG(I2,I3)	IMPUG460
	IF (NT.EQ.0) GO TO 29	IMPUG470
	KQ = -NTAB(NT+1)	IMPUG480
	IF (KQ.LE.0) GO TO 29	IMPUG490
	KQTYPE(KQ) = IABS(KQTYPE(KQ))	IMPUG500

CALL DAUX(0)	IMPU0510
29 IF (NQ.LE.0) GO TO 31	IMPU0520
DO 30 J=1,NQ	IMPU0530
DO 30 I=1,3	IMPU0540
30 V3(I,J) = 0.0	IMPU0550
31 DO 32 J=1,NSEG	IMPU0560
DO 32 I=1,3	IMPU0570
U1(I,J) = 0.0	IMPU0580
32 U2(I,J) = 0.0	IMPU0590
IF (NJNT.LE.0) GO TO 21	IMPU0600
DO 33 J=1,NJNT	IMPU0610
DO 33 I=1,3	IMPU0620
V1(I,J) = 0.0	IMPU0630
33 V2(I,J) = 0.0	IMPU0640
21 IF (NFLX.EQ.0) GO TO 23	IMPU0650
DO 22 J=1,NFLX	IMPU0660
DO 22 I=1,3	IMPU0670
22 V4(I,J) = 0.0	IMPU0680
C	IMPU0690
C	IMPU0700
C	IMPU0710
C	IMPU0720
23 IF (I1.NE.1) GO TO 34	IMPU0730
NT = NTPL(I2,I3)	IMPU0740
M1 = MPL(1,I2,I3)	IMPU0750
M2 = MPL(2,I2,I3)	IMPU0760
M3 = MPL(3,I2,I3)	IMPU0770
CALL PLELP(M2,M3,M1,I3,NT)	IMPU0780
IF (NTAB(NT+1).LT.0) GO TO 37	IMPU0790
K1 = M2	IMPU0800
K2 = M1	IMPU0810
GO TO 39	IMPU0820
34 IF (I1.NE.3) GO TO 35	IMPU0830
NT = NTSEG(I2,I3)	IMPU0840
M1 = MSEG(1,I2,I3)	IMPU0850
M2 = MSEG(2,I2,I3)	IMPU0860
M3 = MSEG(3,I2,I3)	IMPU0870
CALL SEGSEG(I3,M1,M2,M3,NT)	IMPU0880
IF (NTAB(NT+1).LT.0) GO TO 37	IMPU0890
K1 = I3	IMPU0900
K2 = M2	IMPU0910
GO TO 39	IMPU0920
35 IF (I1.NE.4) WRITE (6,36) I1,I2,I3	IMPU0930
36 FORMAT('G IMPROPER ARGUMENTS TO SUBROUTINE IMPULS'/	IMPU0940
* ' ARGUMENTS = ', 3I6 /	IMPU0950
* ' PROGRAM TERMINATED' )	IMPU0960
IF (I1.NE.4) STOP	IMPU0970
C	IMPU0980
C	IMPU0990
C	IMPU1000
RECALL VISPR FOR JOINT STOP.	



IF (IABS(IPIN(I3)).NE.4) GO TO 25	IMPU1010
CALL EJOINT(I2,I3)	IMPU1020
GO TO 26	IMPU1030
25 CALL VISPR(I2,I3)	IMPU1040
26 K1 = IABS(JNT(I3))	IMPU1050
K2 = I3+1	IMPU1060
GO TO 39	IMPU1070
C	IMPU1080
C SET UP SPECIAL U1,U2 FOR FIRST CONTACT OF CONSTRAINT.	IMPU1090
C	IMPU1100
37 KQ = -NTAB(NT+1)	IMPU1110
KQTEST = 1	IMPU1120
KQTYPE(KQ) = -IABS(KQTYPE(KQ))	IMPU1130
K1 = KQ1(KQ)	IMPU1140
K2 = KQ2(KQ)	IMPU1150
IF (K1.GT.NSEG) GO TO 38	IMPU1160
CALL MAT(A13(1,1,2*KQ-1),QQ(1,KQ),U1(1,K1),3,3,1,3,3,3)	IMPU1170
CALL MAT(A23(1,1,2*KQ-1),QQ(1,KQ),U2(1,K1),3,3,1,3,3,3)	IMPU1180
38 IF (K2.GT.NSEG) GO TO 39	IMPU1190
CALL MAT(A13(1,1,2*KQ ),QQ(1,KQ),U1(1,K2),3,3,1,3,3,3)	IMPU1200
CALL MAT(A23(1,1,2*KQ ),QQ(1,KQ),U2(1,K2),3,3,1,3,3,3)	IMPU1210
C	IMPU1220
C FINAL SETUP OF U1 AND U2	IMPU1230
C	IMPU1240
39 DO 40 J=1,NSEG	IMPU1250
DO 40 I=1,3	IMPU1260
U1(I,J) = U1(I,J)*RW(J)	IMPU1270
40 U2(I,J) = U2(I,J)*RPHI(I,J)	IMPU1280
DO 41 I=1,3	IMPU1290
SEGLA(I,NVEH) = 0.0	IMPU1300
41 WMEGD(I,NVEH) = 0.0	IMPU1310
CALL DAUX(I1)	IMPU1320
IF (KQTEST.EQ.1) KQTYPE(KQ) = IABS(KQTYPE(KQ))	IMPU1330
IF (NPRT(10).NE.0) CALL PRINT(6HPREIMP)	IMPU1340
IF (I1.GT.3) GO TO 51	IMPU1350
IF (NPRT(10).NE.0) WRITE (6,42) R11,R21	IMPU1360
42 FORMAT ('0'/(6G20.8))	IMPU1370
CALL CROSS(WMEG (1,K1),R11(1),TEMP)	IMPU1380
CALL DOT(D(1,1,K1),TEMP,DWR1(1),3,1,3)	IMPU1390
CALL CROSS(WMEG (1,K2),R21(1),TEMP)	IMPU1400
CALL DOT(D(1,1,K2),TEMP,DWR2(1),3,1,3)	IMPU1410
CALL CROSS(WMEGD(1,K1),R1I(1),TEMP)	IMPU1420
CALL DOT(D(1,1,K1),TEMP,DWR3(1),3,1,3)	IMPU1430
CALL CROSS(WMEGD(1,K2),R2I(1),TEMP)	IMPU1440
CALL DOT(D(1,1,K2),TEMP,DWR4(1),3,1,3)	IMPU1450
TVREL = 0.0	IMPU1460
TDV = 0.0	IMPU1470
DO 50 I=1,3	IMPU1480
VREL(I) = SEGLV(1,K1)+DWR1(I) - SEGLV(1,K2)-DWR2(I)	IMPU1490
DV (I) = SEGLA(1,K1)+DWR3(I) - SEGLA(1,K2)-DWR4(I)	IMPU1500

	TVREL = TVREL + TTI(1)*VREL(1)	IMPU1510
50	TDV = TDV + TTI(1)*DV (1)	IMPU1520
	GO TO 53	IMPU1530
51	CALL DOT(D(1,1,K1),WMEG (1,K1),DWR1(1),3,1,3)	IMPU1540
	CALL DOT(D(1,1,K2),WMEG (1,K2),DWR2(1),3,1,3)	IMPU1550
	CALL DOT(D(1,1,K1),WMEGD(1,K1),DWR3(1),3,1,3)	IMPU1560
	CALL DOT(D(1,1,K2),WMEGD(1,K2),DWR4(1),3,1,3)	IMPU1570
	TVREL = 0.0	IMPU1580
	TDV = 0.0	IMPU1590
	DO 52 I=1,3	IMPU1600
	VREL(1) = DWR1(1) - DWR2(1)	IMPU1610
	DV (1) = DWR3(1) - DWR4(1)	IMPU1620
	TVREL = TVREL + TTI(1)*VREL(1)	IMPU1630
52	TDV = TDV + TTI(1)*DV (1)	IMPU1640
53	ALPHA = 0.0	IMPU1650
C		IMPU1660
C	NOTE: CREST IS SUPPLIED AS (1+E)/2 WHERE E IS THE CLASSICAL	IMPU1670
C	COEFFICIENT OF RESTITUTION BUT WITH A RANGE OF -1 TO +1.	IMPU1680
C	CREST HAS A RANGE OF 0 TO +1 WHERE 0 (E=-1) REPRESENTS NO IMPULSE.	IMPU1690
C		IMPU1700
	IF (TDV.NE.0.0) ALPHA = -2.0*CREST*TVREL/TDV	IMPU1710
	IF (NPRT(10).NE.0) WRITE (6,42) DWR1,DWR2,DWR3,DWR4,	IMPU1720
	* TT1,VREL,DV,	IMPU1730
	* TVREL,TDV,CREST,ALPHA	IMPU1740
	DO 60 J=1,NSEG	IMPU1750
	DO 60 i=1,3	IMPU1760
	SEGLV(I,J) = SEGLV(I,J) + ALPHA*SEGLA(I,J)	IMPU1770
60	WMEG (I,J) = WMEG (I,J) + ALPHA*WMEGD(I,J)	IMPU1780
	CALL OUTPUT(1)	IMPU1790
	CALL PRINT(6HIMPULS)	IMPU1800
	CALL ELTIME(2,27)	IMPU1810
99	RETURN	IMPU1820
	END	IMPU1830

```

SUBROUTINE KINPUT                                     KINP0010
C                                                     REV 12 12/11/74 KINP0020
C PERFORMS THE FOLLOWING CARD INPUT AFTER CARDS E.1-E.4 (SUBROUTINE KINP0030
C CINPUT) AND BEFORE CARDS F.1-F.5 (SUBROUTINE FINPUT). KINP0040
C   CARD E.5 - NWINDF: NO. OF WIND FORCE FUNCTIONS ON CARDS E.6 KINP0050
C             - NJNTF : NO. OF JOINT FORCE FUNCTIONS ON CARDS E.7 KINP0060
C   CARDS E.6 - DEFINITIONS OF WIND FORCE FUNCTIONS KINP0070
C   CARDS E.7 - DEFINITIONS OF JOINT RESTORING FORCE FUNCTIONS KINP0080
C                                                     KINP0090
C   IMPLICIT REAL*8(A-H,O-Z) KINP0100
C   COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000) KINP0110
C   COMMON/TEMPVS/JTITL(5,51),NF(5),NS(3),KTITL(31),TH(50) KINP0120
C NOTE: TEMPVS IS SHARED HERE WITH SUBROUTINES CINPUT AND FINPUT. KINP0130
C   REAL BLANK/' ' /,JTITL,KTITL KINP0140
C   COMMON/CNSNTS/ PI, RADIANS,G,THIRD,EPS1,EPS4,EPS6,EPS8, KINP0150
C   * EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3) KINP0160
C                                                     KINP0170
C   INPUT CARD E.5 - NWINDF AND NJNTF KINP0180
C                                                     KINP0190
C   READ (5,11) NWINDF,NJNTF KINP0200
C   I1 FORMAT(2I6) KINP0210
C   J1 = MXTB1+1 KINP0220
C   IF (NWINDF.LE.0) GO TO 31 KINP0230
C   DO 30 K=I,NWINDF KINP0240
C                                                     KINP0250
C   INPUT CARD E.6.A - FUNCTION NO. AND TITLE KINP0260
C                                                     KINP0270
C   READ (5,12) I,(KTITL(J),J=1,5) KINP0280
C   I2 FORMAT(I4,4X,5A4) KINP0290
C   WRITE (6,13) I,(KTITL(J),J=1,5),I,J1 KINP0300
C   I3 FORMAT('1 WIND FORCE FUNCTION NO.',I4,4X,5A4,10X,'NTI(',I2,') =', KINP0310
C   * I5,43X,'CARDS E.6'//) KINP0320
C   IF (I.LE.0.OR.I.GT.50) WRITE (6,I4) KINP0330
C   I4 FORMAT('0 IMPROPER FUNCTION NO. PROGRAM TERMINATED.') KINP0340
C   IF (I.LE.0.OR.I.GT.50) STOP KINP0350
C   IF (NTI(I).NE.0) WRITE (6,15) I KINP0360
C   I5 FORMAT('0 FUNCTION NO.',I4,' HAS ALREADY BEEN INPUTTED AND WILL BE KINP0370
C   * REPLACED BY THIS FUNCTION.') KINP0380
C   NTI(I) = J1 KINP0390
C   DO I6 J=I,5 KINP0400
C   I6 JTITL(J,I) = KTITL(J) KINP0410
C   J2 = J1+4 KINP0420
C                                                     KINP0430
C   INPUT CARD E.6.B - DO THRU D4 (FOR NOW A BLANK CARD) KINP0440
C                                                     KINP0450
C   READ (5,I7) (TAB(J),J=J1,J2) KINP0460
C   WRITE (6,18) (TAB(J),J=J1,J2) KINP0470
C   I7 FORMAT(6F12.0) KINP0480
C   I8 FORMAT(10X,'D0',13X,'D1',13X,'D2',13X,'D3',13X,'D4'/5F15.4//) KINP0490
C   J1 = J2+1 KINP0500

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C		KINP0510
C	INPUT CARD E.6.C - NTMPTS	KINP0520
C		KINP0530
	READ (5,11) NTMPTS	KINP0540
	WRITE (6,19) NTMPTS	KINP0550
19	FORMAT('0 WIND FORCE TABLES FOR ',I6,' TIME POINTS.'//	KINP0560
*	11X,'T',14X,'FX(T)',15X,'FY(T)',15X,'FZ(T)' /)	KINP0570
	TAB(J1) = NTMPTS	KINP0580
	J1 = J1+1	KINP0590
	J2 = J1+4*NTMPTS-1	KINP0600
C		KINP0610
C	INPUT CARDS E.6.D-E.6.N - NTMPTS CARDS OF T,FX(T),FY(T),FZ(T)	KINP0620
C		KINP0630
	READ (5,20) (TAB(J),J=J1,J2)	KINP0640
	WRITE (6,21) (TAB(J),J=J1,J2)	KINP0650
20	FORMAT(4F12.0)	KINP0660
21	FORMAT(3X,F12.6,3G20.6)	KINP0670
	J1 = J2+1	KINP0680
30	CONTINUE	KINP0690
31	IF (NJNTF.LE.0) GO TO 51	KINP0700
	DO 50 K=1,NJNTF	KINP0710
C		KINP0720
C	INPUT CARD E.7.A - FUNCTION NO. AND TITLE	KINP0730
C		KINP0740
	READ (5,12) I,(KTITLE(J),J=1,5)	KINP0750
	WRITE (6,32) I,(KTITLE(J),J=1,5),I,J1	KINP0760
32	FORMAT('1 JOINT FORCE FUNCTION NO.',I4,4X,5A4,10X,'NTI(',I2,') ='	KINP0770
*	15,42X,'CARDS E.7'//)	KINP0780
	IF (I.LE.0.OR.1.GT.50) WRITE (6,14)	KINP0790
	IF (I.LE.0.OR.1.GT.50) STOP	KINP0800
	IF (NTI(I).NE.0) WRITE (6,15) I	KINP0810
	NTI(I) = J1	KINP0820
	DO 33 J=1,5	KINP0830
33	JTITLE(J,I) = KTITLE(J)	KINP0840
C		KINP0850
C	INPUT CARD E.7.B - D0,D1,D2,D3,D4 (FOR NOW A BLANK CARD).	KINP0860
C		KINP0870
	J2 = J1+4	KINP0880
	READ (5,17) (TAB(J),J=J1,J2)	KINP0890
	WRITE (6,18) (TAB(J),J=J1,J2)	KINP0900
	J1 = J2+1	KINP0910
C		KINP0920
C	INPUT CARD E.7.C - NTHETA,NPHI	KINP0930
C		KINP0940
	READ (5,11) NTHETA,NPHI	KINP0950
	TAB(J1) = NTHETA	KINP0960
	TAB(J1+1) = NPHI	KINP0970
	J1 = J1+2	KINP0980
	IF (NTHETA.LT.0) GO TO 38	KINP0990
	DO 35 J=1,NTHETA	KINP1000



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35 TH(J) = DFL0AT(J-1)*180.0/DFL0AT(NTHETA-1) KINP1010
   WRITE (6,36) NTHETA,NPH1,(TH(J),J=2,NTHETA) KINP1020
36 FORMAT('0 FUNCTION IS TABULAR FOR' ,13,' X',13,' VALUES OF THETA AKINP1030
   *ND PH1'//30X,'THETA'/5X,'PH1',5X,'THETA0',F16.3,4F20.3/ KINP1040
   * (15X,5F20.3)) KINP1050
37 FORMAT(F9.2,F10.3,5G20.7/(19X,5G20.7)) KINP1060
   GO TO 40 KINP1070
38 NPOLY = -NTHETA -1 KINP1080
   WRITE (6,39) NPOLY,NPH1,(BLANK,J,J=1,NPOLY) KINP1090
39 FORMAT('0 FUNCTION IS COEFFICIENTS OF' ,13,' ORDER POLYNOMIALS IN KINP1100
   *(THETA-THETA0) FOR',13,' VALUES OF PH1.'// KINP1110
   * 27X,'COEFFICIENTS OF (THETA-THETA0)**N'/ KINP1120
   * 5X,'PH1',5X,'THETA0',7X,5(A4,'N =' ,12,11X)/(26X,A4,'N =' ,12,11X,KINP1130
   * A4,'N =' ,12,11X,A4,'N =' ,12,11X,A4,'N =' ,12,11X,A4,'N =' ,12) ) KINP1140
40 WRITE (6,21) KINP1150
   DO 49 I=1,NPH1 KINP1160
   PH1DEG = DFL0AT(I-1)*360.0/DFL0AT(NPH1) - 180.0 KINP1170
C INPUT CARDS E.7.D - E.7.N NPH1 SETS WITH NTHETA ITEMS PER SET. KINP1180
C EACH SET 1 IS FOR PH1(1) = -180 +(1-1)*360/NPH1 DEGREES AND KINP1190
C ASSUMES DATA FOR PH1(NPH1+1) = 180 IS SAME AS PH1(1) = -180. KINP1200
C KINP1210
C KINP1220
   J2 = J1 + IABS(NTHETA) -1 KINP1230
   READ (5,17) (TAB(J),J=J1,J2) KINP1240
   WRITE (6,37) PH1DEG,(TAB(J),J=J1,J2) KINP1250
   IF (NTHETA.LT.0) TAB(J1) = TAB(J1)*RADIAN KINP1260
   IF (NTHETA.LT.0) GO TO 49 KINP1270
C KINP1280
C FOR TABULAR DATA, FILL IN ZERO VALUES WITH INTERPOLATED NEGATIVE KINP1290
C VALUES. OVERWRITE VALUE IN FIRST COLUMN (SUPPLIED AS THETA0) WITH KINP1300
C VALUE FOR THETA = 0 AND ALL OTHER ZERO VALUES. KINP1310
C KINP1320
   THETA0 = TAB(J1) KINP1330
   IF (THETA0.EQ.0.0) GO TO 49 KINP1340
   JJ = THETA0*DFL0AT(NTHETA-1)/180.0 + 1.0 + EPS6 KINP1350
   JJ1 = J1+JJ KINP1360
   IERROR = 0 KINP1370
   IF (JJ1.GT.J2) IERROR = 1 KINP1380
   IF (TAB(JJ1).LE.0.0) IERROR = 2 KINP1390
   IF (IERROR.NE.0) GO TO 46 KINP1400
   DO 45 J=1,JJ KINP1410
   J1J = J1+J-1 KINP1420
   IF (J.NE.1.AND.TAB(J1J).GT.0.0) IERROR = 3 KINP1430
45 TAB(J1J) = TAB(JJ1)*(TH(J)-THETA0)/(TH(JJ+1)-THETA0) KINP1440
46 IF (IERROR.NE.0) WRITE (6,47) IERROR KINP1450
47 FORMAT('0 INPUT ERROR. INCONSISTENT VALUE OF THETA0. IERROR =' ,12,KINP1460
   * ' PROGRAM TERMINATED.') KINP1470
   IF (IERROR.NE.0) STOP KINP1480
49 J1 = J2+1 KINP1490
50 CONTINUE KINP1500

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51 MXTB1 = J1-1  
RETURN  
END

KINP1510  
KINP1520  
KINP1530



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C          SUBROUTINE OUTPUT(IJK)
C
C          REV 12 12/17/74
C          CONTROLS TABULATED OUTPUT ON FORTRAN UNITS (STARTING WITH NO. 21)
C          OF SELECTED OPTIONAL SEGMENT LINEAR AND ANGULAR ACCELERATIONS,
C          VELOCITIES AND DISPLACEMENTS, JOINT PARAMETERS AND SELECTED DATA
C          FROM ALL ALLOWED CONTACT FORCE COMPUTATIONS BETWEEN BODY SEGMENTS
C          AND VEHICLE COMPONENTS.
C
C          IMPLICIT REAL*8 (A-H,O-Z)
C          COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)
C          COMMON/JBARTZ/ MNPL( 20),MNBLT( 8),MNSEG( 22),MNBAG( 6),
C          *          MPL(3,5,20),MBLT(3,5,8),MSEG(3,5,22),MBAG(3,10,6),
C          *          NTPL(5,20),NTBLT(5,8),NTSEG(5,22)
C          COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
C          *          ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
C          COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)
C          *          ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63)
C          *          ,VISC(7,63),JNT(21),IPIN(21),NS,ISING(22)
C          COMMON/CNSNTS/ PI, RADIANG,THIRD,EPS1,EPS4,EPS6,EPS8,
C          *          EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)
C          COMMON/VPOSTN/ TIME,XG(3),XDOTG(3),XCOMP(3),XVCOMP(3),AX(3),
C          *          ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,
C          *          NATAB,NACLR,DVEH(3,3),VMEG(3),VMEGD(3),XACOMP(3),
C          *          THET(3),ZPLT(3)
C          COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),
C          *          NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21)
C          COMMON/TEMPVS/ ACC(6,20),T1(3),T2(3),T3(3),T4(3)
C          COMMON/RSAVE/ XSG(3,20,3),NSG(7),MSG(20,7)
C          DATA LINES/0/,LPP/45/
C
C          IF (IJK.NE.0) GO TO 9
C
C          SET ALL FORCE ARRAYS TO ZERO.
C
C          DO 8 I=1,480
C          8 PSF(I,1) = 0.0
C          DO 7 J=1,NJNT
C          PRJNT(1,J) = 1.0
C          PRJNT(2,J) = 1.0
C          IF (IABS(IPIN(J)).EQ.4) PRJNT(1,J) = 0.0
C          IF (IABS(IPIN(J)).EQ.4) PRJNT(2,J) = 0.0
C          PRJNT(3,J) = 0.0
C          PRJNT(4,J) = 0.0
C          PRJNT(5,J) = 0.0
C          7 PRJNT(6,J) = 0.0
C          RETURN
C
C          9 CALL ELTIME(1,8)
C
C          INCREMENT LINE COUNT AND TEST FOR START OF NEW PAGE ON EACH UNIT.

```

C	LINES = LINES+1	OUTP0510
	IF (MOD(LINES,LPP).NE.1) GO TO 51	OUTP0520
	CALL HEDING(LINES,LPP,MPSF,MBSF,MSSF)	OUTP0530
C		OUTP0540
C	PRINT LINE OF DATA FOR THIS TIME POINT ON EACH OUTPUT UNIT (NT).	OUTP0550
C		OUTP0560
	51 USEC = 1000.0*TIME	OUTP0570
	NT = 2L	OUTP0580
C		OUTP0590
C	COMPUTE AND PRINT DATA FOR 7 TYPES OF OUTPUT ABOVE	OUTP0600
C		OUTP0610
	DO 68 K=1,7	OUTP0620
	IF (NSG(K).LE.0) GO TO 68	OUTP0630
	KSG = NSG(K)	OUTP0640
	J3 = 3	OUTP0650
	IF (K.EQ.7) J3 = 2	OUTP0660
	DO 67 J1=1,KSG,J3	OUTP0670
	J2 = MIN0(J1+J3-1,KSG)	OUTP0680
	NT = NT+1	OUTP0690
	DO 66 J=J1,J2	OUTP0700
	L = MSG(J,K)	OUTP0710
	GO TO (52,54,56,59,61,64,65),K	OUTP0720
C		OUTP0730
C	1. SEGMENT LINEAR ACCELERATIONS IN LOCAL REFERENCE	OUTP0740
C		OUTP0750
	52 CALL CROSS (WMEG(1,L),XSG(1,J,K),T1)	OUTP0760
	CALL CROSS (WMEG(1,L),T1,T2)	OUTP0770
	CALL CROSS (WMEGD(1,L),XSG(1,J,K),T3)	OUTP0780
	CALL MAT(D(1,1,L),SEGLA(1,L),T4,3,3,1,3,3,3)	OUTP0790
	DO 53 I=1,3	OUTP0800
	53 ACC(I,J) = (T4(I)+T3(I)+T2(I))/G	OUTP0810
	GO TO 63	OUTP0820
C		OUTP0830
C	2. SEGMENT LINEAR VELOCITIES IN VEHICLE REFERENCE	OUTP0840
C		OUTP0850
	54 CALL CROSS (WMEG(1,L),XSG(1,J,K),T1)	OUTP0860
	CALL DOT(D(1,1,L),T1,T2,3,1,3)	OUTP0870
	DO 55 I=1,3	OUTP0880
	55 T3(I) = SEGLV(I,L)+T2(I)-XVCOMP(I)	OUTP0890
	GO TO 58	OUTP0900
C		OUTP0910
C	3. SEGMENT LINEAR DISPLACEMENTS IN VEHICLE REFERENCE	OUTP0920
C		OUTP0930
	56 CALL DOT(D(1,1,L),XSG(1,J,K),T1,3,1,3)	OUTP0940
	DO 57 I=1,3	OUTP0950
	57 T3(I) = SEGLP(I,L)+T1(I)-XCOMP(I)	OUTP0960
	58 CALL MAT (DVEH,T3,ACC(1,J),3,3,1,3,3,6)	OUTP0970
	GO TO 63	OUTP0980
C		OUTP0990
		OUTP1000

C	4. SEGMENT ANGULAR ACCELERATIONS IN LOCAL REFERENCE	OUTP1010
C		OUTP1020
	59 DO 60 I=1,3	OUTP1030
	60 ACC(I,J) = WMEGD(I,L)/(2.0*PI)	OUTP1040
	GO TO 63	OUTP1050
C		OUTP1060
C	5. SEGMENT ANGULAR VELOCITIES IN VEHICLE REFERENCE	OUTP1070
C		OUTP1080
	61 CALL DOT (D(1,1,L),WMEG(1,L),T1,3,1,3)	OUTP1090
	CALL MAT (DVEH,T1,T2,3,3,1,3,3,3)	OUTP1100
	DO 62 I=1,3	OUTP1110
	62 ACC(I,J) = (T2(I)-VMEG(I))/(2.0*PI)	OUTP1120
	63 ACC(4,J) = DSQRT(ACC(1,J)**2+ACC(2,J)**2+ACC(3,J)**2)	OUTP1130
	GO TO 66	OUTP1140
C		OUTP1150
C	6. SEGMENT ANGULAR DISPLACEMENTS IN VEHICLE REFERENCE	OUTP1160
C		OUTP1170
	64 CALL DOT (D(1,1,L),DVEH,T1,3,3,3)	OUTP1180
	CALL YPRDEG(T1,ACC(1,J))	OUTP1190
	TRACE = 0.5*(T1(1)+T2(2)+T3(3)-1.0)	OUTP1200
	IF (TRACE.GT. 1.0) TRACE = 1.0	OUTP1210
	IF (TRACE.LT.-1.0) TRACE = -1.0	OUTP1220
	ACC(4,J) = DARCOS(TRACE)/RADIAN	OUTP1230
	GO TO 66	OUTP1240
C		OUTP1250
C	7. JOINT PARAMETERS	OUTP1260
C		OUTP1270
	65 ACC(1,J) = PRJNT(1,L)/RADIAN	OUTP1280
	ACC(2,J) = PRJNT(2,L)/RADIAN	OUTP1290
	ACC(3,J) = PRJNT(3,L)	OUTP1300
	ACC(4,J) = PRJNT(4,L)	OUTP1310
	ACC(5,J) = PRJNT(5,L)	OUTP1320
	ACC(6,J) = PRJNT(6,L)	OUTP1330
	66 CONTINUE	OUTP1340
	IF (K.LE.6) WRITE (NT,121) USEC,((ACC(I,J),I=1,4),J=J1,J2)	OUTP1350
	121 FORMAT(F9.3,3(3X,4F9.2) )	OUTP1360
	67 IF (K.EQ.7) WRITE (NT,123) USEC,((ACC(I,J),I=1,6),J=J1,J2)	OUTP1370
	123 FORMAT(F9.3,2(2X,0P2F7.2,1P4D11.4) )	OUTP1380
	68 CONTINUE	OUTP1390
C		OUTP1400
C	PRINT PLANE FORCES	OUTP1410
C		OUTP1420
	IF (MPSF.EQ.0) GO TO 77	OUTP1430
	DO 76 J1=1,MPSF,2	OUTP1440
	J2 = MIN0(J1+1,MPSF)	OUTP1450
	NT = NT+1	OUTP1460
	76 WRITE (NT,129) USEC,((PSF(I,J),I=1,7),J=J1,J2)	OUTP1470
	129 FORMAT(F9.3,2(F9.3,3F9.2,3F8.2) )	OUTP1480
C		OUTP1490
C	PRINT BELT FORCES	OUTP1500

C		OUTP1510
	77 IF (MBSF.EQ.0) GO TO 79	OUTP1520
	DO 78 J1=1,MBSF,2	OUTP1530
	J2 = MINO(J1+1,MBSF)	OUTP1540
	NT = NT+1	OUTP1550
	78 WRITE (NT,135) USEC,((BSF(I,J),I=1,4),J=J1,J2)	OUTP1560
	135 FORMAT(F9.3,4(F15.6,F12.2,3X) )	OUTP1570
C		OUTP1580
C	PRINT SEGMENT CONTACT FORCES	OUTP1590
C		OUTP1600
	79 IF (MSSF.EQ.0) GO TO 81	OUTP1610
	DO 80 J=1,MSSF	OUTP1620
	NT = NT+1	OUTP1630
	80 WRITE (NT,37) USEC,((SSF(I,J),I=1,10)	OUTP1640
	37 FORMAT(2F9.3,3F9.2,3F8.2,2X,3F8.2)	OUTP1650
C		OUTP1660
C	PRINT AIRBAG FORCES	OUTP1670
C		OUTP1680
	81 IF (NBAG.EQ.0) GO TO 91	OUTP1690
	K1 = 1	OUTP1700
	DO 83 J=1,NBAG	OUTP1710
	IF (MNBAG(J).EQ.0) GO TO 83	OUTP1720
	KBAG = MNBAG(J)+NPANEL(J)+5	OUTP1730
	DO 82 J1=1,KBAG,4	OUTP1740
	J2 = MINO(J1+3,KBAG)	OUTP1750
	K2 = K1+J2-J1	OUTP1760
	NT = NT+1	OUTP1770
	WRITE (NT,21) USEC,((BAGSF(I,K),I=1,3),K=K1,K2)	OUTP1780
	21 FORMAT(F9.3,4(3X,3F9.2))	OUTP1790
	82 K1 = K2+1	OUTP1800
	83 CONTINUE	OUTP1810
	91 CONTINUE	OUTP1820
C		OUTP1830
	CALL ELTIME(2,8)	OUTP1840
	RETURN	OUTP1850
	END	OUTP1860



C	SUBROUTINE PLELP(M,MM,N,NN,NT)	PLEL0010
C		REV 12 11/25/74 PLEL0020
C	COMPUTES FORCES (WHICH ARE ADDED TO U1 ARRAY)	PLEL0030
C	AND TORQUES (WHICH ARE ADDED TO U2 ARRAY)	PLEL0040
C	OF ELLIPSOID (MM) ATTACHED TO BODY SEGMENT (M)	PLEL0050
C	INTERSECTING PLANE (NN) ATTACHED TO SEGMENT (N).	PLEL0060
C		PLEL0070
	IMPLICIT REAL *8(A-H,O-Z)	PLEL0080
	COMMON/TABLES/MXNT1,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)	PLEL0090
	COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)	PLEL0100
	* ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)	PLEL0110
	COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),	PLEL0120
	* NPSF,NBSF,NSSF,NBSGF,NPANEL(6),PRJNT(6,21)	PLEL0130
	COMMON/CNSTRF/ PL(17,20),GAB(8,3),BELT(20,8),TPTS(6,8),BD(24,25)	PLEL0140
	COMMON/CSTRNT/A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24)	PLEL0150
	* ,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12)	PLEL0160
	* ,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12)	PLEL0170
	* ,NQ,KQ1(12),KQ2(12),KQTYPE(12)	PLEL0180
	COMMON/TEMPVS/DMNT(3,3),TEMP(3,3),B(3,3),XMN(3),RLN(3),XMM(3),	PLEL0190
	* TM(3),R(3),RM(3),DMNWN(3),RLM(3),RN(3),VMN(3),VR(3),	PLEL0200
	* WMN(3),WCM(3),WCN(3),VREL(3),FFM(3),FR(3),TQM(3),	PLEL0210
	* TQN(3),TQNT(3),T(3),H(3),T1(3),T2(3),RMD(3),RND(3),	PLEL0220
	* TD(3),TT4(3,4),TT5(3,4),T3(3),T4(3),P,AMR,FM,CF,	PLEL0230
	* VRT,VRTS,TF,MCF,NCF	PLEL0240
	CALL ELTIME(1,21)	PLEL0250
C		PLEL0260
C	COMPUTE PENETRATION DISTANCE, IF NEGATIVE, RETURN.	PLEL0270
C		PLEL0280
	CALL DOT(D(1,1,M),D(1,1,N),DMNT,3,3,3)	PLEL0290
	DO 10 I=1,3	PLEL0300
10	XMN(I) = SEGLP(I,M) - SEGLP(I,N)	PLEL0310
	CALL MAT(D(1,1,M),XMN,XMM,3,3,1,3,3,3)	PLEL0320
	CALL MAT(DMNT,PL(1,NN),TM,3,3,1,3,3,3)	PLEL0330
	BET = PL(4,NN)	PLEL0340
	DO 11 I=1,3	PLEL0350
11	BET = BET - TM(I)*(BD(I+3,MM)+XMM(I))	PLEL0360
	CALL MAT(BD(16,MM),TM,RM,3,3,1,3,3,3)	PLEL0370
	BTS = TM(1)*RM(1) + TM(2)*RM(2) + TM(3)*RM(3)	PLEL0380
	BTE = -DSQRT(BTS)	PLEL0390
	P = BET - BTE	PLEL0400
	MCF = NTAB(NT+1)	PLEL0410
	NCF = -MCF	PLEL0420
	IF (NCF.GT.0) CFQQ(NCF) = -999.	PLEL0430
	IF (P.LE.0.0) GO TO 99	PLEL0440
C		PLEL0450
C	IF COMPLETE PENETRATION, RETURN	PLEL0460
C		PLEL0470
	IF (BET+BTE.GT.0.0) GO TO 99	PLEL0480
C		PLEL0490
C	COMPUTE TG - THE POINT IN SEGMENT REFERENCE AT WHICH THE CONTACT	PLEL0500

C	FORCES ARE TO BE APPLIED WHICH LIES ON THE SCALED	PLEL0510
C	LINE BETWEEN THE POINT OF MAXIMUM PENETRATION (RHO=0)	PLEL0520
C	AND THE CENTER OF THE INTERSECTION ELLIPSE (RHO=1).	PLEL0530
C	AND TEMP - THE SAME POINT IN VEHICLE REFERENCE.	PLEL0540
C		PLEL0550
	RHO = 0.0	PLEL0560
	IF (MCF.GT.0) RHO = TAB(MCF+4)	PLEL0570
	BETE = (1.0+RHO*P/BTE)/BTE	PLEL0580
	AMR = -1.0/BTE	PLEL0590
	DO 13 I=1,3	PLEL0600
	RM(I) = BETE*RM(I)	PLEL0610
	RLM(I) = RM(I) + BD(I+3,MM)	PLEL0620
13	RN(I) = RLM(I) + XMM(I)	PLEL0630
	CALL DOT(DMNT,RN,RLN,3,1,3)	PLEL0640
C		PLEL0650
C	IF BOUNDARY PLANE IS GIVEN, COMPUTE DISTANCE FROM POINT TO PLANE,	PLEL0660
C	IF NEGATIVE OR > LIMIT, RETURN.	PLEL0670
C		PLEL0680
	DO 14 I=8,13,5	PLEL0690
	IF (PL(I+4,NN).LE.0.0) GO TO 14	PLEL0700
	DIST = RLN(1)*PL(I,NN)	PLEL0710
	* + RLN(2)*PL(I+1,NN)	PLEL0720
	* + RLN(3)*PL(I+2,NN) - PL(I+3,NN)	PLEL0730
	IF (DIST.LE.0.0 .OR. DIST.GT.PL(I+4,NN)) GO TO 99	PLEL0740
14	CONTINUE	PLEL0750
	CALL PLSEGF(M,N,NT)	PLEL0760
	IF (MCF.LT.0) GO TO 30	PLEL0770
C		PLEL0780
C	STORE RESULTS FOR OUTPUT ROUTINE.	PLEL0790
C		PLEL0800
	PSF(1,NPSF) = P	PLEL0810
	PSF(2,NPSF) = FM	PLEL0820
	PSF(3,NPSF) = FM*CF	PLEL0830
	IF (VRT.EQ.1.0) PSF(3,NPSF) = FM*CF*VRTS	PLEL0840
	PSF(4,NPSF) = TF	PLEL0850
	DO 24 I=1,3	PLEL0860
24	PSF(I+4,NPSF) = RLN(I)	PLEL0870
	GO TO 99	PLEL0880
30	PSF(1,NPSF) = P	PLEL0890
	DO 31 I=1,3	PLEL0900
	PSF(I+1,NPSF) = T(I)	PLEL0910
31	PSF(I+4,NPSF) = RLN(I)	PLEL0920
	CALL CROSS(WMN,TM,T1)	PLEL0930
	CALL MAT(BD(16,MM),T1,T2,3,3,1,3,3,3)	PLEL0940
	TMT = TM(1)*T2(1) + TM(2)*T2(2) + TM(3)*T2(3)	PLEL0950
	TMT = TMT/BTE	PLEL0960
	DO 32 I=1,3	PLEL0970
32	RMD(I) = (T2(I)-TMT*RM(I))*BETE	PLEL0980
	CALL CROSS(DMNWN,VREL,T1)	PLEL0990
	CALL CROSS(WMN,RMD,T3)	PLEL1000



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CALL DOT(D(1,1,M),T3,RQQ(1,NCF),3,1,3)
SQQ(NCF) = 0.0
DO 36 I=1,3
36 SQQ(NCF) = SQQ(NCF) + TM(I)*(T3(I)+2.0*T1(I))
99 CALL ELTIME(2,21)
RETURN
END

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PLEL1010
PLEL1020
PLEL1030
PLEL1040
PLEL1050
PLEL1060
PLEL1070

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	SUBROUTINE RSTART(IF,IT)	REV 12 12/19/74	RSTA0010
C			RSTA0020
C	THE FIVE FUNCTIONS OF SUBROUTINE RSTART ARE:		RSTA0030
C	1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.		RSTA0040
C	2. WRITE INPUT & INITIALIZATION RECORD UNTO NEW RESTART TAPE.		RSTA0050
C	3. READ TIME POINT RECORD FROM OLD RESTART TAPE.		RSTA0060
C	4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.		RSTA0070
C	5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.		RSTA0080
C			RSTA0090
C	IMPLICIT REAL*8(A-H,O-Z)		RSTA0100
C			RSTA0110
C	ALL LABELED COMMON BLOCKS ARE INCLUDED HERE		RSTA0120
C	TO GIVE A COMPLETE SET FOR REFERENCE		RSTA0130
C	1		RSTA0140
	COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)		RSTA0150
	DIMENSION IC1(49)		RSTA0160
	EQUIVALENCE (IC1(1),NSEG)		RSTA0170
C	2		RSTA0180
	COMMON/CNTRF/ PL(17,20),GAB(8,3),BELT(20,8),TPTS(6,8),BD(24,25)		RSTA0190
	DIMENSION RC2(1172)		RSTA0200
	EQUIVALENCE (RC2(1),PL(1,1))		RSTA0210
C	3		RSTA0220
	COMMON/VPOSTN/ TIME,X0(3),XDOTO(3),XCOMP(3),XVCOMP(3),AX(3),		RSTA0230
	* ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,		RSTA0240
	* NATAB,NACLR,DVEH(3,3),VMEG(3),VMEGD(3),XACOMP(3),		RSTA0250
	* THET(3),ZPLT(3)		RSTA0260
	DIMENSION RC3(1527),RC3A(1511),IC3(2),RC3B(18)		RSTA0270
	EQUIVALENCE (RC3(1),TIME),(RC3A(1),AX(1)),		RSTA0280
	* (IC3(1),NATAB),(RC3B(1),DVEH(1,1))		RSTA0290
C	4		RSTA0300
	COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)		RSTA0310
	* ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)		RSTA0320
	DIMENSION RC4(660)		RSTA0330
	EQUIVALENCE (RC4(1),D(1,1,1))		RSTA0340
C	5		RSTA0350
	COMMON/CMATRX/V1(3,21),V2(3,21),V3(3,12),B12(3,3,42),A22(3,3,42)		RSTA0360
	* ,F(3,21),TQ(3,21),WJ(21)		RSTA0370
	DIMENSION RC5A(918),RC5B(147)		RSTA0380
	EQUIVALENCE (RC5A(1),V1(1,1)),(RC5B(1),F(1,1))		RSTA0390
C	6		RSTA0400
	COMMON /ABDATA/ ABC(3,5), ZA(3,5), DA(3,3,5), BFA(3,5)		RSTA0410
	* ,BCGV(3,5),BMEG(3,5)		RSTA0420
	DIMENSION RC6(120)		RSTA0430
	EQUIVALENCE (RC6(1),ABC(1,1))		RSTA0440
C	7		RSTA0450
	COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),BLTTTL(5,8)		RSTA0460
	* ,PLTTL(5,20),BAGTTL(5,6),SEG(22),JUNIT(21)		RSTA0470
	* ,CGS(21),JS(21)		RSTA0480
	REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT		RSTA0490
	LOGICAL*1 CGS,JS		RSTA0500

	REAL RC7,RC7A,XDTE,XCMENT	RSTA0510
	DIMENSION RC7(238),RC7A(281),XDTE(3),XCMENT(40)	RSTA0520
	EQUIVALENCE (RC7(1),VPSTTL(1)),(RC7A(1),DATE(1))	RSTA0530
C 8	COMMON/CNSNTS/ PI, RADIANG,THIRD,EPS1,EPS4,EPS6,EPS8,	RSTA0540
	* EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)	RSTA0550
	DIMENSION RC8(18)	RSTA0560
	EQUIVALENCE (RC8(1),PI)	RSTA0570
C 9	COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)	RSTA0580
	* ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63)	RSTA0590
	* ,VISC(7,63),JNT(21),IPIN(21),NS,ISING(22)	RSTA0600
	* ,IGLOB(21),JOINTF(21)	RSTA0610
	DIMENSION RC9(1688),IC9(107)	RSTA0620
	EQUIVALENCE (RC9(1),PHI(1,1)),(IC9(1),JNT(1))	RSTA0630
C 10	COMMON/J8ARTZ/ MNPL( 20),MN8LT( 8),MNSEG( 22),MN8AG( 6),	RSTA0640
	* MPL(3,5,20),M8LT(3,5,8),MSEG(3,5,22),MBAG(3,10,6),	RSTA0650
	* NTPL(5,20),NT8LT(5,8),NTSEG(5,22)	RSTA0660
	DIMENSION IC10(1236)	RSTA0670
	EQUIVALENCE (IC10(1),MNPL(1))	RSTA0680
C 11	COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),	RSTA0690
	* NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21)	RSTA0700
	DIMENSION RC11(480),IC11(4),RC11A(126)	RSTA0710
	EQUIVALENCE (RC11(1),PSF(1,1)),(IC11(1),NPSF),	RSTA0720
	* (RC11A(1),PRJNT(1,1))	RSTA0730
C 12	COMMON/INTEST/ SGTEST(3,4,22),XTEST(3,88)	RSTA0740
	DIMENSION RC12(528)	RSTA0750
	EQUIVALENCE (RC12(1),SGTEST(1,1,1))	RSTA0760
C 13	COMMON/CSTRNT/ A13(3,3,24),A23(3,3,24),831(3,3,24),B32(3,3,24)	RSTA0770
	* ,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12)	RSTA0780
	* ,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12)	RSTA0790
	* ,NQ,KQ1(12),KQ2(12),KQTYPE(12)	RSTA0800
	DIMENSION RC13(72),IC13(37),RC13A(1212),RC13H(348)	RSTA0810
	EQUIVALENCE (RC13(1),RK1(1,1)),(IC13(1),NQ),(RC13A(1),A13(1,1,1))	RSTA0820
	* ,(RC13H(1),HHT(1,1,1))	RSTA0830
C 14	COMMON/TABLES/MXNTI,MXNTB,MXT81,MXT82,NTI(50),NTA8(500),TAB(2000)	RSTA0840
	DIMENSION IC14(554)	RSTA0850
	EQUIVALENCE (IC14(1),MXNTI)	RSTA0860
C 15	COMMON/COMAIN/VAR(120),DER(120),DT,HG,HMAX,HMIN,RSTIME,	RSTA0870
	* ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOUT	RSTA0880
	DIMENSION RC15(245),IC15(6)	RSTA0890
	EQUIVALENCE (RC15(1),VAR(1)),(IC15(1),ISTEP)	RSTA0900
C 16	COMMON/CDINT/ E(3,120),FF(5,120),GG(5,120),Y(5,120),U(5,120)	RSTA0910
		RSTA0920
		RSTA0930
		RSTA0940
		RSTA0950
		RSTA0960
		RSTA0970
		RSTA0980
		RSTA0990
		RSTA1000

	* ,H,HPRINT,TSAVE,TPRINT,TSTART,ICNT,IDBL,IFLAG	RSTA1010
C	NOTE: FF REPLACES F FROM SUBROUTINE DINT.	RSTA1020
	DIMENSION RC16(2765),IC16(3)	RSTA1030
	EQUIVALENCE (RC16(1),E(1,1)),(IC16(1),ICNT)	RSTA1040
C 17	COMMON/DAMPER/APSDM(3,20),APSON(3,20),ASD(5,20),	RSTA1050
	* NSO,MSDM(20),MSON(20)	RSTA1060
	DIMENSION RC17(220),IC17(41)	RSTA1070
	EQUIVALENCE (RC17(1),APSDM(1,1)),(IC17(1),NSO)	RSTA1080
C 18	COMMON/CEULER/ IEULER(22),HIR(3,3,21),ANG(3,21),ANGO(3,21),	RSTA1090
	* FE(3,21),TQE(3,21),CONST(3,21)	RSTA1100
	DIMENSION RC18(504)	RSTA1110
	EQUIVALENCE (RC18(1),HIR(1,1,1))	RSTA1120
C 19	COMMON/TEMPVI/ TT1(3),R11(3),R2I(3),CREST,JSTOP(4,2,21)	RSTA1130
	DIMENSION RC19(10),IC19(168)	RSTA1140
	EQUIVALENCE (RC19(1),TTI(1)),(IC19(1),JSTOP(1,1,1))	RSTA1150
C 20	COMMON /WJONES/	RSTA1160
	* FORCE(3,5),TORA(3,5),XBM(5),ZOEP(3,5),VBAGG(5),VSCS(5),	RSTA1170
	* BPHI(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),AB(3,5),SPRK(5),	RSTA1180
	* CYTD(5),CYPAL(5),CYSP(5),CYTO(5),	RSTA1190
	* CYVO(5),CYCO(5),CYK(5),CYR(5),CYAT(5),CYPV(5),CYCDO(5),	RSTA1200
	* CYAO(5),CYPQ(5),CYSS(5),CYLO(5),CYC(5),CYRHOQ(5),CYVMAX(5),	RSTA1210
	* CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYMIN(5),CYMOUT(5),	RSTA1220
	* BAGPV(5),PD(5),VBAG(5),VOLBP(5),SWITCH(5),1FULL(6),	RSTA1230
	* TMP(18),TMPI(3),A(3,3),PF(3),TORQ(3),	RSTA1240
	* TQB(3,10),FRB(3,10),VOL(10),OELF(3),	RSTA1250
	* B(9,4,5),ZB(3,4,5),ZR(3,4,5),BFB(9,4,5),DRR(9,4,5),	RSTA1260
	* DB(9,4,5),PCGV(3,4,5),PMEG(3,4,5),VOLP(4,5),FRA(3,4),PREVT	RSTA1270
	* ,CK(5),CMASS(5)	RSTA1280
	DIMENSION RC20A(30),RC20B(235),RC20C(50),RC20D(109),RC20E(180),	RSTA1290
	* RC20F(60),RC20G(420),RC20H(320),RC20I(10)	RSTA1300
	EQUIVALENCE (RC20A(1),FORCE(1,1)),(RC20B(1),XBM(1)),	RSTA1310
	* (RC20C(1),CYRHO(1)),(RC20D(1),TMP(1)),	RSTA1320
	* (RC20E(1),B(1,1,1)),(RC20F(1),ZB(1,1,1)),	RSTA1330
	* (RC20G(1),ZR(1,1,1)),(RC20H(1),DB(1,1,1)),	RSTA1340
	* (RC20I(1),CK(1))	RSTA1350
C 21	COMMON/RSAGE/ XSG(3,20,3),NSG(7),MSG(20,7)	RSTA1360
	DIMENSION RC21(180),IC21(147)	RSTA1370
	EQUIVALENCE (RC21(1),XSG(1,1,1)),(IC21(1),NSG(1))	RSTA1380
C 22	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8),NFLX	RSTA1390
	DIMENSION RC22(624),IC22(25)	RSTA1400
	EQUIVALENCE (RC22(1),HF(1,1,1)),(IC22(1),NFLEX(1,1))	RSTA1410
C 23	COMMON/HRNESS/ BAR(6,100),XLONG(20),IBAR(2,100),NTHRNS(20),	RSTA1420
	* NHRNSS, NBLTPH(5),NFBNL(5,20),NPTSPB(20)	RSTA1430
		RSTA1440
		RSTA1450
		RSTA1460
		RSTA1470
		RSTA1480
		RSTA1490
		RSTA1500



	DIMENSION RC23(620) , IC23(346)	RSTA1510
	EQUIVALENCE (RC23(1),BAR(1,1)) , (IC23(1),IBAR(1,1))	RSTA1520
C 24	COMMON/KALEPS/ WTIME(30),IWIND(30),MWSEG(5,22)	RSTA1530
	DIMENSION RC24(30) , IC24(140)	RSTA1540
	EQUIVALENCE (RC24(1),WTIME(1)) , (IC24(1),IWIND(1))	RSTA1550
C		RSTA1560
	DIMENSION COMMON(24)	RSTA1570
	DATA COMMON /8HCONTRL ,8HCNTRSRF ,8HVPOSTN ,8HSGMNTS ,	RSTA1580
	* 8HCMATRX ,8HABDATA ,8HTITLES ,8HCNSNTS ,	RSTA1590
	* 8HDESCRP ,8HJBARTZ ,8HFORCES ,8HINTEST ,	RSTA1600
	* 8HCSTRNT ,8HTABLES ,8HCOMAIN ,8HCDINT ,	RSTA1610
	* 8HDAMPER ,8HCEULER ,8HTEMPVI ,8HWJONES ,	RSTA1620
	* 8HRSAVE ,8HFLXBLE ,8HHRNESS ,8HKALEPS /	RSTA1630
	REAL AOLD4,AAOLD4	RSTA1640
	DATA BLANK/8H /	RSTA1650
	DIMENSION INDEX(3)	RSTA1660
	CALL ELTIME(1,25)	RSTA1670
	GO TO (100,200,300,400,500),IF	RSTA1680
C		RSTA1690
C	1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.	RSTA1700
C		RSTA1710
	100 READ (IT) IC1,PL,BD,X0,XDOT0,RC3A,NATAB,ZPLT,NSYM,XDTE,XCMET,	RSTA1720
	* RC7,CGS,JS,RC8,RC9,JNT,IC10,NPANEL,SGTEST,RC13,IC13,	RSTA1730
	* IC14,DT,HC,HMAX,HMIN,NSTEPS,NDINT,RC17,IC17,IEULER,	RSTA1740
	* RC20B,IFULL,RC20E,RC20G,RC20I,RC21,IC21,NS,ISING	RSTA1750
	* ,HF,NFLEX,NFLX,IC19,IGLOB,JOINTF,RC23,IC23,RC24,IC24	RSTA1760
	WRITE (6,I01) IT,XDTE,XCMET	RSTA1770
	101 FORMAT('O INPUT DATA HAS BEEN READ IN FROM UNIT NO.',I4//	RSTA1780
	* 10X,3A4//10X,20A4/10X,20A4)	RSTA1790
	GO TO 999	RSTA1800
C		RSTA1810
C	2. WRITE INPUT & INITIALIZATION RECORD ONTO NEW RESTART TAPE.	RSTA1820
C		RSTA1830
	200 WRITE (IT) IC1,PL,BD,X0,XDOT0,RC3A,NATAB,ZPLT,NSYM,DATE,COMET,	RSTA1840
	* RC7,CGS,JS,RC8,RC9,JNT,IC10,NPANEL,SGTEST,RC13,IC13,	RSTA1850
	* IC14,DT,HC,HMAX,HMIN,NSTEPS,NDINT,RC17,IC17,IEULER,	RSTA1860
	* RC20B,IFULL,RC20E,RC20G,RC20I,RC21,IC21,NS,ISING	RSTA1870
	* ,HF,NFLEX,NFLX,IC19,IGLOB,JOINTF,RC23,IC23,RC24,IC24	RSTA1880
	GO TO 999	RSTA1890
C		RSTA1900
C	3. READ TIME POINT RECORD FROM OLD RESTART TAPE.	RSTA1910
C		RSTA1920
	300 READ (IT) TIME,BELT,TPTS,XCOMP,XVCOMP,RC3B,RC4,RC5B,RC6,IPIN,RC11	RSTA1930
	* ,IC11,PRJNT,TAB,RC16,IC16,RC20A,RC20C,IFULL,RC20H,PREVTR	RSTA1940
	* ,RC21,IC21,VAR,DER,NEQ,XTEST,V4,IC19,RC13H,KQTYPE	RSTA1950
	* ,IEULER,RC23,WTIME,IWIND	RSTA1960
	CALL OUTPUT(1)	RSTA1970
	GO TO 999	RSTA1980
C		RSTA1990
		RSTA2000

C	5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.	RSTA2010
C		RSTA2020
	500 WRITE (IT) TIME,BELT,TPTS,XCOMP,XVCOMP,RC3B,RC4,RC5B,RC6,IPIN,RC11RSTA2030	
	* ,IC11,PRJNT,TAB,RC16,IC16,RC20A,RC20C,IFULL,RC20H,PREVTR STA2040	
	* ,RC21,IC21,VAR,DER,NEQ,XTEST,V4,IC19,RC13H,KQTYPE RSTA2050	
	* ,IEULER,RC23,WTIME,IWIND RSTA2060	
	GO TO 999 RSTA2070	
C		RSTA2080
C	4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.	RSTA2090
C		RSTA2100
	400 READ (5,401) AVAR,INDEX,ITYPE,RR,II,AA,RROLD,IIOLD,AAOLD RSTA2110	
	401 FORMAT(A8,4I4,2(F8.0,I8,A8)) RSTA2120	
	CALL SEARCH(AVAR,INDEX,NCOM,ITEM) RSTA2130	
	IF (NCOM.LE.0) GO TO 490 RSTA2140	
	IF (NCOM.GT.24) GO TO 999 RSTA2150	
	IF (ITYPE.GT.3) GO TO 490 RSTA2160	
	GO TO ( 1, 2, 3, 4, 5, 6, 7, 8, 9,10,11,12, RSTA2170	
	* 13,14,15,16,17,18,19,20,21,22,23,24),NCOM RSTA2180	
C	COMMON /CONTRL/ RSTA2190	
	1 IF (ITEM.GT.49) GO TO 490 RSTA2200	
	IF (ITYPE.NE.2) GO TO 490 RSTA2210	
	IOLD = IC1(ITEM) RSTA2220	
	IC1(ITEM) = II RSTA2230	
	GO TO 494 RSTA2240	
C	COMMON /CNTSRF/ RSTA2250	
	2 IF (ITEM.GT.1172) GO TO 490 RSTA2260	
	IF (ITYPE.NE.1) GO TO 490 RSTA2270	
	ROLD = RC2(ITEM) RSTA2280	
	RC2(ITEM) = RR RSTA2290	
	GO TO 492 RSTA2300	
C	COMMON /VPOSTN/ RSTA2310	
	3 IF (ITEM.GT.1527) GO TO 402 RSTA2320	
	IF (NTYPE.NE.1) GO TO 490 RSTA2330	
	ROLD = RC3(ITEM) RSTA2340	
	RC3(ITEM) = RR RSTA2350	
	GO TO 492 RSTA2360	
	402 IF (ITEM.GT.1529) GO TO 403 RSTA2370	
	IF (NTYPE.NE.2) GO TO 490 RSTA2380	
	IOLD = IC3(ITEM-1527) RSTA2390	
	IC3(ITEM-1527) = II RSTA2400	
	GO TO 494 RSTA2410	
	403 IF (ITEM.GT.1553) GO TO 490 RSTA2420	
	IF (NTYPE.NE.1) GO TO 490 RSTA2430	
	ROLD = RC3B(ITEM-1529) RSTA2440	
	RC3B(ITEM-1529) = RR RSTA2450	
	GO TO 492 RSTA2460	
C	COMMON /SGMNTS/ RSTA2470	
	4 IF (ITEM.GT.660 ) GO TO 404 RSTA2480	
	IF (ITYPE.NE.1) GO TO 490 RSTA2490	
	ROLD = RC4(ITEM) RSTA2500	



RC4(ITEM) = RR	RSTA2510
GO TO 492	RSTA2520
404 IF (ITEM.GT.682 ) GO TO 490	RSTA2530
IF (ITYPE.NE.1) GO TO 490	RSTA2540
IOLD = NSYM(ITEM-660)	RSTA2550
NSYM(ITEM-660) = II	RSTA2560
GO TO 494	RSTA2570
C COMMON /CMATRIX/	RSTA2580
5 IF (ITEM.GT.1065) GO TO 490	RSTA2590
IF (ITYPE.NE.1) GO TO 490	RSTA2600
ROLD = RC5A(ITEM)	RSTA2610
RC5A(ITEM) = RR	RSTA2620
GO TO 492	RSTA2630
C COMMON /ABDATA/	RSTA2640
6 IF (ITEM.GT.120 ) GO TO 490	RSTA2650
IF (ITYPE.NE.1) GO TO 490	RSTA2660
ROLD = RC6(ITEM)	RSTA2670
RC6(ITEM) = RR	RSTA2680
GO TO 492	RSTA2690
C COMMON /TITLES/ NOTE: NO PROVISION FOR CGS OR JS.	RSTA2700
7 IF (ITEM.GT.281 ) GO TO 490	RSTA2710
IF (ITYPE.NE.3) GO TO 490	RSTA2720
AOLD = RC7A(ITEM)	RSTA2730
RC7A(ITEM) = AA	RSTA2740
GO TO 496	RSTA2750
C COMMON /CNSNTS/	RSTA2760
8 IF (ITEM.GT.15 ) GO TO 408	RSTA2770
IF (ITEM.LE.12 ) GO TO 408	RSTA2780
IF (ITYPE.NE.3) GO TO 490	RSTA2790
AOLD = RC8(ITEM)	RSTA2800
RC8(ITEM) = AA	RSTA2810
GO TO 496	RSTA2820
408 IF (ITYPE.NE.1) GO TO 490	RSTA2830
ROLD = RC8(ITEM)	RSTA2840
RC8(ITEM) = RR	RSTA2850
GO TO 492	RSTA2860
C COMMON /DESCRP/	RSTA2870
9 IF (ITEM.GT.1688) GO TO 409	RSTA2880
IF (ITYPE.NE.1) GO TO 490	RSTA2890
ROLD = RC9(ITEM)	RSTA2900
RC9(ITEM) = RR	RSTA2910
GO TO 492	RSTA2920
409 IF (ITEM.GT.1795) GO TO 490	RSTA2930
IF (ITYPE.NE.2) GO TO 490	RSTA2940
IOLD = IC9(ITEM-1688)	RSTA2950
IC9(ITEM-1688) = II	RSTA2960
GO TO 494	RSTA2970
C COMMON /JBARTZ/	RSTA2980
10 IF (ITEM.GT.1236) GO TO 490	RSTA2990
IF (ITYPE.NE.2) GO TO 490	RSTA3000

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      IOLD = IC10(ITEM)
      IC10(ITEM) = II
      GO TO 494
C     COMMON /FORCES/
11    IF (ITEM.GT.480) GO TO 411
      IF (NTYPE.NE.1) GO TO 490
      ROLD = RC11(ITEM)
      RC11(ITEM) = RR
      GO TO 492
411   IF (ITEM.GT.490) GO TO 412
      IF (NTYPE.NE.2) GO TO 490
      IOLD = IC11(ITEM-480)
      IC11(ITEM-480) = II
      GO TO 494
412   IF (ITEM.GT.616) GO TO 490
      IF (NTYPE.NE.1) GO TO 490
      ROLD = RC11A(ITEM-490)
      RC11A(ITEM-490) = RR
      GO TO 492
C     COMMON /INTEST/
12    IF (ITEM.GT.528 ) GO TO 490
      IF (ITYPE.NE.1) GO TO 490
      ROLD = RC12(ITEM)
      RC12(ITEM) = RR
      GO TO 492
C     COMMON /CSTRNT/
13    IF (ITEM.GT.1212) GO TO 413
      IF (ITYPE.NE.1) GO TO 490
      ROLD = RC13A(ITEM)
      RC13A(ITEM) = RR
      GO TO 492
413   IF (ITEM.GT.1249) GO TO 490
      IF (ITYPE.NE.2) GO TO 490
      IOLD = IC13(ITEM-1212)
      IC13(ITEM-1212) = II
      GO TO 494
C     COMMON /TABLES/
14    IF (ITEM.GT.554 ) GO TO 414
      IF (ITYPE.NE.2) GO TO 490
      IOLD = IC14(ITEM)
      IC14(ITEM) = II
      GO TO 494
414   IF (ITEM.GT.2554) GO TO 490
      IF (ITYPE.NE.1) GO TO 490
      ROLD = TAB(ITEM-554)
      TAB(ITEM-554) = RR
      GO TO 492
C     COMMON /COMAIN/
15    IF (ITEM.GT.245 ) GO TO 415
      IF (ITYPE.NE.1) GO TO 490

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RSTA3010
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RSTA3500

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        ROLD = RC15(ITEM)
        RC15(ITEM) = RR
        GO TO 492
415 IF (ITEM.GT.251 ) GO TO 490
    IF (ITYPE.NE.2)   GO TO 490
    IOLD = IC15(ITEM-245)
    IC15(ITEM-245) = II
    GO TO 494
C      COMMON /CDINT /
16 IF (ITEM.GT.2765) GO TO 416
    IF (ITYPE.NE.1)   GO TO 490
    ROLD = RC16(ITEM)
    RC16(ITEM) = RR
    GO TO 492
416 IF (ITEM.GT.2768) GO TO 490
    IF (ITYPE.NE.2)   GO TO 490
    IOLD = IC16(ITEM-2765)
    IC16(ITEM-2765) = II
    GO TO 494
C      COMMON /DAMPER/
17 IF (ITEM.GT.220 ) GO TO 417
    IF (ITYPE.NE.1)   GO TO 490
    ROLD = RC17(ITEM)
    RC17(ITEM) = RR
    GO TO 492
417 IF (ITEM.GT.261 ) GO TO 490
    IF (ITYPE.NE.2)   GO TO 490
    IOLD = IC17(ITEM-220)
    IC17(ITEM-220) = II
    GO TO 494
C      COMMON /CEULER/
18 IF (ITEM.GT.22 ) GO TO 418
    IF (ITYPE.NE.2)   GO TO 490
    IOLD = IEULER(ITEM)
    IEULER(ITEM) = II
    GO TO 494
418 IF (ITEM.GT.526 ) GO TO 490
    IF (ITYPE.NE.1)   GO TO 490
    ROLD = RC18(ITEM-22)
    RC18(ITEM-22) = RR
    GO TO 492
C      COMMON /TEMPVI/
19 IF (ITEM.GT.10 ) GO TO 419
    IF (ITYPE.NE.1)   GO TO 490
    ROLD = RC19(ITEM)
    RC19(ITEM) = RR
    GO TO 492
419 IF (ITEM.GT.178 ) GO TO 490
    IF (ITYPE.NE.2)   GO TO 490
    IOLD = IC19(ITEM-10)

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RSTA4000

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        IC16(ITEM-10) = II
        GO TO 494
C      COMMON /WJONES/
20    IF (ITEM.GT.315 ) GO TO 420
        IF (ITYPE.NE.1)  GO TO 490
        ROLD = RC20A(ITEM)
        RC20A(ITEM) = RR
        GO TO 492
420    IF (ITEM.GT.321 ) GO TO 320
        IF (ITYPE.NE.2)  GO TO 490
        IOLD = IFULL(ITEM-315)
        IFULL(ITEM-315) = II
        GO TO 494
320    IF (ITEM.GT.1433) GO TO 490
        IF (ITYPE.NE.1)  GO TO 490
        ROLD = RC200(ITEM-321)
        RC200(ITEM-321) = RR
        GO TO 492
C      COMMON /RSAVE/
21    IF (ITEM.GT.180 ) GO TO 421
        IF (ITYPE.NE.1 ) GO TO 490
        ROLD = RC21(ITEM)
        RC21(ITEM) = RR
        GO TO 492
421    IF (ITEM.GT.327 ) GO TO 490
        IF (ITYPE.NE.2 ) GO TO 490
        IOLD = IC21(ITEM-180)
        IC21(ITEM-180) = II
        GO TO 494
C      COMMON /FLXBLE/
22    IF (ITEM.GT.624 ) GO TO 422
        IF (ITYPE.NE.1 ) GO TO 490
        ROLD = RC22(ITEM)
        RC22(ITEM) = RR
        GO TO 492
422    IF (ITEM.GT.649 ) GO TO 490
        IF (ITYPE.NE.2 ) GO TO 490
        IOLD = IC22(ITEM-624)
        IC22(ITEM-624) = II
        GO TO 494
C      COMMON /HRNESS/
23    IF (ITEM.GT.620 ) GO TO 423
        IF (ITYPE.NE.1)  GO TO 490
        ROLD = RC23(ITEM)
        RC23(ITEM) = RR
        GO TO 492
423    IF (ITEM.GT.966 ) GO TO 490
        IF (ITYPE.NE.2)  GO TO 490
        IOLD = IC23(ITEM-620)
        IC23(ITEM-620) = II

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RSTA4490
RSTA4500

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      GO TO 494
C     COMMON/KALEPS/
24  IF (ITEM.GT.30 ) GO TO 424
    IF (ITYPE.NE.1) GO TO 490
    ROLD = RC24(ITEM)
    RC24(ITEM) = RR
    GO TO 492
424 IF (ITEM.GT.170 ) GO TO 490
    IF (ITYPE.NE.2) GO TO 490
    IOLD = IC24(ITEM-30 )
    IC24(ITEM-30 ) = II
    GO TO 494
C
C     ERROR MESSAGE - TERMINATE PROGRAM.
C
490 WRITE (6,491) AVAR,INDEX,NCOM,ITEM,ITYPE,RR,II,AA
491 FORMAT('0 SUBROUTINE RSTART INPUT ERROR'//
*       ' AVAR= ',A8,' INDEX=',I3,' NCOM=',I6,' ITEM=',I6,
*       ' ITYPE=',I6,' RR=',G15.8,' II=',I8,' AA= ',A8//
*       ' PROGRAM IS BEING TERMINATED.')
    STOP
C
C     PRINT MESSAGE FOR REAL VARIABLES.
C
492 WRITE (6,493) AVAR,INDEX,COMMON(NCOM),ROLD,RR
493 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/',
*       ' HAS BEEN CHANGED FROM ',G15.8,' TO ',G15.8)
    IF (RROLD.EQ.0.0) GO TO 400
    IF (DABS(RROLD-ROLD).LE.0.00001*RROLD) GO TO 400
    WRITE (6,383) RROLD
383 FORMAT(' INPUT VALUE FOR RROLD WAS ',G15.8//)
    GO TO 490
C
C     PRINT MESSAGE FOR INTEGER VARIABLES.
C
494 WRITE (6,495) AVAR,INDEX,COMMON(NCOM),IOLD,II
495 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/',
*       ' HAS BEEN CHANGED FROM ', I8,' TO ', I8)
    IF (IIOLD.EQ.0) GO TO 400
    IF (IOLD.EQ.IIOLD) GO TO 400
    WRITE (6,385) IIOLD
385 FORMAT(' INPUT VALUE FOR IIOLD WAS ',I8//)
    GO TO 490
C
C     PRINT MESSAGE FOR ALPHANUMERIC VARIABLES.
C
496 WRITE (6,497) AVAR,INDEX,COMMON(NCOM),AOLD,AA
497 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/',
*       ' HAS BEEN CHANGED FROM ', A8,' TO ', A8)
    IF (AAOLD.EQ.BLANK) GO TO 400

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RSTA4510
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RSTA4990
RSTA5000

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AAOLD4 = AAOLD
AOLD4 = AOLD
IF (AOLD4.EQ.AAOLD4) GO TO 400
WRITE (6,387) AAOLD
387 FORMAT(' INPUT VALUE FOR AAOLD WAS ',A8//)
GO TO 490
999 CALL ELTIME(2,25)
RETURN
END
```

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RSTA5010
RSTA5020
RSTA5030
RSTA5040
RSTA5050
RSTA5060
RSTA5070
RSTA5080
RSTA5090
```



CCCC

CCC

CCC

CCC

CCC

	*	3,22,0	,	3,22,0	,	3,22,0	,	22,0,0	/	SEAR0510
C										SEAR0520
C	5	COMMON/CMATRX/								SEAR0530
C										SEAR0540
		DIMENSION C5 ( 8) , NC5 ( 24)								SEAR0550
		EQUIVALENCE (C5 (1),BVAR( 46)) , (NC5 (1),NDIM(1, 46))								SEAR0560
		DATA C5 /	8HV1	,	8HV2	,	8HV3	,	8HB12	, SEAR0570
	*		8HF	,	8HTQ	,	8HWJ	,	/	SEAR0580
		DATA NC5 /	3,21,0	,	3,21,0	,	3,12,0	,	3,3,42	, SEAR0590
	*		3,21,0	,	3,21,0	,	21,0,0	,	/	SEAR0600
C										SEAR0610
C	6	COMMON/ABDATA/								SEAR0620
C										SEAR0630
		DIMENSION C6 ( 6) , NC6 ( 18)								SEAR0640
		EQUIVALENCE (C6 (1),BVAR( 54)) , (NC6 (1),NDIM(1, 54))								SEAR0650
		DATA C6 /	8HABC	,	8HZA	,	8HDA	,	8HBFA	, SEAR0660
	*		8HBMEG	,	/					SEAR0670
		DATA NC6 /	3,5,0	,	3,5,0	,	3,3,5	,	3,5,0	, SEAR0680
	*		3,5,0	,	/					SEAR0690
C										SEAR0700
C	7	COMMON/TITLES/								SEAR0710
C										SEAR0720
		DIMENSION C7 ( 11) , NC7 ( 33)								SEAR0730
		EQUIVALENCE (C7 (1),BVAR( 60)) , (NC7 (1),NDIM(1, 60))								SEAR0740
		DATA C7 /	8HDATE	,	8HCOMENT	,	8HVPSTTL	,	8HBDYTTL	, SEAR0750
	*		8HPLTTL	,	8HBAGTTL	,	8HSEG	,	8HJOINT	, SEAR0760
	*		8HJS	,	/					SEAR0770
		DATA NC7 /	3,0,0	,	40,0,0	,	20,0,0	,	5,0,0	, SEAR0780
	*		5,20,0	,	5,6,0	,	22,0,0	,	21,0,0	, SEAR0790
	*		21,0,0	,	/					SEAR0800
C										SEAR0810
C	8	COMMON/CNSNTS/								SEAR0820
C										SEAR0830
		DIMENSION C8 ( 16) , NC8 ( 48)								SEAR0840
		EQUIVALENCE (C8 (1),BVAR( 71)) , (NC8 (1),NDIM(1, 71))								SEAR0850
		DATA C8 /	8HPI	,	8HRADIAN	,	8HG	,	8HTHIRD	, SEAR0860
	*		8HEPS4	,	8HEPS6	,	8HEPS8	,	8HEPS12	, SEAR0870
	*		8HEPS20	,	8HEPS24	,	8HUNITL	,	8HUNITM	, SEAR0880
	*		8HGRAVITY	,	/					SEAR0890
		DATA NC8 /	0,0,0	,	0,0,0	,	0,0,0	,	0,0,0	, SEAR0900
	*		0,0,0	,	0,0,0	,	0,0,0	,	0,0,0	, SEAR0910
	*		0,0,0	,	0,0,0	,	0,0,0	,	0,0,0	, SEAR0920
	*		3,0,0	,	/					SEAR0930
C										SEAR0940
C	9	COMMON/DESCRP/								SEAR0950
C										SEAR0960
		DIMENSION C9 ( 16) , NC9 ( 48)								SEAR0970
		EQUIVALENCE (C9 (1),BVAR( 87)) , (NC9 (1),NDIM(1, 87))								SEAR0980
		DATA C9 /	8HPI	,	8HW	,	8HSR	,	8HHA	, SEAR0990
	*		8HHT	,	8HRPHI	,	8HRW	,	8HSPRING	, SEAR1000

*	8HJNT	,8HIPIN	,8HNS	,8HISING	,8HIGLOB	, SEAR1010
*	8HJOINTF	/				SEAR1020
DATA NC9 /	3,22,0	, 22,0,0	, 3,42,0	, 3,42,0	, 3,42,0	, SEAR1030
*	3,3,42	, 3,22,0	, 22,0,0	, 5,63,0	, 7,63,0	, SEAR1040
*	21,0,0	, 21,0,0	, 0,0,0	, 22,0,0	, 21,0,0	, SEAR1050
*	21,0,0	/				SEAR1060
C						SEAR1070
C 10	COMMON/JBARTZ/					SEAR1080
C						SEAR1090
	DIMENSION C10( 11) , NC10( 33)					SEAR1100
	EQUIVALENCE (C10(1),BVAR(103)) , (NC10(1),NDIM(1,103))					SEAR1110
	DATA C10/ 8HMNPL	,8HMNBLT	,8HMNSEG	,8HMNBAG	,8HMPL	, SEAR1120
*	8HMBLT	,8HMSEG	,8HMBAG	,8HNTPL	,8HNTBLT	, SEAR1130
*	8HNTSEG	/				SEAR1140
	DATA NC10/ 20,0,0	, 8,0,0	, 22,0,0	, 6,0,0	, 3,5,20	, SEAR1150
*	3,5,8	, 3,5,22	, 3,10,6	, 5,20,0	, 5,8,0	, SEAR1160
*	5,22,0	/				SEAR1170
C						SEAR1180
C 11	COMMON/FORCES/					SEAR1190
C						SEAR1200
	DIMENSION C11( 10) , NC11( 30)					SEAR1210
	EQUIVALENCE (C11(1),BVAR(114)) , (NC11(1),NDIM(1,114))					SEAR1220
	DATA C11/ 8HPSF	,8HBSF	,8HSSF	,8HBAGSF	,8HNPSF	, SEAR1230
*	8HNBSF	,8HNSSF	,8HNBGSF	,8HNPANEL	,8HPRJNT	/ SEAR1240
	DATA NC11/ 7,20,0	, 4,20,0	, 10,20,0	, 3,20,0	, 0,0,0	, SEAR1250
*	0,0,0	, 0,0,0	, 0,0,0	, 6,0,0	, 6,21,0	/ SEAR1260
C						SEAR1270
C 12	COMMON/INTEST/					SEAR1280
C						SEAR1290
	DIMENSION C12( 2) , NC12( 6)					SEAR1300
	EQUIVALENCE (C12(1),BVAR(124)) , (NC12(1),NDIM(1,124))					SEAR1310
	DATA C12/ 8HSGTEST	,8HXTTEST	/			SEAR1320
	DATA NC12/ 3,4,22	, 3,88,0	/			SEAR1330
C						SEAR1340
C 13	COMMON/CSTRNT/					SEAR1350
C						SEAR1360
	DIMENSION C13( 17) , NC13( 51)					SEAR1370
	EQUIVALENCE (C13(1),BVAR(126)) , (NC13(1),NDIM(1,126))					SEAR1380
	DATA C13/ 8HA13	,8HA23	,8HB31	,8HB32	,8HHHT	, SEAR1390
*	8HRK1	,8HRK2	,8HQQ	,8HTQQ	,8HRQQ	, SEAR1400
*	8HHQQ	,8HSQQ	,8HCFQQ	,8HNQ	,8HKQ1	, SEAR1410
*	8HKQ2	,8HKQTYPE	/			SEAR1420
	DATA NC13/ 3,3,24	, 3,3,24	, 3,3,24	, 3,3,24	, 3,3,12	, SEAR1430
*	3,12,0	, 3,12,0	, 3,12,0	, 3,12,0	, 3,12,0	, SEAR1440
*	3,12,0	, 12,0,0	, 12,0,0	, 0,0,0	, 12,0,0	, SEAR1450
*	12,0,0	, 12,0,0	/			SEAR1460
C						SEAR1470
C 14	COMMON/TABLES/					SEAR1480
C						SEAR1490
	DIMENSION C14( 7) , NC14( 21)					SEAR1500

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EQUIVALENCE (C14(1),8VAR(143)) , (NC14(1),NDIM(1,143))
DATA C14/ 8HMXNTI ,8HMXNT8 ,8HMXT81 ,8HMXT82 ,8HNTI ,
*      8HNTA8 ,8HTA8 /
DATA NC14/ 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 50,0,0 ,
*      500,0,0 , 2000,0,0/

C
C 15 COMMON/COMAIN/
C
DIMENSION C15( 13) , NC15( 39)
EQUIVALENCE (C15(1),8VAR(150)) , (NC15(1),NDIM(1,150))
DATA C15/ 8HVAR ,8HDER ,8HDT ,8HHO ,8HHMAX ,
*      8HHMIN ,8HRSTIME ,8H1STEP ,8HNSTEPS ,8HNDINT ,
*      8HNEQ ,8HIRSIN ,8HIRSOUT /
DATA NC15/ 120,0,0 , 120,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,
*      0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,
*      0,0,0 , 0,0,0 , 0,0,0 /

C
C 16 COMMON/CDINT /
C
DIMENSION C16( 13) , NC16( 39)
EQUIVALENCE (C16(1),8VAR(163)) , (NC16(1),NDIM(1,163))
DATA C16/ 8HE ,8HFF ,8HGG ,8HY ,8HU ,
*      8HH ,8HHPRINT ,8HTSAVE ,8HTPRINT ,8HTSTART ,
*      8HICNT ,8HIDBL ,8HIFLAG /
DATA NC16/ 3,120,0 , 5,120,0 , 5,120,0 , 5,120,0 , 5,120,0 ,
*      0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,
*      0,0,0 , 0,0,0 , 0,0,0 /

C
C 17 COMMON/DAMPER/
C
DIMENSION C17( 6) , NC17( 18)
EQUIVALENCE (C17(1),8VAR(176)) , (NC17(1),NDIM(1,176))
DATA C17/ 8HAPSDM ,8HAPSDN ,8HASD ,8HNSD ,8HMSDM ,
*      8HMSDN /
DATA NC17/ 3,20,0 , 3,20,0 , 5,20,0 , 0,0,0 , 20,0,0 ,
*      20,0,0 /

C
C 18 COMMON/CEULER/
C
DIMENSION C18( 7) , NC18( 21)
EQUIVALENCE (C18(1),8VAR(182)) , (NC18(1),NDIM(1,182))
DATA C18/ 8HIEULER ,8HHIR ,8HANG ,8HANGD ,8HFE ,
*      8HTQE ,8HCONST /
DATA NC18/ 22,0,0 , 3,3,21 , 3,21,0 , 3,21,0 , 3,21,0 ,
*      3,21,0 , 3,21,0 /

C
C 19 COMMON/TEMPVI/
C
DIMENSION C19( 5) , NC19( 15)
EQUIVALENCE (C19(1),8VAR(189)) , (NC19(1),NDIM(1,189))

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	DATA C19/ 8HTT1	,8HR11	,8HR21	,8HCREST	,8HJSTOP	/	SEAR2010
	DATA NC19/ 3,0,0	, 3,0,0	, 3,0,0	, 0,0,0	, 4,2,21	/	SEAR2020
C							SEAR2030
C 20	COMMON/WJONES/						SEAR2040
C							SEAR2050
	DIMENSION C20( 64)	, NC20( 192)					SEAR2060
	EQUIVALENCE (C20(1),8VAR(194))	, (NC20(1),ND1M(1,194))					SEAR2070
	DATA C20/ 8HFORCE	,8HTORA	,8HX8M	,8HZDEP	,8HV8AGG	,	SEAR2080
*	8HVSCS	,8H8PH1	,8HD8R	,8HDPVCTR	,8HDEPLOY	,	SEAR2090
*	8HAB	,8HSPRK	,8HCYTD	,8HCYPA	,8HCYSP	,	SEAR2100
*	8HCYTO	,8HCYVC	,8HCYCD	,8HCYK	,8HCYR	,	SEAR2110
*	8HCYAT	,8HCYPV	,8HCYCD0	,8HCYA0	,8HCYP0	,	SEAR2120
*	8HCYSS	,8HCYL0	,8HCYC	,8HCYRH00	,8HCYVMAX	,	SEAR2130
*	8HCYORFC	,8HCYRHO	,8HCYT	,8HCYP	,8HCYMIN	,	SEAR2140
*	8HCYMOUT	,8H8AGPV	,8HPD	,8HVBAG	,8HVOL8P	,	SEAR2150
*	8HSWITCH	,8H1FULL	,8HTMP	,8HTMP1	,8HA	,	SEAR2160
*	8HPF	,8HTORQ	,8HTQ8	,8HFR8	,8HVOL	,	SEAR2170
*	8HDELf	,8H8	,8HZ8	,8HZR	,8HBF8	,	SEAR2180
*	8HDDR	,8HD8	,8HPCGV	,8HPMEG	,8HVOLP	,	SEAR2190
*	8HFRA	,8HPREVT	,8HCK	,8HCMASS	/		SEAR2200
	DATA NC20/ 3,5,0	, 3,5,0	, 5,0,0	, 3,5,0	, 5,0,0	,	SEAR2210
*	5,0,0	, 3,5,0	, 3,3,5	, 3,5,0	, 3,5,0	,	SEAR2220
*	3,5,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2230
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2240
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2250
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2260
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2270
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2280
*	5,0,0	, 6,0,0	, 18,0,0	, 3,0,0	, 3,3,0	,	SEAR2290
*	3,0,0	, 3,0,0	, 3,10,0	, 3,10,0	, 10,0,0	,	SEAR2300
*	3,0,0	, 9,4,5	, 3,4,5	, 3,4,5	, 9,4,5	,	SEAR2310
*	9,4,5	, 9,4,5	, 3,4,5	, 3,4,5	, 4,5,0	,	SEAR2320
*	3,4,0	, 0,0,0	, 5,0,0	, 5,0,0	/		SEAR2330
C							SEAR2340
C 21	COMMON/RSAGE/						SEAR2350
C							SEAR2360
	DIMENSION C21( 3)	, NC21( 9)					SEAR2370
	EQUIVALENCE (C21(1),8VAR(258))	, (NC21(1),NDIM(1,258))					SEAR2380
	DATA C21/ 8HXSG	,8HNSG	,8HMSG	/			SEAR2390
	DATA NC21/ 3,20,3	, 7,0,0	, 20,7,0	/			SEAR2400
C							SEAR2410
C 22	COMMON/FLXBLE/						SEAR2420
C							SEAR2430
	DIMENSION C22( 5)	, NC22( 15)					SEAR2440
	EQUIVALENCE (C22(1),8VAR(261))	, (NC22(1),NDIM(1,261))					SEAR2450
	DATA C22/ 8HHF	,8HB42	,8HV4	,8HNFLEX	,8HNFLX	/	SEAR2460
	DATA NC22/ 4,12,8	, 3,3,24	, 3,8,0	, 3,8,0	, 0,0,0	/	SEAR2470
C							SEAR2480
C 23	COMMON/HRNESS/						SEAR2490
	DIMENSION C23( 8)	, NC23( 24)					SEAR2500

	EQUIVALENCE (C23(1),8VAR(266)) , (NC23(1),NDIM(1,266))	SEAR2510
	DATA C23/ 8H8AR ,8HXLONG ,8H1BAR ,8HN1HRNS ,8HNHRNSS ,	SEAR2520
*	8HNB1TPH ,8HNFBLT ,8HNPTSPB /	SEAR2530
	DATA NC23/ 6,100,0 , 20,0,0 , 2,100,0 , 20,0,0 , 0,0,0 ,	SEAR2540
*	5,0,0 , 5,20,0 , 20,0,0 /	SEAR2550
C		SEAR2560
C 24	COMMON/KALEPS/	SEAR2570
	DIMENSION C24( 4) , NC24( 12)	SEAR2580
	EQUIVALENCE (C24(1),8VAR(274)) , (NC24(1),NDIM(1,274))	SEAR2590
	DATA C24/ 8HWTIME ,8HIWIND ,8HMWSEG /	SEAR2600
	DATA NC24/ 30,0,0 , 30,0,0 , 5,22,0 /	SEAR2610
	NCOM = 50	SEAR2620
	IF (AVAR.EQ.BLANK) GO TO 99	SEAR2630
C		SEAR2640
C	SEARCH FOR VARIABLE NO. IV.	SEAR2650
C		SEAR2660
	NCOM = C	SEAR2670
	DO 10 IV=1,NVAR	SEAR2680
	IF (AVAR.EQ.BVAR(IV)) GO TO 12	SEAR2690
10	CONTINUE	SEAR2700
	GO TO 99	SEAR2710
C		SEAR2720
C	SEARCH FOR COMMON NO. IC.	SEAR2730
C		SEAR2740
12	DO 20 IC=1,KOM	SEAR2750
	IF (IV.GE.KOUNT(IC).AND.IV.LT.KOUNT(IC+1)) GO TO 22	SEAR2760
20	CONTINUE	SEAR2770
	GO TO 99	SEAR2780
C		SEAR2790
C	COMPUTE ITEM NO. FOR VARIABLE IV IN COMMON IC.	SEAR2800
C		SEAR2810
22	K1 = KOUNT(IC)	SEAR2820
	K2 = IV-1	SEAR2830
	ITEM = 1	SEAR2840
	IF (K1.EQ.IV) GO TO 25	SEAR2850
	DO 24 K=K1,K2	SEAR2860
	NI = 1	SEAR2870
	DO 23 I=1,3	SEAR2880
	IF (NDIM(I,K).NE.0) NI=NI*NDIM(I,K)	SEAR2890
23	CONTINUE	SEAR2900
24	ITEM = ITEM+NI	SEAR2910
25	DO 26 I=1,3	SEAR2920
	IF (INDEX(I).EQ.0 .AND. NDIM(I,IV).NE.0) GO TO 99	SEAR2930
	IF (NDIM(I,IV).EQ.0 .AND. INDEX(I).GT.1) GO TO 99	SEAR2940
	NJ(I) = MAX0(INDEX(I)-1,0)	SEAR2950
	NK(I) = MAX0(NDIM(I,IV),1)	SEAR2960
	IF (NJ(I).GE.NK(I)) GO TO 99	SEAR2970
26	CONTINUE	SEAR2980
	ITEM = ITEM+NJ(1)+NJ(2)*NK(1)+NJ(3)*NK(2)*NK(1)	SEAR2990
	NCOM = IC	SEAR3000



99 RETURN  
END

SEAR3010  
SEAR3020



C		UPDA0510
C	CALL UPDFDC FOR EACH ALLOWED PLANE-SEGMENT CONTACT.	UPDA0520
C		UPDA0530
	NPSF = 0	UPDA0540
	DO 11 J = 1,NPL	UPDA0550
	NK = MNPL(J)	UPDA0560
	IF (NK.LE.0) GO TO 11	UPDA0570
	DO 10 K = 1, NK	UPDA0580
	NPSF = NPSF+1	UPDA0590
	NT = NTPL(K,J)	UPDA0600
	NF = NTAB(NT+5)	UPDA0610
	CALL UPDFDC(NT)	UPDA0620
	IF (NT.GT.0.OR.TAB(NF+3).EQ.0.0) GO TO 10	UPDA0630
	CALL IMPULS(1,K,J)	UPDA0640
	I = -1	UPDA0650
10	CONTINUE	UPDA0660
11	CONTINUE	UPDA0670
12	IF (NBLT.LE.0) GO TO 15	UPDA0680
C		UPDA0690
C	CALL UPDFDC FOR EACH ALLOWED BELT-SEGMENT CONTACT.	UPDA0700
C		UPDA0710
	DO 14 J = 1,NBLT	UPDA0720
	NK = MNBLT(J)	UPDA0730
	IF (NK.LE.0) GO TO 14	UPDA0740
	DO 13 K = 1,NK	UPDA0750
	NT = NTBLT(K,J)	UPDA0760
	NF = NTAB(NT+5)	UPDA0770
	NT6 = NT+6	UPDA0780
	CALL UPDFDC(NT)	UPDA0790
C		UPDA0800
C	AND FOR 2ND FUNCTION, IF FULL BELT FRICTION.	UPDA0810
C		UPDA0820
13	IF (NF.NE.0) CALL UPDFDC(NT6)	UPDA0830
14	CONTINUE	UPDA0840
C		UPDA0850
C	CALL UPDFDC FOR EACH ALLOWED SEGMENT-SEGMENT CONTACT.	UPDA0860
C		UPDA0870
15	NSSF = 0	UPDA0880
	DO 17 J=1,NSEG	UPDA0890
	NK = MNSEG(J)	UPDA0900
	IF (NK.LE.0) GO TO 17	UPDA0910
	DO 16 K = 1,NK	UPDA0920
	NSSF = NSSF+1	UPDA0930
	NT = NTSEG(K,J)	UPDA0940
	NF = NTAB(NT+5)	UPDA0950
	CALL UPDFDC(NT)	UPDA0960
	IF (NT.GT.0.OR.TAB(NF+3).EQ.0.0) GO TO 16	UPDA0970
	CALL IMPULS(3,K,J)	UPDA0980
	I = -1	UPDA0990
16	CONTINUE	UPDA1000

17	CONTINUE	UPDA1010
	IF (NHRNSS.LE.0) GO TO 71	UPDA1020
C		UPDA1030
C	CALL UPDFDC FOR EACH BELT OF HARNESS-BELT SYSTEMS.	UPDA1040
C		UPDA1050
	J1 = 1	UPDA1060
	K1 = 1	UPDA1070
	DO 70 I1=1,NHRNSS	UPDA1080
	IF (NBLTPH(I1).LE.0) GO TO 70	UPDA1090
	J2 = J1 + NBLTPH(I1) - 1	UPDA1100
	DO 69 J=J1,J2	UPDA1110
	IF (NPTSPB(J).LE.0) GO TO 69	UPDA1120
	K2 = K1 + NPTSPB(J) - 1	UPDA1130
	NT = NTHRNS(J)	UPDA1140
	NF = NTAB(NT+5)	UPDA1150
	CALL UPDFDC(NT)	UPDA1160
	K1 = K2+1	UPDA1170
69	CONTINUE	UPDA1180
	J1 = J2+1	UPDA1190
70	CONTINUE	UPDA1200
71	IF (NJNT.LE.0) GO TO 39	UPDA1210
C		UPDA1220
C	CHECK FOR IMPULSE ON JOINT STOPS	UPDA1230
C	TO BE CALLED IF IN JOINT STOP (JSTOP(1)=1) THIS TIME STEP	UPDA1240
C	BUT NOT IN IN JOINT STOP (JSTOP(2)=0) AT PREVIOUS TIME.	UPDA1250
C		UPDA1260
	DO 20 K=1,NJNT	UPDA1270
	IF (JNT(K).EQ.0) GO TO 20	UPDA1280
	IF (IABS(IPIN(K)).NE.4 .AND. VISC(7,3*K-2).EQ.0.0) GO TO 19	UPDA1290
	DO 18 J=1,3	UPDA1300
	K3J = 3*K-3+J	UPDA1310
	IF (IABS(IPIN(K)).NE.4) K3J=3*K-2	UPDA1320
	IF (IABS(IPIN(K)).EQ.4 .AND. VISC(7,K3J).EQ.0.0) GO TO 18	UPDA1330
	IF (JSTOP(J,1,K).NE.1.OR.JSTOP(J,2,K).NE.0) GO TO 18	UPDA1340
	CALL IMPULS(4,J,K)	UPDA1350
	I = -1	UPDA1360
18	JSTOP(J,2,K) = JSTOP(J,1,K)	UPDA1370
19	IF (IGLOB(K).EQ.0) GO TO 20	UPDA1380
	NT = IGLOB(K)	UPDA1390
	MT = NTAB(NT+5)	UPDA1400
	CALL UPDFDC(NT)	UPDA1410
	IF (TAB(MT+3).EQ.0.0) GO TO 20	UPDA1420
	IF (JSTOP(4,1,K).NE.1.OR.JSTOP(4,2,K).NE.0) GO TO 20	UPDA1430
	CALL IMPULS(4,4,K)	UPDA1440
	I = -1	UPDA1450
20	JSTOP(4,2,K) = JSTOP(4,1,K)	UPDA1460
C		UPDA1470
C	TEST TO LOCK OR UNLOCK JOINTS	UPDA1480
C		UPDA1490
C		UPDA1500

C	CONDITIONS TO CHANGE SIGN OF IPIN(J)	UPDA1510
C		UPDA1520
C	PINNED                  UNPINNED	UPDA1530
C	LOCKED (-1)  H.TQ  > T1      (-2)  TQ  > T1	UPDA1540
C		UPDA1550
C	UNLOCKED (+1)  H.TQ  < T2      (+2)  TQ  < T2	UPDA1560
C	OR                                  OR	UPDA1570
C	WJ < T3                                  WJ < T3	UPDA1580
C		UPDA1590
	DO 30 J=1,NJNT	UPDA1600
	IF (IABS(IPIN(J)).EQ.4) GO TO 30	UPDA1610
	IF (IPIN(J)) 21,30,22	UPDA1620
21	T1 = VISC(4,3*J-2)	UPDA1630
	IF (T1.EQ.0.0) GO TO 30	UPDA1640
	IF (IPIN(J).LE.-2) TQM = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)	UPDA1650
	IF (IPIN(J).EQ.-1) TQM = DABS(XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J)))	UPDA1660
	IF (TQM-T1) 30,30,29	UPDA1670
22	T2 = VISC(5,3*J-2)	UPDA1680
	IF (T2.EQ.0.0) GO TO 23	UPDA1690
	IF (IPIN(J).GE.2) TQM = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)	UPDA1700
	IF (IPIN(J).EQ. 1) TQM = DABS(XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J)))	UPDA1710
	IF (TQM-T2) 28,30,30	UPDA1720
23	T3 = VISC(6,3*J-2)	UPDA1730
	IF (T3.EQ.0.0) GO TO 30	UPDA1740
	IF (WJ(J)-T3) 28,30,30	UPDA1750
28	CALL IMPLS2(0,J,HB(1,2*J))	UPDA1760
	1 = -1	UPDA1770
29	IPIN(J) = -IPIN(J)	UPDA1780
30	CONTINUE	UPDA1790
C		UPDA1800
C	TEST TO LOCK OR UNLOCK EULER JOINTS AXES.	UPDA1810
C	USE SAME TEST AS ABOVE BUT ON EACH AXIS SERARATELY.	UPDA1820
C		UPDA1830
C	IF LOCK(IEULER,K) IS NEGATIVE, AXIS K IS LOCKED;	UPDA1840
C	TO UNLOCK AXIS SET IEULER TO -LOCK(IEULER,K).	UPDA1850
C		UPDA1860
C	IF LOCK(IEULER,K) IS POSITIVE, AXIS K IS UNLOCKED;	UPDA1870
C	TO LOCK AXIS SET IEULER TO LOCK(IEULER,K).	UPDA1880
C		UPDA1890
	DO 60 J=1,NJNT	UPDA1900
	IF (IABS(IPIN(J)).NE.4) GO TO 60	UPDA1910
	JEULER = IEULER(J)	UPDA1920
	CALL DOT(HIR(1,1,J),TQ(1,J),TQTEST,3,1,3)	UPDA1930
	DO 55 K=1,3	UPDA1940
	K3J = 3*J-3+K	UPDA1950
	NLOCK = LOCK(JEULER,K)	UPDA1960
	IF (NLOCK.GT.0) GO TO 52	UPDA1970
	IF (VISC(4,K3J).EQ.0.0) GO TO 55	UPDA1980
	IF (DABS(TQTEST(K)).GT.VISC(4,K3J)) JEULER = -NLOCK	UPDA1990
	GO TO 55	UPDA2000



52	IF (VISC(5,K3J).EQ.0.0) GO TO 53	UPDA2010
	IF (DABS(TQTEST(K)).LT.VISC(5,K3J)) JEULER = NLOCK	UPDA2020
	GO TO 55	UPDA2030
53	IF (VISC(6,K3J).EQ.0.0) GO TO 55	UPDA2040
	IF (DABS(ANGD(K,J)).LT.VISC(6,K3J)) JEULER = NLOCK	UPDA2050
55	CONTINUE	UPDA2060
	IF (JEULER.EQ.1EULER(J)) GO TO 60	UPDA2070
	IF (JEULER.EQ.8) GO TO 59	UPDA2080
	MODE = -1	UPDA2090
	K = JEULER	UPDA2100
	IF (K.LE.3) GO TO 57	UPDA2110
	MODE = 1	UPDA2120
	K = K-3	UPDA2130
	IF (K.GT.3) MODE=0	UPDA2140
57	1EULER(J) = 8	UPDA2150
	IPIN(J) = 4	UPDA2160
	CALL IMPLS2(MODE,J,H1R(1,K,J))	UPDA2170
	1 = -1	UPDA2180
59	1EULER(J) = JEULER	UPDA2190
	IPIN(J) = 4	UPDA2200
	IF (1EULER(J).NE.8) IPIN(J) = -4	UPDA2210
60	CONTINUE	UPDA2220
C		UPDA2230
39	IF (NQ.LE.0) GO TO 99	UPDA2240
	DO 40 K=1,NQ	UPDA2250
	IF (KQTYPE(K).LT.3) GO TO 40	UPDA2260
	IF (KQTYPE(K).GT.4) GO TO 40	UPDA2270
	IF (CFQQ(K).LT.0.0) KQTYPE(K) = -KQTYPE(K)	UPDA2280
	IF (CFQQ(K).LT.0.0) GO TO 42	UPDA2290
C		UPDA2300
C	TEST IF ROLLING CONSTRAINT SHOULD BE SLIDING AND VICE VERSA.	UPDA2310
C		UPDA2320
	QN = -XDY(TQQ(1,K),HHT(1,1,K),QQ(1,K))	UPDA2330
	IF (NPRT(24).NE.0) WRITE (6,41) KQTYPE(K),KQ1(K),KQ2(K),	UPDA2340
	* (RK1(11,K),11=1,3),(RK2(11,K),11=1,3),	UPDA2350
	* ((HHT(11,J,K),J=1,3),11=1,3),	UPDA2360
	* (QQ(11,K),11=1,3),(TQQ(11,K),11=1,3),(RQQ(11,K),11=1,3),	UPDA2370
	* (HQQ(11,K),11=1,3),SQQ(K),CFQQ(K),QN	UPDA2380
41	FORMAT('O UPDATE ROLL-SLIDE TEST'/(2X,9G14.6))	UPDA2390
	IF (QN.LT.0.0) KQTYPE(K) = -4	UPDA2400
	IF (QN.LT.0.0) GO TO 42	UPDA2410
	QDOTQ = QQ(1,K)**2 + QQ(2,K)**2 + QQ(3,K)**2	UPDA2420
	QT = DSQRT(QDOTQ-QN**2)	UPDA2430
	IF (KQTYPE(K).EQ.3 .AND. QT.LE.CFQQ(K)*QN) GO TO 40	UPDA2440
	IF (KQTYPE(K).EQ.4 .AND. QT.GE.0.9*CFQQ(K)*QN) GO TO 40	UPDA2450
	KQTYPE(K) = 7-KQTYPE(K)	UPDA2460
42	CALL OUTPUT(C)	UPDA2470
	CALL SETUP2	UPDA2480
	CALL DAUX(K)	UPDA2490
	CALL OUTPUT(1)	UPDA2500



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CALL PRINT(6HUPDATE)
I = -1
40 CONTINUE
99 CALL ELTIME(2,7)
RETURN
END
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UPDA2510
UPDA2520
UPDA2530
UPDA2540
UPDA2550
UPDA2560
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	SUBROUTINE VEHPOS	REV 12 12/16/74	VEHP0010
C			VEHP0020
C	COMPUTE COMPONENTS OF VEHICLE POSITION AND MOTION AS A FUNCTION		VEHP0030
C	OF TIME USING DATA AND TABLES PRODUCED BY SUBROUTINE VINPUT.		VEHP0040
C			VEHP0050
	IMPLICIT REAL*8 (A-H,O-Z)		VEHP0060
	COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)		VEHP0070
	COMMON/SGMNTS/O(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)		VEHP0080
	* ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)		VEHP0090
	COMMON/VPOSTN/ TIME,XO(3),XDOTO(3),XCOMP(3),XVCOMP(3),AX(3),		VEHP0100
	* ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,		VEHP0110
	* NATAB,NACLR,DVEH(3,3),VMEG(3),VMEGO(3),XACOMP(3),		VEHP0120
	* THET(3),ZPLT(3)		VEHP0130
	COMMON/CNSNTS/ PI, RADIAN,G,THIRO,EPS1,EPS4,EPS6,EPS8,		VEHP0140
	* EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)		VEHP0150
	DIMENSION AC(3)		VEHP0160
	DATA TLAST/-100000.0/		VEHP0170
	T = TIME		VEHP0180
	IF(NATAB.NE.0) GO TO 20		VEHP0190
C			VEHP0200
C	HALF-SINE WAVE DECELERATION		VEHP0210
C			VEHP0220
	IF(T.GT.VTIME) T=VTIME		VEHP0230
	WT = OMEGA*T		VEHP0240
	CWT1 = OCOS(WT)-1.0		VEHP0250
	SWT = OSIN(WT)		VEHP0260
	DO 10 I=1,3		VEHP0270
	AW = AX(I)*OMEGA		VEHP0280
	XACOMP(I) = -AW*OMEGA*SWT		VEHP0290
	XCOMP(I) = AX(I)*SWT + 1*(XDOTO(I)-AW)+XO(I)		VEHP0300
	10 XVCOMP(I) = AW*CWT1 + XDOTO(I)		VEHP0310
	GO TO 99		VEHP0320
	20 IF (NATAB.LT.0) GO TO 30		VEHP0330
C			VEHP0340
C	UNIDIRECTIONAL DECELERATION		VEHP0350
C			VEHP0360
	IF (T.LT.VTIME) GO TO 21		VEHP0370
C			VEHP0380
C	TIME POINT EXCEEDS TABLE, EXTRAPOLATE.		VEHP0390
C			VEHP0400
	DLT = T-VTIME		VEHP0410
	ACO = ATAB(1,NATAB)		VEHP0420
	AC(1) = ATAB(2,NATAB) + G*ACO*OLT		VEHP0430
	AC(2) = ATAB(3,NATAB) + AC(1)*DLT + 0.5*G*ACO*DLT**2		VEHP0440
	GO TO 25		VEHP0450
C			VEHP0460
C	USE QUADRATIC INTERPOLATION FROM TABLES FOR CURRENT VALUE OF		VEHP0470
C	TIME TO BE CONSISTENT WITH SIMPSON INTEGRATION OF TABLES.		VEHP0480
C			VEHP0490
	21 J= 0.5*(T-ATO)/ADT +1.0		VEHP0500

XK = T/ADT -DFLOAT(2*J-1)	VEHP0510
X1 = XK+1.0	VEHP0520
X2 = XK**2-XK+1.0	VEHP0530
X3 = XK-1.0	VEHP0540
UNITS = -G	VEHP0550
DO 23 I=1,2	VEHP0560
T1 = (ATAB(I,2*J-1)-2.0*ATAB(I,2*J)+ATAB(I,2*J+1))/6.0	VEHP0570
T2 = (ATAB(I,2*J+1)-ATAB(I,2*J-1))/4.0	VEHP0580
T3 = ATAB(I,2*J)	VEHP0590
AC(I) = ATAB(I+1,2*J-1)+ADT*X1*(X2*T1+X3*T2+T3)*UNITS	VEHP0600
23 UNITS = 1.0	VEHP0610
ACC = 0.5*XK*X3*ATAB(1,2*J-1)	VEHP0620
* - X3*X1*ATAB(1,2*J )	VEHP0630
* + 0.5*XK*X1*ATAB(1,2*J+1)	VEHP0640
C	VEHP0650
C	VEHP0660
C	VEHP0670
COMPONENTS OF VEHICLE ACCELERATION, VELOCITY AND POSITION.	VEHP0680
25 DO 29 I=1,3	VEHP0690
XACOMP(I) = -G*AX(I)*ACC	VEHP0700
XVCOMP(I) = AX(I)*AC(1)	VEHP0710
29 XCOMP(I) = X0(I)+AX(I)*AC(2)	VEHP0720
GO TO 99	VEHP0730
C	VEHP0740
C	VEHP0750
C	VEHP0760
OMNIDIRECTIONAL DECELERATION	VEHP0770
30 IF (TIME.EQ.TLAST) GO TO 99	VEHP0780
DLTA = TIME-TLAST	VEHP0790
IF (TLAST.EQ.-100000.0) DLTA = 0.0	VEHP0800
TLAST = TIME	VEHP0810
J = (TIME-ATO)/ADT+1.0	VEHP0820
IF (J.GE.-NATAB) GO TO 32	VEHP0830
C	VEHP0840
C	VEHP0850
C	VEHP0860
C	VEHP0870
INTERPOLATION FROM VINPOT TABLES OF COMPONENTS OF VEHICLE	VEHP0880
LINEAR AND ANGULAR ACCELERATION, VELOCITY AND DISPLACEMENT.	VEHP0890
TJ = ATO + DFLOAT(J-1)*ADT	VEHP0900
DLT = TIME-TJ	VEHP0910
DO 31 I=1,3	VEHP0920
AL2 = (ATAB(I,J+1)-ATAB(I,J))*DLT/ADT*G	VEHP0930
AL1 = G*ATAB(I,J)	VEHP0940
XACOMP(I) = -AL1-AL2	VEHP0950
AL2 = 0.5*AL2	VEHP0960
XVCOMP(I) = ATAB(I+3,J)-DLT*(AL1+AL2)	VEHP0970
XCOMP(I) = ATAB(I+6,J)+DLT*(ATAB(I+3,J)-DLT*(0.5*AL1+AL2/3.0))	VEHP0980
AA2 = (ATAB(I+9,J+1)-ATAB(I+9,J))*RADIAN/ADT	VEHP0990
THET(I) = DLTA*(VMEG(I)+DLTA*(0.5*VMEGD(I)+DLTA*AA2/6.0))	VEHP1000
AA2 = AA2 * DLT	
AA1 = ATAB(I+9,J)*RADIAN	
VMEGD(I) = AA1 + AA2	
31 VMEG(I) = ATAB(I+12,J)*RADIAN + DLT*(AA1+0.5*AA2)	

	GO TO 34	VEHP1010
C		VEHP1020
C	TIME POINT EXCEEDS TABLE, EXTRAPOLATE.	VEHP1030
C		VEHP1040
	32 J = - NATAB	VEHP1050
	TJ = ATO + DFLOAT(J-1)*ADT	VEHP1060
	DLT = TIME-TJ	VEHP1070
	DO 33 I=1,3	VEHP1080
	XACOMP(1) = ATAB(I,J)*G	VEHP1090
	XVCOMP(I) = ATAB(I+3,J) +G*ATAB(I,J)*DLT	VEHP1100
	XCOMP (I) = ATAB(I+6,J) +ATAB(I+3,J)*DLT + 0.5*G*ATAB(I,J)*DLT**2	VEHP1110
	VMEGD(I) = 0.0	VEHP1120
	VMEG (I) = ATAB(I+12,J)*RADIAN	VEHP1130
	33 THET (I) = DLTA*VMEG(I)	VEHP1140
C		VEHP1150
C	UPDATE DIRECTION COSINE MATRIX OF VEHICLE.	VEHP1160
C		VEHP1170
	34 CALL DSETD(DVEH,THET,THT)	VEHP1180
C		VEHP1190
C	STORE VEHICLE DATA INTO NVEH SEGMENT DATA.	VEHP1200
C		VEHP1210
	99 DO 42 I=1,3	VEHP1220
	DO 41 J=1,3	VEHP1230
	41 D(I,J,NVEH) = DVEH(I,J)	VEHP1240
	SEGLP(I,NVEH) = XCOMP(1)	VEHP1250
	SEGLV(I,NVEH) = XVCOMP(I)	VEHP1260
	SEGLA(1,NVEH) = XACOMP(1)	VEHP1270
	WMEG (1,NVEH) = VMEG (I)	VEHP1280
	42 WMEGD(I,NVEH) = VMEGD(I)	VEHP1290
	RETURN	VEHP1300
	END	VEHP1310

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C          SUBROUTINE VINPUT                                VINPG010
C                                                     REV 12 12/16/74VINPG020
C PERFORMS CARD INPUT AND COMPUTES DATA AND TABLES REQUIRED BY VINPG030
C SUBROUTINE VEHPOS TO INTEGRATE THE CRASH VEHICLE MOTION FOR ONE OFVINPG040
C THREE PERMISSABLE OPTIONS: VINPG050
C   (1) HALF SINE-WAVE LINEAR DECELERATION IMPULSE VINPG060
C   (2) UNIDIRECTIONAL LINEAR DECELERATION TABULAR INPUT VINPG070
C   (3) OMNIDIRECTIONAL LINEAR AND ANGULAR ACCELERATION TABULAR VINPG080
C       INPUT (6 DEGREES OF FREEDOM VEHICLE MOTION) VINPG090
C                                                     VINPG100
C IMPLICIT REAL*8 (A-H,O-Z) VINPG110
C COMMON/CONTRL/NSEG,NJN,N3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40) VINPG120
C COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22) VINPG130
C *      ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22) VINPG140
C COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42) VINPG150
C *      ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63) VINPG160
C *      ,VISC(7,63),JNT(21),IPIN(21),NS,ISING(22) VINPG170
C COMMON/VPOSTN/ TIME,X0(3),XDOT0(3),XCOMP(3),XVCOMP(3),AX(3), VINPG180
C *      ,ANGLE(3),VMPPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA, VINPG190
C *      ,NATAB,NACLR,DVEH(3,3),VMEG(3),VMEGD(3),XACOMP(3), VINPG200
C *      ,THET(3),ZPLT(3) VINPG210
C COMMON/CNSNTS/ PI, RADIANT,G,THIRD,EPS1,EPS4,EPS6,EPS8, VINPG220
C *      ,EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)VINPG230
C COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),BLTTTL(5,8)VINPG240
C *      ,PLTTL(5,20),BAGTTL(5,6),SEG(22),JOINT(21) VINPG250
C *      ,CGS(22),JS(21) VINPG260
C REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT VINPG270
C LOGICAL*1 CGS,JS VINPG280
C REAL VEH,GRND VINPG290
C DATA VEH/' VEH'/,GRND/'GRND'/ VINPG300
C VINPG310
C READ AND PRINT CONTENTS OF CARDS C.1 AND C.2 VINPG320
C VINPG330
C READ (5,10) VPSTTL VINPG340
10 FORMAT (20A4) VINPG350
C READ(5,11) ANGLE,VMPPH,VTIME,X0,NATAB,ATO,ADT VINPG360
11 FORMAT(8F6.0,I6,2F6.0) VINPG370
C WRITE (6,14) VPSTTL,ANGLE,VMPPH,VTIME,X0,NATAB,ATO,ADT VINPG380
14 FORMAT('1 VEHICLE DECELERATION INPUTS',91X,'CARDS C'// VINPG390
C *      ,3X,20A4//7X,'YAW',9X,'PITVINPG400
C *CH',7X,'ROLL',8X,'VMPPH',8X,'VTIME',7X,'X0(X)',7X,'X0(Y)',7X,'X0(Z)VINPG410
C *',7X,'NATAB',4X,'ATO',9X,'ADT'/8F12.3,I10,2X,2F12.6) VINPG420
C VIPS = VMPPH VINPG430
C DA1 = ANGLE(1)*RADIAN VINPG440
C DA2 = ANGLE(2)*RADIAN VINPG450
C AX(3) = DCOS(DA2) VINPG460
C AX(1) = DCOS(DA1)*AX(3) VINPG470
C AX(2) = DSIN(DA1)*AX(3) VINPG480
C AX(3) = DSIN(DA2) VINPG490
C IF(NATAB.NE.0) GO TO 20 VINPG500

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C		VINP0510
C	HALF-SINE WAVE DECELERATION	VINP0520
C		VINP0530
	DMEGA = PI/VTIME	VINP0540
	AT = 0.5*VIPS/DMEGA	VINP0550
	IF (VIPS.LT.0.0) VIPS = 0.0	VINP0560
	DO 12 I=1,3	VINP0570
	XDDT0(I) = VIPS*AX(I)	VINP0580
12	AX(I) = AT*AX(I)	VINP0590
	WRITE (6,I3) VIPS,UNITL,UNITT,ANGLE,VTIME,UNITT	VINP0600
13	FORMAT('0 PASSENGER COMPARTMENT DISPLACEMENT HISTORY'/	VINP0610
	* ' ANALYTICAL HALF-SINE WAVE DECELERATION'/	VINP0620
	* ' VG=',F8.3,1X,A4,'/',A4,' OBLIQUE ANGLES =',3F7.2,	VINP0630
	* ' DEGREES, TIME DURATION =',F7.3,1X,A4//)	VINP0640
	GO TO 41	VINP0650
20	IF (NATAB.LT.0) GO TO 50	VINP0660
C		VINP0670
C	FOR UNIDIRECTIONAL VEHICLE MOTION	VINP0680
C	READ LINEAR DECELERATION TABLES FROM CARDS C.3	VINP0690
C		VINP0700
	READ (5,21) (ATAB(I,I),I=1,NATAB)	VINP0710
21	FORMAT (I2F6.0)	VINP0720
C		VINP0730
C	EXTEND TABLE IF NECESSARY SUCH THAT NATAB IS ODD AND	VINP0740
C	LAST ENTRY NEED NOT BE ZERO. IF TABLE SIZE IS EXCEEDED ON TIME,	VINP0750
C	VALUE OF LAST ENTRY WILL BE USED.	VINP0760
C		VINP0770
	IF (MOD(NATAB,2).EQ.1) GO TO 23	VINP0780
	ATAB(1,NATAB+1) = ATAB(1,NATAB)	VINP0790
	NATAB = NATAB+1	VINP0800
23	VTIME = ADT * DFLOAT(NATAB-1)	VINP0810
C		VINP0820
C	USING SIMPSON'S INTEGRATION, COMPUTE VELOCITY AND DISPLACEMENT	VINP0830
C	TABLE FOR NATAB EQUALLY SPACED (ADT) TIME POINTS.	VINP0840
C	FOR I=1,NATAB	VINP0850
C	ATAB(1,I) = LINEAR DECELERATION (G'S)	VINP0860
C	ATAB(2,I) = LINEAR VELOCITY (L UNITS/T UNITS)	VINP0870
C	ATAB(3,I) = LINEAR DISPLACEMENT (L UNITS)	VINP0880
C		VINP0890
	ATAB(2,1) = VIPS	VINP0900
	ATAB(3,1) = 0.0	VINP0910
	DA1 = ADT/3.0	VINP0920
	DA2 = ADT/12.0	VINP0930
	UNITS = -G	VINP0940
	DO 30 J=2,3	VINP0950
	DO 25 I=2,NATAB,2	VINP0960
	F1 = ATAB(J-1,I-1) * UNITS	VINP0970
	F2 = ATAB(J-1,I) * UNITS	VINP0980
	F3 = ATAB(J-1,I+1) * UNITS	VINP0990
	ATAB(J,I) = ATAB(J,I-1) + DA2*(5.0*F1+8.0*F2-F3)	VINP1000



25	ATAB(J,I+1) = ATAB(J,I-1) + DA1*( F1+4.0*F2+F3)	VINP1010
30	UNITS = 1.0	VINP1020
C		VINP1030
C	PRINT TABLES	VINP1040
C		VINP1050
	WRITE (6,36) (UNITL,UNITT,UNITL,I=1,2)	VINP1060
36	FORMAT('C UNIDIRECTIONAL VEHICLE POSITION TABLES'//	VINP1070
*	2(' TIME ACC VELOCITY POSITION ')/	VINP1080
*	2(' (MILLESEC) (G) (' ,A4,'/' ,A4,')' ,5X,'(' ,A4,')' )/)	VINP1090
	DO 40 J=1,50	VINP1100
	IF (J.GT.NATAB) GO TO 40	VINP1110
	T1 = (AT0 + DFLOAT(J-1)*ADT)*1000.0	VINP1120
	IF (J+50.LE.NATAB) GO TO 38	VINP1130
	WRITE (6,37) T1,(ATAB(I,J),I=1,3)	VINP1140
37	FORMAT(2(F11.5,F10.2,F13.4,F13.5,3X))	VINP1150
	GO TO 40	VINP1160
38	T2 = (AT0 + DFLOAT(J+49)*ADT)*1000.0	VINP1170
	WRITE (6,37) T1,(ATAB(I,J),I=1,3),T2,(ATAB(I,J+50),I=1,3)	VINP1180
40	CONTINUE	VINP1190
C		VINP1200
C	INITIALIZATION	VINP1210
C		VINP1220
	DO 35 I=1,3	VINP1230
35	XDOT0(I)= VIPS*AX(I)	VINP1240
41	DO 43 I=1,3	VINP1250
	DO 42 J=1,3	VINP1260
42	DVEH(1,J) = 0.0	VINP1270
	DVEH(I,I) = 1.0	VINP1280
	VMEGD(I) = 0.0	VINP1290
43	VMEG(I) = 0.0	VINP1300
	GO TO 99	VINP1310
C		VINP1320
C	FOR OMNIDIRECTIONAL (6 DEGREES OF FREEDOM) VEHICLE MOTION	VINP1330
C	READ LINEAR DECELERATION AND AUGULAR ACCELERATION TABLES	VINP1340
C	FROM CARDS C.4.	VINP1350
C		VINP1360
50	MATAB = -NATAB	VINP1370
	READ(5,51) ((ATAB(I,J),I=1,3),(ATAB(1,J),I=10,12),J=1,MATAB)	VINP1380
51	FORMAT(10X,6F10.0)	VINP1390
	DO 60 J=1,MATAB	VINP1400
	IF (MOD(J,50).NE.1) GO TO 53	VINP1410
C		VINP1420
C	PRINT PAGE HEADING AT START OF EACH 50 TIME POINTS.	VINP1430
C		VINP1440
	IF (J.NE.1) WRITE (6,44)	VINP1450
44	FORMAT('1')	VINP1460
	IPAGE = (J-1)/50 + 1	VINP1470
	WRITE (6,52) IPAGE,UNITL,UNITT,UNITL,UNITT	VINP1480
52	FORMAT('O ROTATING VEHICLE LINEAR TIME HISTORY',	VINP1490
*	67X,'PAGE NO.',I3//	VINP1500

*	4X,'TIME',12X,'LINEAR DECELERATIONS (G''S)',	VINP1510
*	10X,'LINEAR VELOCITIES ('A4','/'A4,')',	VINP1520
*	11X,'LINEAR DISPLACEMENTS ('A4,')' /	VINP1530
\$	3X,'('A4,')',3(11X,'X',11X,'Y',11X,'Z',3X) / )	VINP1540
53	IF (J.GT.1) GO TO 57	VINP1550
C		VINP1560
C	INTEGRATION INITIALIZATION FOR TIME = 0.	VINP1570
C		VINP1580
	DO 54 I=1,3	VINP1590
	ATAB(I+6,J) = X0(I)	VINP1600
	ATAB(I+12,J) = 0.0	VINP1610
54	THET(I) = ANGLE(I)*RADIAN	VINP1620
	CALL DRCYPR(DVEH,ANGLE,3,2,1)	VINP1630
	DO 55 I=1,3	VINP1640
	XDOT0(I) = VIPS*DVEH(1,I)	VINP1650
55	ATAB(I+3,J) = XDOT0(I)	VINP1660
	GO TO 59	VINP1670
57	DO 58 I=1,3	VINP1680
C		VINP1690
C	INTEGRATE LINEAR VELOCITY AND DISPLACEMENT.	VINP1700
C		VINP1710
	ATAB(I+3,J) = ATAB(I+3,J-1)-G*ADT/2.0*(ATAB(I,J-1)+ATAB(I,J))	VINP1720
58	ATAB(I+6,J) = ATAB(I+6,J-1)	VINP1730
	* +ADT*(ATAB(I+3,J-1)-G*ADT/6.0*(2.0*ATAB(I,J-1)+ATAB(I,J)))	VINP1740
59	T1 = (ATO + DFLOAT(J-1)*ADT)	VINP1750
60	WRITE(6,61) T1,(ATAB(I,J),I=1,9)	VINP1760
61	FORMAT(F9.5,3(3X,3F12.3))	VINP1770
	DO 70 J=1,MATAB	VINP1780
	IF(MOD(J,50).NE.1) GO TO 63	VINP1790
C		VINP1800
C	PRINT PAGE HEADING AT START OF EACH 50 TIME POINTS.	VINP1810
C		VINP1820
	IPAGE = (J-1)/50+1	VINP1830
	WRITE (6,62) IPAGE,UNITT,UNITT,UNITT	VINP1840
62	FORMAT('1 ROTATING VEHICLE ANGULAR TIME HISTORY',	VINP1850
	* 66X,'PAGE NO.',I3//	VINP1860
	* 4X,'TIME', 6X,'ANGULAR ACCELERATIONS (DEG/'A4,'**2)',	VINP1870
	* 10X,'ANGULAR VELOCITIES (DEG/'A4,')',	VINP1880
	* 11X,'ANGULAR DISPLACEMENTS (DEG)' /	VINP1890
	* 3X,'('A4,')',2(11X,'X',11X,'Y',11X,'Z',3X),	VINP1900
	* 10X,'YAW',8X,'PITCH',8X,'ROLL' /)	VINP1910
63	IF(J.EQ.1) GO TO 65	VINP1920
C		VINP1930
C	INTEGRATE ANGULAR VELOCITY AND DISPLACEMENT.	VINP1940
C		VINP1950
	DO 64 I=1,3	VINP1960
	ATAB(I+12,J) = ATAB(I+12,J-1)+(ATAB(I+9,J-1)+ATAB(I+9,J))*ADT/2.0	VINP1970
64	THET(I) = ADT*(ATAB(I+12,J-1)+(2.0*ATAB(I+9,J-1)+ATAB(I+9,J))*ADT	VINP1980
	*/6.0)*RADIAN	VINP1990
	CALL DSETD(DVEH,THET,THT)	VINP2000

65	CALL YPRDEG(DVEH,THET)	VINP2010
	T1 = (ATO + DFLOAT(J-1)*ADT)	VINP2020
70	WRITE (6,71) T1,(ATAB(1,J),1=10,15),THET	VINP2030
71	FORMAT(F9.5,3(3X,3F12.3))	VINP2040
C		VINP2050
C	PROGRAM INITIALIZATION FOR TIME = 0.	VINP2060
C		VINP2070
	CALL DRCYPR (DVEH,ANGLE,3,2,1)	VINP2080
	DO 72 I=1,3	VINP2090
	VMEG(I) = ATAB(I+12,1)*RADIAN	VINP2100
72	VMEGD(I) = ATAB(I+9,1)*RADIAN	VINP2110
C		VINP2120
C	SET UP SEGMENT DATA FOR GROUND.	VINP2130
C		VINP2140
99	NVEH = NSEG+1	VINP2150
	NGRND = NVEH+1	VINP2160
	SEG(NVEH) = VEH	VINP2170
	SEG(NGRND) = GRND	VINP2180
	IF (NVEH -1.GT.NJNT) JNT (NVEH -1) = 0	VINP2190
	IF (NVEH -1.GT.NJNT) IPIN(NVEH -1) = 0	VINP2200
	IF (NGRND-1.GT.NJNT) JNT (NGRND-1) = 0	VINP2210
	IF (NGRND-1.GT.NJNT) IPIN(NGRND-1) = 0	VINP2220
	DO 82 I=1,3	VINP2230
	DO 81 J=1,3	VINP2240
81	D(I,J,NGRND) = 0.0	VINP2250
	D(I,I,NGRND) = 1.0	VINP2260
	SEGLP(1,NGRND) = 0.0	VINP2270
	SEGLA(I,NGRND) = 0.0	VINP2280
	SEGLV(I,NGRND) = 0.0	VINP2290
	WMEG (I,NGRND) = 0.0	VINP2300
82	WMEGD(I,NGRND) = 0.0	VINP2310
	DO 83 J=NVEH,NGRND	VINP2320
	W(J) = 0.0	VINP2330
	RW(J) = 0.0	VINP2340
	DO 83 I=1,3	VINP2350
	PHI(I,J) = 0.0	VINP2360
83	RPHI(I,J) = 0.0	VINP2370
	RETURN	VINP2380
	END	VINP2390

C	SUBROUTINE VISPR(IJ,NJ)	REV 12 12/19/74	VISP0010
C	COMPUTES VISCOS AND SPRING TORQUES AT THE JOINTS		VISP0020
C	AND ADDS THEM TO THE U2 ARRAY.		VISP0030
C			VISP0040
C	ARGUMENTS:		VISP0050
C	NJ = 0 - REGULAR COMPUTATION FOR ALL JOINTS		VISP0060
C	# 0 - COMPUTE ONLY FOR JOINT NJ IMPULSE		VISP0070
C			VISP0080
C	IJ = 1 IMPULSE FOR FLEXURE ONLY		VISP0090
C	= 2 IMPULSE FOR TORSION ONLY		VISP0100
C	= 4 IMPULSE FOR GLOBALGRAPHIC ONLY		VISP0110
C			VISP0120
C			VISP0130
	IMPLICIT REAL*8 (A-H,O-Z)		VISP0140
	COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)		VISP0150
	COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)		VISP0160
*	,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63)		VISP0170
*	,VISC(7,63),JNT(21),IPIN(21),NS,ISING(22)		VISP0180
*	,IGLOB(21),JOINTF(21)		VISP0190
	COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)		VISP0200
*	,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)		VISP0210
	COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),		VISP0220
*	NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21)		VISP0230
	COMMON/CMATRX/V1(3,21),V2(3,21),V3(3,12),B12(3,3,42),A22(3,3,42)		VISP0240
*	,F(3,21),TQ(3,21),WJ(21)		VISP0250
	COMMON/CEULER/ IEULER(22),HIR(3,3,21),ANG(3,21),ANGD(3,21),		VISP0260
*	FE(3,21),TQE(3,31),CONST(3,21)		VISP0270
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)		VISP0280
	COMMON/TEMPVS/T1(3),T2(3),T3(3),T4(3),T5(3),T6(3),T7(3),T8(3)		VISP0290
*	,T9(3),HAD,HBD,WIJM,CV,CSA,CSB,WIJ(3),ANGL(3),TQC		VISP0300
*	,THETO,THETOP,DH1(3,3),DH2(3,3),HD3(3,3),CC(3)		VISP0310
	COMMON/TEMPVI/ TTI(3),RII(3),R2I(3),CREST,JSTOP(4,2,21)		VISP0320
	COMMON/CNSNTS/ PI, RADIANT,G,THIRD,EPS1,EPS4,EPS6,EPS8,		VISP0330
*	EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)		VISP0340
	COMMON /VPOSTN/ TIME		VISP0350
	IF (NJNT.LE.0) GO TO 99		VISP0360
	CALL ELTIME(1,13)		VISP0370
	IF (NPRT(12).NE.0) WRITE (6,11) TIME		VISP0380
11	FORMAT('1 VISPR COMPUTATIONS FOR TIME =',F12.6)		VISP0390
	J1 = 1		VISP0400
	J2 = NJNT		VISP0410
	IF (NJ.EQ.0) GO TO 13		VISP0420
	J1 = NJ		VISP0430
	J2 = NJ		VISP0440
13	DO 90 J=J1,J2		VISP0450
	DO 12 L=1,3		VISP0460
12	TQ(L,J) = 0.0		VISP0470
	WJ(J) = 0.0		VISP0480
C			VISP0490
C	DO NOT COMPUTE TORQUES FOR NULL, LOCKED OR EULER JOINTS.		VISP0500

C	I = IABS(JNT(J))	VISP0510
	IF (I.LE.0) GO TO 90	VISP0520
	IF (IPIN(J).LT.0 .OR. IPIN(J).GT.3) GO TO 90	VISP0530
C		VISP0540
C	ZERO T1-T9 ARRAYS, VARIABLES HAD,HBD,WIJM,CV,CSA, AND CS8,	VISP0550
C	WIJ AND ANGL ARRAYS AND VARIABLES TQC,THETO AND THETOP.	VISP0560
C		VISP0570
	DO 10 L=1,42	VISP0580
10	TI(L) = 0.0	VISP0590
	CALL DOT(D(1,1,I ),HT(I,I,2*J-1),DH1,3,3,3)	VISP0600
	CALL DOT(D(1,1,J+1),HT(1,I,2*J ),DH2,3,3,3)	VISP0610
	CALL DOT(DH1,DH2,HD3,3,3,3)	VISP0620
C		VISP0630
C	NOTE: THIS VERSION CORRESPONDS TO OLDER VERSIONS AS FOLLOWS:	VISP0640
C		VISP0650
C	(HT) = ( (HC) (H8) (HA) )	VISP0660
C		VISP0670
C	(DH1) = ( (A) (T2) (TI) )	VISP0680
C		VISP0690
C	(DH2) = ( (B) (T5) (T4) )	VISP0700
C		VISP0710
C	WHERE A = T2 X T1	VISP0720
C	B = T5 X T4	VISP0730
C		VISP0740
C	( A.B A.T5 A.T4 )	VISP0750
C	(HD3) = ( T2.8 T2.T5 T2.T4 )	VISP0760
C	( T1.B TI.T5 TI.T4 )	VISP0770
C		VISP0780
C		VISP0790
	HAD = HD3(3,3)	VISP0800
	IF (HAD.GT. 1.0) HAD = 1.0	VISP0810
	IF (HAD.LT.-1.0) HAD = -1.0	VISP0820
	ANGL(1) = DARCOS(HAD)	VISP0830
	ANGL(2) = 0.0	VISP0840
	IF (HD3(2,3).NE.0.0 .OR. HD3(1,3).NE.0.0)	VISP0850
*	ANGL(2) = DATAN2(HD3(2,3),HD3(1,3))	VISP0860
	CSAP = 0.0	VISP0870
	IF (NJ.NE.0.AND.IJ.EQ.4) GO TO 27	VISP0880
C		VISP0890
C	CONVERT TO INERTIAL REFERENCE SYSTEM	VISP0900
C	T3= D(I)*WMEG(I) T6=D(J+1)*WMEG(J+1)	VISP0910
C		VISP0920
C	HAD = COS TA = HD3(3,3)	VISP0930
C	WIJ = T3-T6	VISP0940
C	WJ =  WIJ	VISP0950
C		VISP0960
	DO 20 L=1,3	VISP0970
	DO 15 M=1,3	VISP0980
	T3(L) = T3(L)+ D(M,L,I)* WMEG(M,I)	VISP0990
15	T6(L) = T6(L)+ D(M,L,J+1)* WMEG(M,J+I)	VISP1000



	WIJ(L)= T3(L)-T6(L)	VISP1010
20	WIJM = WIJM + WIJ(L)**2	VISP1020
	WIJM = DSQRT(WIJM)	VISP1030
	WJ(J) = WIJM	VISP1040
C		VISP1050
C	T7 = T1 X T4	VISP1060
C	HAC =  T7	VISP1070
C		VISP1080
	CALL CROSS (DH1(1,3),DH2(1,3),T7)	VISP1090
	HAC = DSQRT((1.0-HAD)*(1.0+HAD))	VISP1100
C		VISP1110
C	COMPUTE CV, THE MAGNITUDE OF VISCOUS AND COULOMB TORQUE/WIJM	VISP1120
C	RA = -SGN TA DOT = WIJ.T7	VISP1130
C	AND CSA, THE MAGNITUDE OF FLEXURE TORQUE/HAC	VISP1140
C		VISP1150
	CV = VISCOS(WIJM,VISC(1,3*J-2))	VISP1160
	CREST = VISC(7,3*J-2)	VISP1170
	RA = WIJ(1)*T7(1)+WIJ(2)*T7(2)+WIJ(3)*T7(3)	VISP1180
	JSTP = 0	VISP1190
	IF (JOINTF(J).EQ.0) CSA = EFUNCT(ANGL(1),RA,SPRING(1,3*J-2),JSTP)	VISP1200
	IF (JOINTF(J).NE.0) CSA = FINTERP(ANGL(1),ANGL(2),JOINTF(J))	VISP1210
	CSAP = CSA	VISP1220
	IF (HAC.NE.0.0) CSA = CSA/HAC	VISP1230
	IF (NJ.EQ.0) JSTOP(1,1,J) = JSTP	VISP1240
	IF (IP1N(J).EQ.1) GO TO 34	VISP1250
C		VISP1260
C	FOR UNPINNED FREE JOINTS	VISP1270
C	CONVERT TO INERTIAL REFERENCE SYSTEM	VISP1280
C	T2 = D(I)*HB(NJ) T5 = D(J+1)*HB(MJ)	VISP1290
C		VISP1300
C	T8 = T2 X T5	VISP1310
C	HBD = COS T8 = T2.T5	VISP1320
C	HBC =  T8	VISP1330
C		VISP1340
	ANGL(3) = DATAN2(HD3(2,1)-HD3(1,2),HD3(2,2)+HD3(1,1))	VISP1350
C		VISP1360
C	RB = -SGN T8 DOT = WIJ.T8	VISP1370
C	COMPUTE CSB, THE MAGNITUDE OF TORSIONAL TORQUE.	VISP1380
C		VISP1390
	RB = WIJ(1)*DH2(1,3) + WIJ(2)*DH2(2,3) + WIJ(3)*DH2(3,3)	VISP1400
	CSB = EFUNCT(ANGL(3),RB,SPRING(1,3*J-1),JSTP)	VISP1410
	IF (NJ.EQ.0) JSTOP(2,1,J) = JSTP	VISP1420
	IF (NJ.GT.0) GO TO 34	VISP1430
C		VISP1440
C	COMPUTE EFFECT OF GLOBALGRAPHIC JOINT STOP	VISP1450
C		VISP1460
27	IF (IGLOB(J).EQ.0) GO TO 34	VISP1470
	IF (DABS(HAD).GT.1.0-EPS6) GO TO 34	VISP1480
	NT = IGLOB(J)	VISP1490
	CALL HERRON(HD3(1,3),NTAB(NT+1),THETO,THETOP)	VISP1500



JSTOP(4,1,J) = 0	VISP1510
IF (ANGL(1).LE.THETO) GO TO 34	VISP1520
JSTOP(4,1,J) = 1	VISP1530
MT = NTAB(NT+5)	VISP1540
CREST = TAB(MT+3)	VISP1550
STH2 = 1.0-HAD**2	VISP1560
STH = DSQRT(STH2)	VISP1570
CTH = HAD/STH	VISP1580
CST = DSQRT(STH2+THETOP**2)	VISP1590
DR = (ANGL(1)-THETO)*STH/CST	VISP1600
LT = NTAB(NT)	VISP1610
TAB(LT) = DR	VISP1620
TQF = FRCDL(DR,NT,1)	VISP1630
TQC = TQF/CST	VISP1640
CC(1) = -HD3(2,3) + HD3(1,3)*CTH*THETOP	VISP1650
CC(2) = HD3(1,3) + HD3(2,3)*CTH*THETOP	VISP1660
CC(3) = -STH*THETOP	VISP1670
DO 28 L=1,3	VISP1680
28 T9(L) = CC(1)*DH1(L,1) + CC(2)*DH1(L,2) + CC(3)*DH1(L,3)	VISP1690
C	VISP1700
C COMPUTE TOTAL TORQUE IN INERTIAL REFERENCE BY	VISP1710
C TQ = -CV*WIJ + CSA*T7 + CSB*T8 + TQC*T9	VISP1720
C	VISP1730
34 IF (NJ.EQ.0) GO TO 36	VISP1740
CV = 0.0	VISP1750
IF (IJ.NE.1) CSA = 0.0	VISP1760
IF (IJ.NE.2) CSB = 0.0	VISP1770
IF (IJ.NE.4) TQC = 0.0	VISP1780
36 DO 37 L=1,3	VISP1790
TQ(L,J) = -CV*WIJ(L) + CSA*T7(L) + CSB*DH2(L,3) + TQC*T9(L)	VISP1800
37 TTI(L) = TQ(L,J)	VISP1810
IF (NPRT(12).NE.0) WRITE (6,39)	VISP1820
* J, CV, CSA, CSB, TQC, HAD, HAC, HBC, RA, RB,	VISP1830
* HD3, WIJ, T7, T9,	VISP1840
* (TQ(L,J), L=1,3)	VISP1850
39 FORMAT(I4,1P9D14.6/(4X,9D14.6))	VISP1860
C	VISP1870
C ADD TORQUE CONVERTED TO LOCAL REFERENCE BY	VISP1880
C U2I = U2I + DI*TQ	VISP1890
C U2J = U2J - DJ*TQ	VISP1900
C	VISP1910
DO 40 L=1,3	VISP1920
DO 40 M=1,3	VISP1930
U2(L,I) = U2(L,I) + D(L,M,I)*TQ(M,J)	VISP1940
40 U2(L,J+1) = U2(L,J+1) - D(L,M,J+1)*TQ(M,J)	VISP1950
C	VISP1960
C STORE DATA FOR OUTPUT ROUTINE INTO PRJNT ARRAY.	VISP1970
C	VISP1980
PRJNT(1,J) = ANGL(1)	VISP1990
PRJNT(2,J) = ANGL(3)	VISP2000

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PRJNT(3,J) = CSAP
PRJNT(4,J) = CSB
PRJNT(5,J) = CV*WIJM
PRJNT(6,J) = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)
90 CONTINUE
CALL ELTIME(2,13)
99 RETURN
END
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VISP2010
VISP2020
VISP2030
VISP2040
VISP2050
VISP2060
VISP2070
VISP2080
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C          SUBROUTINE WINDY(M,MM,N,NN,NT)
C
C          REV 12 12/20/74
C          COMPUTES FORCES AND TORQUES ADDING THEM TO THE U1 AND U2 ARRAYS
C          OF WIND BLAST FORCES DETERMINED BY FUNCTION STORED IN TAB(NT)
C          ON ELLIPSOID (MM) ATTACHED TO BODY SEGMENT (M) WHICH EXTENDS
C          THROUGH THE INTERSECTING PLANE (NN) ATTACHED TO SEGMENT (N).
C
C          IMPLICIT REAL*8 (A-H,O-Z)
C          COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)
C          COMMON/TABLES/MXNT1,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)
C          COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
C          *          ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
C          COMMON/CNTRSF/ PL(17,20),GAB(8,3),BELT(20,8),TPTS(6,8),BD(24,25)
C          COMMON/CNSNTS/ PI, RADIANT,G,THIRD,EPS1,EPS4,EPS6,EPS8,
C          *          EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)
C          COMMON/VPOSTN/ TIME,XO(3),XDOTO(3),XCOMP(3),XVCOMP(3),AX(3),
C          *          ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,
C          *          NATAB,NACLR,DVEH(3,3),VMEG(3),VMEGD(3),XACOMP(3),
C          *          THET(3),ZPLT(3)
C          COMMON/TEMPVS/ DMNT(3,3),XMN(3),XMM(3),TM(3),BET,BTS,P,FT(3),
C          *          FF(3),AF(3),FAF,TF,BREF,SCALE,TRACER,AREA,RLM(3),
C          *          TQM(3),RM(3)
C          COMMON/KALEPS/WTIME(30),IWIND(30)
C          CALL ELTIME(1,35)
C
C          COMPUTE PENETRATION DISTANCE; IF NEGATIVE, RETURN.
C
C          CALL DOTD(D(1,1,M),D(1,1,N),DMNT,3,3,3)
C          DO 10 I=1,3
C          10 XMN(I) = SEGLP(I,M) - SEGLP(I,N)
C          CALL MAT(D(1,1,M),XMN,XMM,3,3,1,3,3,3)
C          CALL MAT(DMNT,PL(1,NN),TM,3,3,1,3,3,3)
C          BET = PL(4,NN)
C          DO 11 I=1,3
C          11 BET = BET - TM(I)*(BD(I+3,MM)+XMM(I))
C          CALL MAT(BD(16,MM),TM,RM,3,3,1,3,3,3)
C          BTS = TM(1)*RM(1) + TM(2)*RM(2) + TM(3)*RM(3)
C          BTE = -DSQRT(BTS)
C          P = BET - BTE
C          IF (P.LT.0.0) GO TO 99
C
C          FETCH OR STORE INITIAL PENETRATION TIME.
C
C          IWIND(M) = M
C          IF (TIME.LE.WTIME(M)) WTIME(M) = TIME
C          FTIME = TIME - WTIME(M)
C
C          GET FORCE VECTOR FT FROM TABLE NT FOR TIME = FTIME.
C
C          22 KT = NTI(NT)

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NENTRY = TAB(KT+5)	WIND0510
KI = K1+10	WIND0520
K2 = 4*NENTRY + KT+2	WIND0530
IF (NENTRY.EQ.1) GO TO 31	WIND0540
DO 30 K=K1,K2,4	WIND0550
IF (FTIME.GT.TAB(K)) GO TO 30	WIND0560
KK = K	WIND0570
R1 = (TAB(K)-FTIME)/(TAB(K)-TAB(K-4))	WIND0580
GO TO 32	WIND0590
30 CONTINUE	WIND0600
31 KK = K2	WIND0610
R1 = 0.0	WIND0620
32 R2 = 1.0 - R1	WIND0630
DO 33 I=1,3	WIND0640
K= KK+I	WIND0650
33 FT(I) = R2*TAB(K) + R1*TAB(K-4)	WIND0660
C	WIND0670
C	WIND0680
C	WIND0690
COMPUTE PRESENTED AREA TO WIND FORCE.	WIND0700
CALL MAT(D(I,I,M),FT,FF,3,3,1,3,3,3)	WIND0710
CALL MAT(BD(7,MM),FF,AF,3,3,1,3,3,3)	WIND0720
FAF = FF(I)*AF(1) + FF(2)*AF(2) + FF(3)*AF(3)	WIND0730
IF (FAF.LE.0.0) GO TO 99	WIND0740
TF = TM(1)*FF(I) + TM(2)*FF(2) + TM(3)*FF(3)	WIND0750
BREF = DSQRT(BTS-TF*TF/FAF)	WIND0760
SCALE = (-BET+BREF)/(-BTE+BREF)	WIND0770
IF (SCALE.GE.1.0) GO TO 99	WIND0780
IF (SCALE.LT.0.0) SCALE = 0.0	WIND0790
TRACER = (BD( 7,MM)-AF(1)**2/FAF)*(BD(I1,MM)-AF(2)**2/FAF)	WIND0800
* + (BD( 7,MM)-AF(1)**2/FAF)*(BD(I5,MM)-AF(3)**2/FAF)	WIND0810
* + (BD(11,MM)-AF(2)**2/FAF)*(BD(15,MM)-AF(3)**2/FAF)	WIND0820
* - (BD( 8,MM)-AF(1)*AF(2)/FAF)**2	WIND0830
* - (BD( 9,MM)-AF(1)*AF(3)/FAF)**2	WIND0840
* - (BD(12,MM)-AF(2)*AF(3)/FAF)**2	WIND0850
AREA = (I.0-SCALE**2) * PI / DSQRT(TRACER)	WIND0860
C	WIND0870
C	WIND0880
C	WIND0890
ADD FORCE AND TORQUES TO UI AND U2 ARRAYS FOR SEGMENT M.	WIND0900
SCALE = SCALE/BTE	WIND0910
DO 36 I=1,3	WIND0920
RLM(I) = RM(I)*SCALE + BD(I+3,MM)	WIND0930
FT (I) = FT(I)*AREA	WIND0940
36 FF (I) = FF(I)*AREA	WIND0950
CALL CROSS (RLM,FF,TQM)	WIND0960
DO 39 I=1,3	WIND0970
UI(I,M) = U1(I,M) + FT(I)	WIND0980
39 U2(I,M) = U2(I,M) + TQM(I)	WIND0990
IF (NPRT(14).NE.0) WRITE (6,41) TIME,M,P,AREA,FT,TQM	WIND1000
41 FORMAT(' WIND FORCE',F14.6,I6,2F10.3,3X,3F12.5,3X,3F12.5)	
99 CALL ELTIME (2,35)	